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## DRAFT: OPTIMAL MOTION GENERATION FOR EXITING A PARALLEL MANIPULATOR FROM A TYPE 2 SINGULARITY

Georges Pagis<sup>1,2,3</sup>, Sébastien Briot<sup>1\*</sup>, Nicolas Bouton<sup>3</sup> and Philippe Martinet<sup>1,2</sup>

<sup>1</sup> Institut de Recherche en Communications et Cybernétique de Nantes (IRCCyN), UMR CNRS 6597, 44321 Nantes, France

<sup>2</sup> LUNAM, Ecole Centrale de Nantes, 44321 Nantes, France

<sup>3</sup> Institut Pascal, IFMA, MMS department, UMR CNRS 6602, 63000 Clermont-Ferrand, France  
{Georges.Pagis,Sébastien.Briot,Philippe.Martinet}@ircryn.ec-nantes.fr  
nicolas.bouton@ifma.fr

### ABSTRACT

*Parallel robots have proved they can have better performances than serial ones in term of rigidity and payload-to-weight ratio. Nevertheless their workspace is largely reduced by the presence of singularities. In particular, the Type 2 singularities (parallel singularities) separate the workspace in different aspects, corresponding to one (or more) robot assembly modes. In order to enlarge the workspace size, it has been proved that a mechanism can cross the singularity loci by using an optimal motion planning. However, if the trajectory is not robust to modelling errors, the robot can stop in the singularity and stay blocked.*

*Therefore, the objective of this paper is to show new general procedure that allows the exit of a parallel manipulator from a Type 2 singularity. Two strategies are presented. The first one proposes the computation of an optimal trajectory that makes it possible for the robot to exit the singularity. This trajectory must respect a criterion that ensures the consistency of the robot dynamic model all along the singularity loci. The second trajectory consists in de-clutching one of the robot actuator in order to change the kinematic and dynamic behavior of the mechanism so that no singularity exists anymore. Theoretical works are illustrated, discussed and analysed through simulations achieved on a planar five-bar mechanism.*

### 1 Introduction

Parallel manipulators have many advantages in terms of acceleration capacities and payload-to-weight ratio, but one of their main drawbacks concerns the presence of singularities [1–5] which divide the workspace into different aspects, each aspect corresponding to one (or more) assembly modes [6]. The physical interpretation of a singularity in kinematics refers to the parallel manipulators configurations in which either the manipulator loses the ability to move in some directions, or its platform gains instantaneously some unconstrained motions.

In [2], three different types of singularities are described:

- Type 1 singularities are configurations where the platform loses a degree of freedom; the Type 1 singularities are configurations where the end-effector reaches the limits of the workspace,
- Type 2 singularities are configurations where an uncontrollable motion of the platform appears; the Type 2 singularities have much more complex loci, which divides the workspace in different aspects, resulting in a reduction of the manipulator's workspace; in general, in the neighborhood of such singularities, the reaction in passive and active joints considerably increase, thus preventing the manipulator to cross them,
- Type 3 singularities are configurations where both Type

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\*Address all correspondence to this author.

1 and Type 2 singular configurations appear at the same time.

Moreover, in addition of these first works, other types of singularities, such as the constraint singularities [5], have been studied. For a global overview of the singularity problem, the reader is referred to [3]. However, the present paper focus only on Type 2 singularities as they are probably the most constraining singularities a parallel manipulator can meet.

In order to increase the workspace size, largely reduced by Type 2 singularity, several approaches have been envisaged in the literature. The most usual one is the design of parallel robots without singularities. Many works have been proposed in this direction, using optimal design approaches [7–9] or even the creation of decoupled mechanisms without any singularity [10,11]. However, except in the case of decoupled robot that have a lack of stiffness, the design of robots in which only a portion of the workspace is free of singularity is generally envisaged.

Another solution was to use redundancy [12–14]. However, this solution is costly and increase the control complexity. To avoid this problem, it has been proposed in [4] to use mechanisms with variable actuation modes to increase the size of the workspace. These mechanisms allow, without the addition of any supplementary actuators, to change the way they are actuated, via the use of clutches. This low-cost solution is attractive, however, the change in the actuation mode must be done when the manipulator is stopped, thus increasing the time for doing the requested trajectory.

A last solution is to create mechanisms with singularities inside the workspace, but to plan trajectories that allow the manipulators to go from one assembly mode to another. Two types of approaches have been developed in this direction:

1. the non singular assembly mode changing [15,16]: by encircling cusp points, it has been demonstrated that the robot assembly modes can be changed; however, the computation of the cusp point loci is still a challenge in kinematics and such solution requires high mathematical skills. Moreover, it does not guaranty that the manipulator will be able to reach the whole workspace aspects,
2. the singular assembly mode changing [17–19]: using the manipulator inertial properties, it has been demonstrated that it was possible to cross a Type 2 singularity without any considerable increase in the joint reactions and input torques; in [17], the physical condition for crossing a Type 2 singularity has been demonstrated.

The last approach is promising. However, if the trajec-

tory for crossing the singularity is poorly planned (because of problems of robustness to modeling errors, for example), there is a risk that the mechanism can stop on the singularity and stay blocked inside. If such case appears, some methodologies for exiting the singularities must be found. Therefore the present paper aims at defining two strategies for exiting a Type 2 singularity if the manipulator is stopped inside.

## 2 Dynamic modelling of parallel mechanisms

### 2.1 Lagrangian formalism

Let us consider a parallel manipulator composed of  $m$  links,  $n$  degrees of freedom (*dof*) and driven by  $n$  actuators. In general, for such mechanism, the Lagrangian  $L$  of the system is expressed as a function of both the actuator and platform coordinates, i.e.

$$L = L(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{x}, \mathbf{v}) \quad (1)$$

where

- $\mathbf{q} = [q_1, q_2, \dots, q_n]^T$  and  $\dot{\mathbf{q}} = [\dot{q}_1, \dot{q}_2, \dots, \dot{q}_n]^T$  represent respectively the vector of active joints variables and active joints velocities,
- $\mathbf{x} = [x, y, z, \phi, \psi, \theta]^T$  and  $\mathbf{v} = [\dot{x}, \dot{y}, \dot{z}, \dot{\phi}, \dot{\psi}, \dot{\theta}]^T$  are the end-effector pose parameters and their derivatives with respect to time, respectively.  $x, y$  and  $z$  represent the position of the platform controlled point and  $\phi, \psi$  and  $\theta$  the orientation parameters of the platform about three axes  $\mathbf{a}_\phi, \mathbf{a}_\psi$  and  $\mathbf{a}_\theta$ .

The Lagrangian dynamic formulation for the considered parallel manipulator can be thus expressed as [20],

$$\tau = \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\mathbf{q}}} \right) - \frac{\partial L}{\partial \mathbf{q}} + \mathbf{B}^T \lambda \quad (2)$$

where

- $\tau$  is the vector of the input efforts,
- $\lambda$  is the vector of the Lagrange multipliers, whose expression can be computed using

$$\mathbf{A}^T \lambda = \frac{d}{dt} \left( \frac{\partial L}{\partial \mathbf{v}} \right) - \frac{\partial L}{\partial \mathbf{x}} = \mathbf{w}_p \quad (3)$$

in which

- $\mathbf{A}$  and  $\mathbf{B}$  are two matrices deduced from the kinematic model, such that  $\mathbf{A}\mathbf{v} = \mathbf{B}\dot{\mathbf{q}}$  [6],

- $\mathbf{w}_p$  is the wrench applied to the platform by the legs and external forces [21].

Then, by substituting (3) into (2), and assuming that the matrix  $\mathbf{A}$  is regular, one can obtain [20]:

$$\tau = \mathbf{w}_b + \mathbf{J}^T {}^0\mathbf{w}_p, \text{ in which } \mathbf{w}_b = \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\mathbf{q}}} \right) - \frac{\partial L}{\partial \mathbf{q}} \quad (4)$$

where

- ${}^0\mathbf{w}_p$  is the expression of the wrench  $\mathbf{w}_p$  in the base frame, i.e.  ${}^0\mathbf{w}_p = \mathbf{D}\mathbf{w}_p$  with  $\mathbf{D}$  the matrix relating the platform twist  $\mathbf{t}$  (expressed in the base frame) to the vector  $\mathbf{v}$  by  $\mathbf{t} = \mathbf{D}\mathbf{v}$  [6],
- $\mathbf{J} = {}^0\mathbf{A}^{-1}\mathbf{B}$  is the Jacobian matrix between the platform twist  $\mathbf{t}$  and  $\dot{\mathbf{q}}$ , with  ${}^0\mathbf{A}$  is the expression of the matrix  $\mathbf{A}$  in the base frame, i.e.  ${}^0\mathbf{A} = \mathbf{A}\mathbf{D}^{-1}$ .

Thus, by analyzing (4), it can be deduced that if matrix  ${}^0\mathbf{A}$  is singular, the dynamic model (4) cannot be computed. As a consequence, the next part deals with the conditions of singularity for matrix  ${}^0\mathbf{A}$ .

## 2.2 Parallel mechanism's singularities

As presented in the introduction, the authors of [2] present three different types of singularities that can be obtained through the analysis of the kinematic model:

$${}^0\mathbf{A}\mathbf{t} = \mathbf{B}\dot{\mathbf{q}} \quad (5)$$

**Type 1 singularities** occur when the mechanism is in a position such as the kinematic matrix  $\mathbf{B}$  becomes rank deficient. In such configurations, the mechanism loses the ability to move in one given direction.

**Type 2 singularities** occur when the kinematic matrix  ${}^0\mathbf{A}$  becomes rank deficient. The Type 2 singularities divides the workspace in different aspects, resulting in a reduction of the manipulator's workspace. Moreover, in the presence of such singularities, the robot may also not be able to resist to an external wrench applied on the platform and the reaction in joints grows to infinity.

**Type 3 singularities** are configurations where both Type 1 and Type 2 singular configurations appear at the same time. They are discarded in the following of the paper as they appear if both Types 1 and 2 singularity exist.

In the next section, it is explained how to pass through a Type 2 singularity without making the dynamic model (4) degenerating, thus keeping the joint reactions in the parallel manipulator finite.

## 2.3 Condition for passing through a Type 2 singularity

In [17], it has been proved that a parallel mechanism can cross a Type 2 singularity without making the dynamic model (4) degenerating if and only if the trajectory respects a particular criterion at the singular point. Indeed, on a Type 2 singularity, the columns of  ${}^0\mathbf{A}$  are linearly dependent, i.e. there exist a vector  $\mathbf{t}_s$  such that:

$${}^0\mathbf{A}\mathbf{t}_s = 0 \Leftrightarrow \mathbf{t}_s^T {}^0\mathbf{A}^T = 0 \quad (6)$$

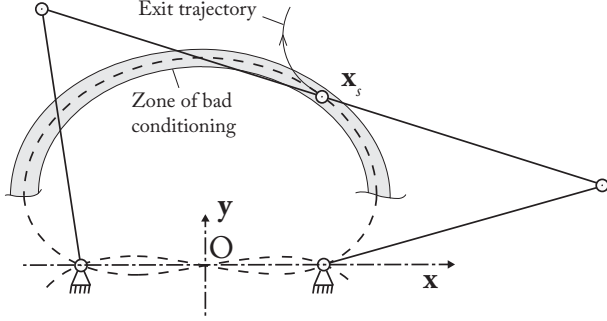
The vector  $\mathbf{t}_s$  represents the twist of the uncontrollable motion of the platform in the singularity locus [6]. Thus, multiplying (3) by  $\mathbf{t}_s^T$  leads to :

$$\mathbf{t}_s^T {}^0\mathbf{A}^T \lambda = 0 \Rightarrow \mathbf{t}_s^T {}^0\mathbf{w}_p = 0 \quad (7)$$

As a result, if the desired manipulator motion doesn't guaranty the creation of a wrench  $\mathbf{w}_p$  that respects the condition (7), the dynamic model is degenerated and the manipulator desired input efforts must grow to infinity to produce the desired platform motion. Physically, this condition means that the parallel manipulator can cross the Type 2 singularity if and only if the wrench  ${}^0\mathbf{w}_p$  exerted by the legs and external efforts on the platform is reciprocal to the twist  $\mathbf{t}_s$  of the uncontrollable motion in the Type 2 singularity. Based on this observation, it has been proved in [17] that it is possible to plan a trajectory that crosses a Type 2 singularity as long as the criterion (7) is respected on the singularity. It should be finally mentioned that, for one given set of robot inertial parameters, this condition depends only on the input joint and platform coordinates, velocities and accelerations.

## 3 Methodologies for exiting a singularity

If any parallel manipulator user wants to cross a Type 2 singularity by applying the criterion (7), it should be aware that if the trajectory is poorly planned (because of problems of robustness to modeling errors, for example), the mechanism can stop on the singularity and stay blocked inside. If such case appears, some methodologies for exiting the singularities must be found. This part aims at defining two strategies for getting out of Type 2 singularities. The first one consists in generating an optimal motion for the mechanism in order to follow an exit trajectory that guaranties the input efforts continuity all along the path. The second solution proposed relies on declutching one of the motor in order to change the mechanism's dynamical behaviour.



**FIGURE 1.** A PLANAR 5R MECHANISM BLOCKED ON A TYPE 2 SINGULARITY

### 3.1 First solution: generation of an optimal motion

The main idea of this solution can be explained as follows. Let us assume that the mechanism is stopped on the singularity locus at a point of coordinate  $\mathbf{x}_s$  (as the 5R mechanism presented in Fig. 1). To exit the singularity, the mechanism must generate a trajectory that:

- is tangent to the singularity locus at point  $\mathbf{x}_s$  as, when stopped, it cannot generate a motion orthogonal to the singularity locus,
- is  $\mathcal{C}^2$  continuous to ensure the input effort continuity all along the path,
- respects the criterion (7) at point  $\mathbf{x}_s$ .

However, the mechanism being stopped into the singularity, i.e. its velocity being null when starting the motion at  $\mathbf{x}_s$ , if there is no external wrench applied such as the gravity field, this trajectory may fail exiting the robot from the singularity as it may have not enough energy to compensate the friction and local mechanical instability effects (due to the robot loss of stiffness) around the singularity point. As a result, in order to acquire enough energy, it is worth moving the robot inside the singularity loci during a certain amount of time before exiting the singularity. Thus, the trajectory can be cut into two parts:

1. a first trajectory that makes the robot platform move along the singularity locus,
2. a second trajectory that is  $\mathcal{C}^2$  continuous with the first one and able to make the robot go away from the singularity locus.

Obviously, the whole trajectory must guaranty that the input efforts remain finite during the whole motion. The way to compute these two different trajectories is detailed in the next sections.

#### 3.1.1 First trajectory: moving along the singularity locus

**Trajectory generation along the singularity** In general, the computation of the singularity loci in the workspace is not an easy and straightforward problem [6]. Therefore, it is mostly difficult to get the symbolic constraint equations for the platform pose coordinates that impose the robot to stay in singularity. On the contrary, it is shown below that it is possible to find some sets of platform velocity parameters that can guaranty the robot to stay on the singularity loci.

Differentiating (6) with respect to time, it comes that:

$${}^0\mathbf{A}\dot{\mathbf{t}}_s + {}^0\dot{\mathbf{A}}\mathbf{t}_s = 0 \quad (8)$$

in which, as matrix  ${}^0\mathbf{A}$  depends on the variables  $\mathbf{x}$  and  $\mathbf{q}$  only [6],

$${}^0\dot{\mathbf{A}} = \sum_i \left( \frac{\partial {}^0\mathbf{A}}{\partial x_i} \dot{x}_i + \frac{\partial {}^0\mathbf{A}}{\partial q_i} \dot{q}_i \right) \quad (9)$$

where  $x_i$  ( $q_i$ , resp.) is the  $i$ -th coordinate of the vector  $\mathbf{x}$  ( $\mathbf{q}$ , resp.). Multiplying the right side of (9) by  $\mathbf{t}_s$ , it comes:

$$\begin{aligned} {}^0\dot{\mathbf{A}}\mathbf{t}_s &= \sum_i \left( \frac{\partial {}^0\mathbf{A}}{\partial x_i} \mathbf{t}_s \dot{x}_i + \frac{\partial {}^0\mathbf{A}}{\partial q_i} \mathbf{t}_s \dot{q}_i \right) \\ &= \mathbf{A}_x^d \mathbf{v} + \mathbf{A}_q^d \dot{\mathbf{q}} = \mathbf{A}_x^d \mathbf{D}^{-1} \mathbf{t} + \mathbf{A}_q^d \dot{\mathbf{q}} \end{aligned} \quad (10)$$

where the  $i$ -th column of  $\mathbf{A}_x^d$  ( $\mathbf{A}_q^d$ , resp.) is equal to  $\frac{\partial {}^0\mathbf{A}}{\partial x_i} \mathbf{t}_s$  ( $\frac{\partial {}^0\mathbf{A}}{\partial q_i} \mathbf{t}_s$ , resp.).

Introducing (5) into (10) leads to

$$\begin{aligned} {}^0\dot{\mathbf{A}}\mathbf{t}_s &= \mathbf{A}_x^d \mathbf{D}^{-1} \mathbf{t} + \mathbf{A}_q^d \mathbf{B}^{-1} {}^0\mathbf{A} \mathbf{t} \\ &= \left( \mathbf{A}_x^d \mathbf{D}^{-1} + \mathbf{A}_q^d \mathbf{B}^{-1} {}^0\mathbf{A} \right) \mathbf{t} \\ &= \mathbf{A}_x \mathbf{t} \end{aligned} \quad (11)$$

Putting this expression into (8), it comes that

$${}^0\mathbf{A}\dot{\mathbf{t}}_s + \mathbf{A}_x \mathbf{t} = 0 \Rightarrow \mathbf{t} = -\mathbf{A}_x^{-1} {}^0\mathbf{A}\dot{\mathbf{t}}_s = \mathbf{A}_t \dot{\mathbf{t}}_s \quad (12)$$

As vectors  $\mathbf{t}_s$  and  $\dot{\mathbf{t}}_s$  are only defined on the singularity loci, (12) gives the conditions such that the robot stays in singularity. If the condition (12) is not verified for at least one value of the vector  $\dot{\mathbf{t}}_s$ , the manipulator could potentially exit the singularity.

As a result, to move the robot on the singularity, two conditions must be achieved:

- (12) for obtaining the kinematic constraints such that the robot can stay in singularity,
- (7) for obtaining the dynamic constraints that guarantee the dynamic model to be not degenerated.

Introducing (12) into (7) leads to the obtention of a non-linear differential equation of the second order that must be solved for computing the robot displacement on the singularity loci.

**Computation of the input efforts** Even if the criterion (7) is respected, it is still problematic to compute the input efforts when the robot is in the singularity. Having a look at (3), if  $p$  denotes the rank of the matrix  $\mathbf{A}$  in singularity ( $p < n$ ), it appears that only  $p$  equations are linearly dependent. Thus, there is an infinity of possible sets for the values of the  $n$  Lagrange multipliers  $\lambda$  that satisfies the equation (3). Physically speaking, this means that the robot is locally over-constrained in the singularity. As a result, several approaches could be chosen to compute the values of the Lagrange multipliers such as the use of the pseudo-inverse of the matrix  $\mathbf{A}$  (as it was done in the case of actuation redundant parallel robots [22]) or setting  $(n - p)$  Lagrange multipliers to a given constant value. This last approach will be used in the following of the paper.

### 3.1.2 Second trajectory: exiting the singularity locus

#### Trajectory generation for exiting the singularity

Once the mechanism has acquired enough energy, the second trajectory that allows the exit from the singularity loci must be followed. This trajectory must be  $\mathcal{C}^2$  continuous with the first one in order to avoid any torque discontinuity (Fig. 1). Several types of  $\mathcal{C}^2$  curves can thus be used, such as Lamé curves [23], clothoids [24, 25] or also S-curves [26]. In the following of the paper, clothoids are used. The way to link the clothoids to the trajectory defined in the section 3 is not detailed here. For more informations the reader is referred to [27].

One could wonder how to chose the aspect of the workspace in which the robot must go after exiting the singularity? Indeed, as on the singularity loci, one platform *dof* is non constrained, the robot is locally underactuated. As a result, it seems impossible to plan a trajectory that is opposed to the free dynamics of this unconstrained *dof*. To know what is the best assembly mode to reach, the natural direction of movement of the mechanism free of actuation forces must be defined at the exit point. This can be done *in simulation* by declutching all actuators at the exit point after the motion along the singularity locus and by using

the direct dynamic model that express the mechanism acceleration as a function of the input efforts (that are null in this case) to compute the robot displacement [20]. The mechanism will spontaneously move to one of the workspace aspects that will be the one to reach with the exit trajectory.

**Computation of the input efforts** Theoretically, the matrix  ${}^0\mathbf{A}$  is not invertible only on the Type 2 singularity locus. However when the mechanism is very close to a singular position, the conditioning of the matrix  ${}^0\mathbf{A}$  is very high (Fig. 1). The dynamic model is therefore still degenerated in a area around the singularity locus. Inside this zone, it is irrelevant to use the numerical invert of  ${}^0\mathbf{A}$  to compute the input efforts. The best way to do is to consider that the robot is still in singularity in this area and to compute the input efforts using the methods presented in the Section 3.1.1.

When the robot exits this zone, i.e. when the conditioning of the matrix  ${}^0\mathbf{A}$  becomes acceptable, the input efforts can be computed using (2) and (3). In the following of the paper, the value of the conditioning of the matrix  ${}^0\mathbf{A}$  is said acceptable if it is equal or inferior to 100. Obviously, this value is arbitrary, but it will be shown in the next section that it leads to correct results.

### 3.1.3 Discussion on the amount of energy necessary for exiting the singularity

It has been explained above that the change between the two trajectories must be achieved when the mechanism has acquired enough energy to exit the singularity. So, when does this appear and how to have the corresponding information? This point is still an open question for the moment, however, one possible answer is to consider the energy consumed by the actuators for compensating the friction in the passive joints and the energy of the moving robot platform and passive links. If the amount of the robot platform and passive links energy is large enough (e.g. 5 times larger) with respect to the amount of energy for compensating the dissipative terms, thus the change on the trajectory can be done. This point must be deeply analyzed in our future work.

### 3.2 Second solution: declutch one of the actuators

A second solution for exiting the singularity is to change the robot dynamics by changing its actuation mode, e.g. by declutching one of the actuators from the rest of the robot. As a consequence, the parallel mechanism becomes underactuated, which completely changes its singular configurations and dynamic properties.

Without loss of generality, let us assume that the input

effort of the actuator  $n$  is vanished, i.e. the last component of vector  $\tau$  of (2) is set to 0. Rewriting (2), it comes that:

$$\begin{bmatrix} \tau_1 \\ \vdots \\ \tau_{n-1} \\ 0 \end{bmatrix} = \begin{bmatrix} w_{b_1} \\ \vdots \\ w_{b_{n-1}} \\ w_{b_n} \end{bmatrix} + \begin{bmatrix} \mathbf{b}_1 \\ \vdots \\ \mathbf{b}_{n-1} \\ \mathbf{b}_n \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_{n-1} \\ \lambda_n \end{bmatrix} \quad (13)$$

$$\mathbf{w}_p = \begin{bmatrix} \mathbf{a}_1 \\ \vdots \\ \mathbf{a}_{n-1} \\ \mathbf{a}_n \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_{n-1} \\ \lambda_n \end{bmatrix} \quad (14)$$

where  $\tau_i$  is the  $i$ -th component of the vector  $\tau$ ,  $w_{b_i}$  the  $i$ -th component of the vector  $\mathbf{w}_b$ ,  $\lambda_i$  is the  $i$ -th component of the vector  $\lambda$ ,  $\mathbf{a}_i$  the  $i$ -th row of the matrix  $\mathbf{A}^T$  and  $\mathbf{b}_i$  the  $i$ -th row of the matrix  $\mathbf{B}^T$ . Rearranging these equations,

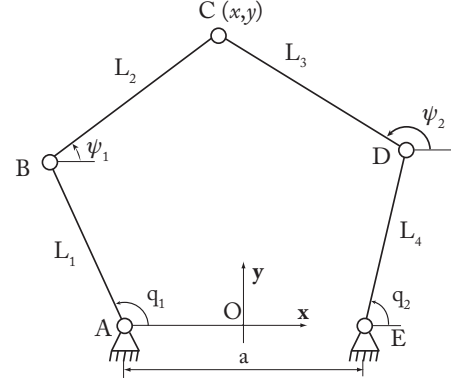
$$\begin{bmatrix} \tau_1 \\ \vdots \\ \tau_{n-1} \end{bmatrix} = \begin{bmatrix} w_{b_1} \\ \vdots \\ w_{b_{n-1}} \end{bmatrix} + \begin{bmatrix} \mathbf{b}_1 \\ \vdots \\ \mathbf{b}_{n-1} \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_{n-1} \\ \lambda_n \end{bmatrix} \quad (15)$$

$$\begin{bmatrix} \mathbf{w}_p \\ -w_{b_n} \end{bmatrix} = \begin{bmatrix} \mathbf{a}_1 \\ \vdots \\ \mathbf{a}_{n-1} \\ \mathbf{a}_n \\ \mathbf{b}_n \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_{n-1} \\ \lambda_n \end{bmatrix} = \mathbf{A}^* \lambda \quad (16)$$

in which the matrix  $\mathbf{A}^*$  is now invertible and can be used to compute the Lagrange multipliers in the singularity loci. Obviously, the expression (16) must be used on the singularity only (and also in a small zone around, as explained in the Section 3.1.2). As soon as the robot is nomore on the singularity, matrix  $\mathbf{A}$  becomes regular and (14) can be used as it. However, as one actuator is declutched and as the robot is under-actuated, the direct dynamic model must be used for computing the robot displacement and being sure that there is no link collision during the motion [20]. In order to avoid this problem, the best way to proceed is to give a small impulse of motion to only one of the actuators and to stop it quite quickly in order to avoid a too large platform displacement.

### 3.3 Discussion about the advantages and drawbacks of the two proposed solutions

The two proposed solutions have advantages and drawbacks. In the first solution, the mechanism is fully controlled during its whole motion while in the second one, as



**FIGURE 2.** PLANAR 5R PARALLEL MECHANISM DESCRIPTION

one actuator is declutched, there is a risk that the robot falls down under the application of external efforts such as the gravity. However, the first solution requires larger computational skills and needs to define two special types of trajectories whereas the second one seems simpler in terms of computation complexity. Therefore, both solutions have interests, depending of robots on which they are applied.

## 4 Illustrative example

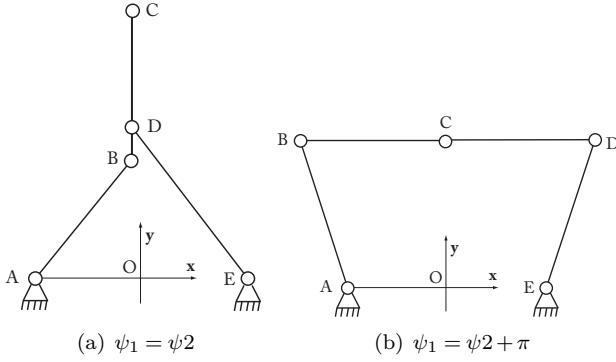
The two methodologies proposed to exit a Type 2 singularity are applied and simulated using the model of a 5R planar mechanism.

### 4.1 Description and modelling of the 5R mechanism

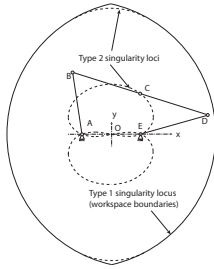
The planar 5R parallel mechanism is composed of two legs connecting by a revolute joint the end-effector located at point C to the base, as shown in Fig. 2. Each leg is composed of two rigid elements, called the *proximal* and *distal* elements, respectively. The proximal element is linked to the base via an actuated revolute joint and to the proximal element via a passive revolute joint. The two revolute joints connecting the legs to the base are actuated (located at the points A and E on the Fig. 2), which enables the end-effector located at point C to be positionned in the plane ( $Oxy$ ).

The notations used in the following of the paper are:

- $q_1$  and  $q_2$  are the angles of the actuated revolute joints
- $\psi_1$  and  $\psi_2$  are the passive angles of joints located at points B and D
- $L_i$  is the length of the leg  $i$
- $x$  and  $y$  are the end-effector's positions along the  $\mathbf{x}$  and  $\mathbf{y}$  axes, respectively,
- $a$  is the distance between the two actuators.



**FIGURE 3.** TYPE 2 SINGULARITIES OF THE 5R PLANAR MECHANISM.



**FIGURE 4.** SINGULARITY LOCI FOR THE PLANAR 5R MECHANISM UNDER STUDY.

For the 5R planar mechanism, Type 2 singularities occur when the two distal elements are parallel [28]. Two different cases may appear, as shown on the Fig. 3, either  $\psi_1 = \psi_2$  (Fig. 3(a)) or  $\psi_1 = \psi_2 + \pi$  (Fig. 3(b)).

In the following of the paper, the gravity field is directed along the  $\mathbf{z}$ -axis. The equations of the dynamic model for the 5R mechanisms have been described in [17], and the vectors and matrices necessary for computing the dynamic model (2) take the form:

$$\mathbf{w}_b = \begin{bmatrix} m_{B_1} L_1^2 \ddot{q}_1 + m_{C_1} L_1 (\ddot{y} \cos q_1 - \ddot{x} \sin q_1) \\ m_{D_2} L_4^2 \ddot{q}_2 + m_{C_3} L_4 (\ddot{y} \cos q_2 - \ddot{x} \sin q_2) \end{bmatrix} \quad (17)$$

$$\begin{aligned} \mathbf{w}_p = & \begin{bmatrix} m_{C_2} \ddot{x} - m_{C_1} L_1 (\ddot{q}_1 \sin q_1 + \dot{q}_1^2 \cos q_1) \\ m_{C_2} \ddot{y} + m_{C_1} L_1 (\ddot{q}_1 \cos q_1 - \dot{q}_1^2 \sin q_1) \end{bmatrix} \\ & + \begin{bmatrix} -m_{C_3} L_4 (\ddot{q}_2 \sin q_2 + \dot{q}_2^2 \cos q_2) \\ m_{C_3} L_4 (\ddot{q}_2 \cos q_2 - \dot{q}_2^2 \sin q_2) \end{bmatrix} \end{aligned} \quad (18)$$

$$\mathbf{A} = \begin{bmatrix} x + a/2 - L_1 \cos q_1 & y - L_1 \sin q_1 \\ x - a/2 - L_4 \cos q_2 & y - L_4 \sin q_2 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \quad (19)$$

$$\mathbf{B} = - \begin{bmatrix} L_1 (\sin q_1 a_{11} - \cos q_1 a_{12}) & 0 \\ 0 & L_4 (\sin q_2 a_{21} - \cos q_2 a_{22}) \end{bmatrix} \quad (20)$$

with

$$\begin{aligned} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} &= \mathbf{B}^{-1} \mathbf{A} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} \\ \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} &= \mathbf{B}^{-1} \left( \mathbf{A} \begin{bmatrix} \ddot{x} \\ \ddot{y} \end{bmatrix} + \dot{\mathbf{A}} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} - \dot{\mathbf{B}} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} \right) \end{aligned} \quad (21)$$

and

$$\begin{aligned} m_{C_1} &= m_{22} r_2 (1 - r_2) \\ m_{C_2} &= m_{22} r_2^2 + m_{32} r_3^2 + m_{23} + m_{21} \\ m_{C_3} &= m_{32} r_3 (1 - r_3) \\ m_{B_1} &= m_{12} r_1^2 + m_{22} (1 - r_2)^2 + m_{13} + m_{21} \\ m_{D_2} &= m_{32} (1 - r_3)^2 + m_{42} r_4^2 + m_{31} + m_{41} \end{aligned} \quad (22)$$

in which  $r_1$  ( $r_2$ ,  $r_3$ ,  $r_4$ , resp.) is a ratio such that  $r_1 L_1$  ( $r_2 L_2$ ,  $r_3 L_3$ ,  $r_4 L_4$ , resp.) is the distance between the center of masses of the element 1 (2, 3, 4, resp.) and the point A (B, D, E, resp.), and

$$\begin{bmatrix} m_{j1} \\ m_{j2} \\ m_{j3} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ r_j & 0 & 1 - r_j \\ r_j^2 L_j^2 & 0 & (1 - r_j)^2 L_j^2 \end{bmatrix}^{-1} \begin{bmatrix} m_j \\ 0 \\ I_j \end{bmatrix}, \text{ for } j = 1, \dots, 4 \quad (23)$$

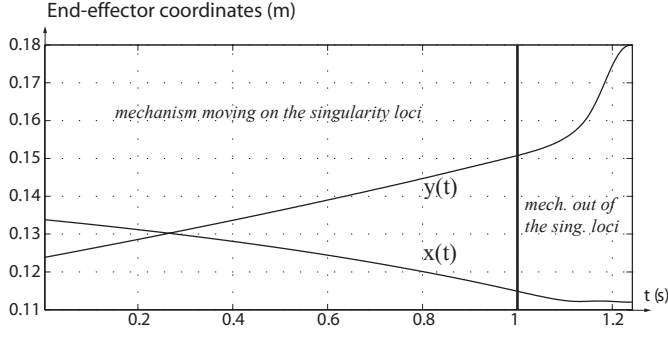
where  $m_j$  is the mass of the link  $j$  and  $I_j$  its axial moment of inertia expressed at the center of masses (for  $j = 1, \dots, 4$ ). For deeper explanations on the way to obtain these expressions, the reader is referred to [17].

In the following of the paper, the values of the geometric and inertial parameters of the robot are set to:

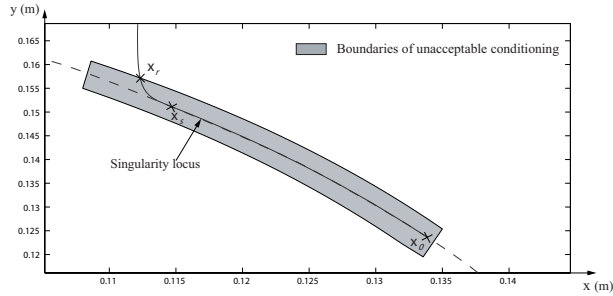
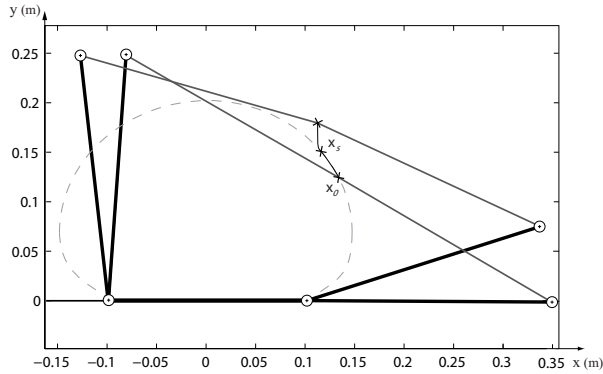
- $L_1 = L_2 = L_3 = L_4 = 0.25$  m and  $a = 0.2$  m
- $m_1 = m_4 = 2.81$  kg
- $m_2 = m_3 = 1.41$  kg
- $I_1 = I_4 = 0.02$  kg.m<sup>2</sup>
- $I_2 = I_3 = 0.01$  kg.m<sup>2</sup>

## 4.2 Moving a 5R mechanism out of a singular position

Let us now assume that the 5R mechanism is blocked on the singularity, such as represented in Fig. 4. In this example, the end-effector position is set at:  $\mathbf{x}_0 = [0.13m, 0.12m]^T$ .



**FIGURE 5. EVOLUTION OF THE END EFFECTOR COORDINATES ALONG THE EXIT TRAJECTORY**



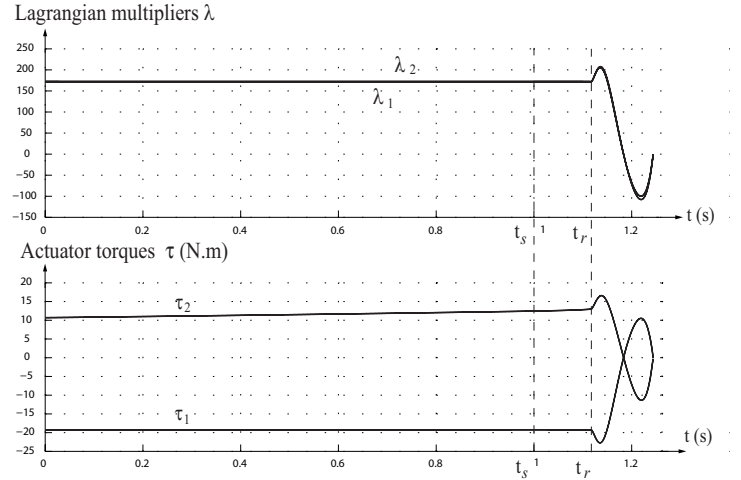
**FIGURE 6. EXIT TRAJECTORY OF THE 5R MECHANISM**

This section presents the calculation of the exit trajectory computed using the two methodologies.

#### 4.2.1 First Solution: generation of an optimal motion

##### Moving along the singularity locus

In order to move along the singularity, it has been shown in Section 3 that the two conditions (7) and (12) must be respected. For the studied robot, the vector  $\mathbf{t}_s$  that defined the uncontrollable twist of the robot in the Type 2



**FIGURE 7. TORQUES VALUES ON THE EXIT TRAJECTORY**

singularity is equal to  $[-\sin \psi, \cos \psi]^T$  [17], where

$$\psi = \tan^{-1} \left( \frac{y - L_1 \sin q_1}{x - L_1 \cos q_1 - a/2} \right) \quad (24)$$

Thus, condition (7) can be expressed as:

$$\begin{aligned} & -\sin \psi [m_{C_2} \ddot{x} - m_{C_1} L_1 (\ddot{q}_1 \sin q_1 + \dot{q}_1^2 \cos q_1) \\ & - m_{C_3} L_4 (\ddot{q}_2 \sin q_2 + \dot{q}_2^2 \cos q_2)] \\ & + \cos \psi [m_{C_2} \ddot{y} + m_{C_1} L_1 (\ddot{q}_1 \cos q_1 - \dot{q}_1^2 \sin q_1) \\ & + m_{C_3} L_4 (\ddot{q}_2 \cos q_2 - \dot{q}_2^2 \sin q_2)] = 0 \end{aligned} \quad (25)$$

in which the values of  $\dot{q}_i$  and  $\ddot{q}_i$  are expressed in (21).

Moreover, developing condition (12), it comes that:

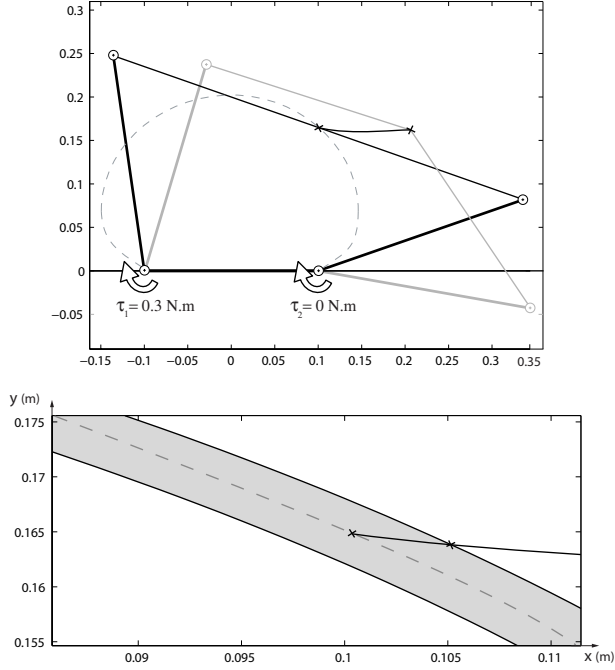
$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \mathbf{A}_x^{-1} \mathbf{A} \begin{bmatrix} \dot{\psi} \cos \psi \\ \dot{\psi} \sin \psi \end{bmatrix} \quad \text{where } \mathbf{A}_x = \mathbf{A}_x^d + \mathbf{A}_q^d \mathbf{A} \quad (26)$$

$$\mathbf{A}_x^d = \begin{bmatrix} -\sin \psi & \cos \psi \\ -\sin \psi & \cos \psi \end{bmatrix}, \quad \mathbf{A}_q^d = - \begin{bmatrix} L_1 \cos(\psi - q_1) & 0 \\ 0 & L_4 \cos(\psi - q_2) \end{bmatrix} \quad (27)$$

Starting with  $\dot{x} = -0.0127$  m/s and  $\dot{y} = 0.0124$  m/s, the non-linear differential equations are solved using Matlab toolboxes for a trajectory duration of 1 s. The resulting values are plotted in Fig. 5 for  $t \leq 1$  s.

After 1 s of motion, the mechanism is in the position  $\mathbf{x}_s = [0.11, 0.15]^T$  (Fig. 6), with a velocity of 0.26 m/s and





**FIGURE 8.** EXIT TRAJECTORY WITH THE SECOND ACTUATOR DECLUTCHED

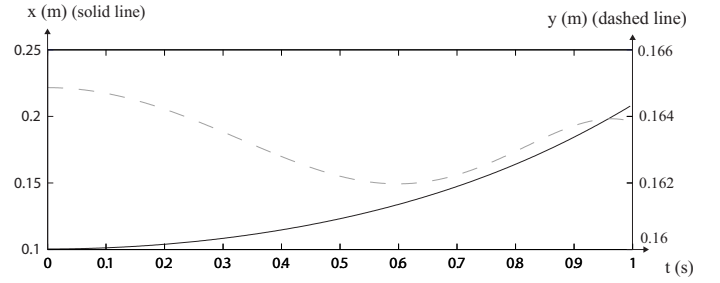
an acceleration of  $0.44 \text{ m/s}^2$ . To know in which workspace aspect the mechanism should exit, its free behavior is simulated, i.e. the actuators are virtually suppressed in simulation at  $t = 1\text{s}$ . In the studied case, the mechanism is spontaneously moving to workspace aspect numbered as the aspect 1 in the Fig. 6.

It can be demonstrated that the radius of curvature of the singularity locus at  $\mathbf{x}_s$  is equal to  $R_c = 0.137\text{m}$ , which permits to define the clothoid that can extend the exit trajectory after  $t = 1\text{s}$ . The values of the end-effector position when moving along the clothoid path are presented in Fig. 5 when  $t > 1\text{s}$ . The total trajectory in the workspace is shown in Fig. 6.

Using the methodology presented in section 3.1, the input torques are computed with a constant value for the Lagrange multiplier  $\lambda_2 = \lambda_2(X_r) = 1.72$  till the mechanism is on the singularity (or in the zone of bad conditioning of matrix  $\mathbf{A}$ ). The input torques values are shown in Fig. 7. It can be observed that the input torques are completely finite on the whole trajectory, even when moving on the singularity loci.

#### 4.2.2 Second Solution: Declutch one of the actuators

In this section the mechanism is stopped in the same singular position as in Section 4.2.1.



**FIGURE 9.** EVOLUTION OF THE END EFFECTOR COORDINATES ALONG THE DECLUTCHED TRAJECTORY

The second actuator is declutched and a constant torque equal to  $0.3 \text{ N.m}$  is applied on the first actuator. Using the equations defined in section 3.2, the mechanism displacement can be computed. After  $250 \text{ ms}$ , the mechanism is out of the area where the condition number of the matrix  $\mathbf{A}$  is superior to 100. Figure 8 represents the computed exit trajectory in the mechanism workspace. It can be shown that the mechanism exit the singularity in the workspace aspect number 1. The end effector coordinates along this trajectory are represented on Figure 9.

It could also be shown that by applying on motor 1 the opposite torque, the mechanism exit the singularity in the other workspace aspect (number 2). Based on the initial singular position, the input torques can be adjusted in order to move the mechanism in the desired assembly mode.

## 5 Conclusion

In order to increase the workspace size, past works have proved that a mechanism can cross the singularity loci by using an optimal motion planning. However, if the trajectory is not robust to modelling errors, the robot can stop in the singularity and stay blocked. Therefore, this paper proposes a new generic method dedicated to parallel manipulators in order to allow the exit from a Type 2 singularity. Based on the robot dynamic model, two strategies have been presented. The first one consists in a new algorithm dedicated to the computation of an optimal trajectory that allows the robot to exit the singularity. More precisely, the optimal trajectory is computed according to a specific dynamic criterion that ensures the consistency of the robot dynamic model all along the singularity loci. Then, the second trajectory is characterized by the declutching of one of the robot actuator in order to change the kinematic and dynamic behavior of the mechanism. Therefore, the under-actuated mechanism is no longer in a singular position, and its dynamic model is used to move away from the original mechanism Type 2 singularity.

Theoretical developments are illustrated, discussed and

analysed through advanced simulations achieved on a planar five-bar mechanism. Simulations results demonstrate that the proposed algorithms permit to exit the parallel manipulator from the singularity. Furthermore, the optimal trajectory planning guarantee that the mechanism input torques stay finite even when the mechanism is moving on a singularity.

Future works will be dedicated to the implementation of the proposed algorithms on a real five-bar mechanism that is currently being developed.

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