

# An image driven vision-based control framework for wheeled mobile robots

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**Abstract**—We deal in this paper with an original visual servoing method intended to control a nonholonomic wheeled mobile robot. These works are a part of a complete image-based framework for navigation of a mobile robot, using only a monocular vision system embedded on the robot. The navigation system uses a set of relay images to enable the robot to reach a goal configuration expressed as a desired attitude of visual landmarks in the image plane. This paper particularly focuses on a suitable image-based control law of a nonholonomic robot for navigating in image database, with the assumption that the ground is obstacle free. We show how computing a suitable homographic transformation between the current camera image and a desired one allows to estimate an error vector on the state of the robot relative to a virtual straight line. This line is joined and followed thanks to a control law designed according to a well suited chained system of the state of the robot. Simulations illustrate this point, and experimental results for a two wheels driven robot confirm the validity of our approach.

## I. INTRODUCTION

Navigation of a mobile robot includes many sub-tasks which are strongly dependent on each other. Given a global task of navigation, perception and control systems are used to make the robot succeed on it. From a perception module, with proprioceptive and/or exteroceptive sensors, a representation of the robot environment can be built, and it is then possible to locate the robot into this representation using the same perception system. This localisation allows to planify and generates adequate motions to achieve the specified task. Clearly, embedded sensors play a central role. Sonar and laser were the first sensors used for wheeled mobile robots navigation. More recently, the advent of fast and inexpensive digital imaging technology has allowed camera systems to be integrated as part of navigation systems. Given the advantages and shortcomings of each sensor, navigation approaches based on the fusion of observations provided by various sensors has been explored [3].

Computer vision can provide a powerful way of sensing the environment and controlling the robot motions. It is thus not surprising that more recent works have focused on the use of conventional or omnidirectional cameras as main sensors to navigate in partially or totally unknown environments. Indoor navigation tasks give a rise to a particular interest. Such workspaces are complex but well structured. Strong hypothesis such as parallelism of the floor and the ceiling or verticality of walls are generally respected. Such constraints are useful

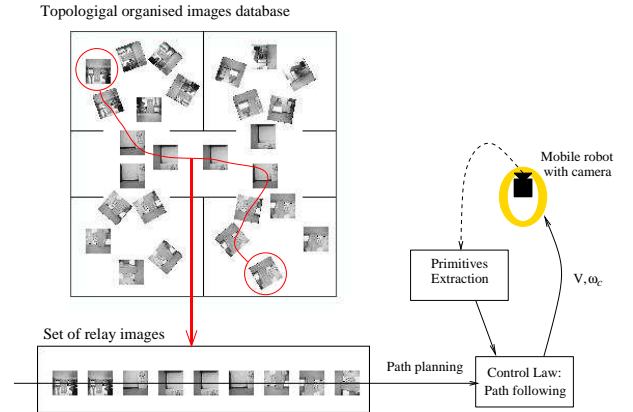


Fig. 1. Global strategy for indoor navigation

for 3D pose reconstruction methods, which allow the camera to be used as a global positioning system to locate the robot with respect to the observed environment. In order to obtain the 3D pose of the camera, several types of features can be used, such as straight lines [1] or rectangular patterns [8].

From the control point of view, this kind of localization systems is useful because it allows to use directly state feedback based control laws designed for nonholonomic robots [10], which are proved asymptotically stable. A learn or planned path can be replayed with a control law adapted to path following, as it is done in [16] with a CP-DGPS.

In our approach, the whole problem of navigation of a mobile robot is formulated in the camera image space, as described in [2] and represented by Fig.1. Given an image database describing the robot environment, the robot motions are controlled from its current position to a desired one, specified through a target image selected in the image database. The image database is obtained and indexed off-line during a supervised learning step, and constitutes a visual memory of the robot. The contents of this memory is thus a set of images which provide a representative sample of all the points of view which could be reached during the displacement phase. When the robot is let staying at an unspecified place of its workspace, we determine which image of the memory is the closest from the observed one. This can be done, as Remazeilles and al propose in [14], by comparing the photometric invariants of the

request image with those of the images of the visual memory. The task is specified as a target image to reach, chosen among the images of the database. A set of relay images describing a path from the current to the goal locations of the robot is then obtained thanks to the topological indexing of the database. The last step of this framework concerns the control scheme to bring an image of the given set to the next one and so on. This is the object of this paper.

The use of relay images to achieve large displacement positioning tasks is a promising approach. In [13], the authors propose a multi-images framework to control the 6 *dof* of a robotic arm. The stabilization to a point is reformulated as a trajectory following in the image space through key images. Tsakiris et al [17] have pointed out that image-based visual servoing techniques can be extended to nonholonomic mobile robots by adding degrees of freedom to the hand-eye system. The authors propose to embed the visual servoing control scheme in the task function formalism. Vision-based mobile robotic tasks such as wall following or self positioning with respect to landmarks is thus possible using this framework [9]. Control laws for specific tasks have been developed, as for path following, if these extra degrees of freedom are not available. These methods relies on the uncoupling of the lateral and longitudinal control. Yi Ma et al present in [11] a theoretical framework to regulate the orientation of a wheeled mobile robot with respect to a ground curve using a single camera, by expressing in the image a state vector extracted from optical flow. More recently, motivated by the development of 2D 1/2 visual-servoing method proposed by Malis et al (see [12]), some authors have investigated the use of homography estimation and epipolar geometry of the scene for visual-servoing of mobile robots.

In [6] and [5], a partial estimation of the camera displacement between the current and desired views is used to design control laws. The camera displacement is estimated by uncoupling translation and rotation components of an homography matrix. In [6], a time-varying control allows an asymptotic stabilisation on a desired image. In [5], a trajectory following task is achieved. The trajectory to follow is defined by a prerecorded video and the control law is proved stable using Lyapunov-based analysis.

In our case, as a difference with a whole video sequence, we deal with a set of relay images which have been acquired from geometrically spaced out point of view. As a consequence, we design an homography-based visual-servoing control law appropriated to large displacements, i.e where the initial error is large. The authors of [13] and [14] deal with this issue for a manipulator robot. Taking into account the nonholonomic constraints of wheeled mobile robots, we propose a suitable formulation of our problem as a path following, with the assumption that the evolution plane of the robot is obstacle free. We show that computing a suitable planar homography between the current image and the next relay one allows to design a path connecting these images. This path can then be followed using a suitable control law. We propose to uncouple guidance and longitudinal control thanks to a chained form

of the kinematics of the system. Leaving the longitudinal speed free allows more flexibility for the navigation task. In this paper, the evolved theory is illustrated in an indoor environment. However, other applications could be considered, as navigation of urban vehicles, which should move in a structured environment at low velocities.

The remainder of this paper is organized as follows. In Section II, the problem we address and the models used through the paper are described. The Section III is devoted to the control law design. As an example of the generic proposed framework, the particular case of indoor navigation with a camera looking at the ceiling is treated in Section IV. In Section V, simulation and experimental results which confirm the validity of the proposed approach are presented.

## II. PROBLEM FORMULATION AND MODELS

Throughout the paper, we consider a nonholonomic system with unicycle kinematics. Let  $\mathcal{F}_c$  and  $\mathcal{F}_m$  be the frames attached to the camera and to the mobile robot respectively and consider a plane  $\Pi$  on which is lying some natural or artificial landmarks. We note  $\mathcal{F}_c^*$  the desired frame corresponding to the camera pose from which a relay image  $\mathcal{I}^*$  was shot. Our aim is to bring  $\mathcal{F}_c$  to  $\mathcal{F}_c^*$  by moving the mobile robot along a nonholonomic path.

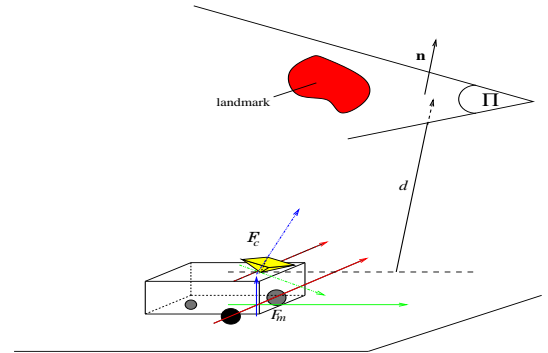


Fig. 2. Considered setup

### A. Geometric relations

The plane  $\Pi$  is supposed to contain some landmarks which can be tracked in the image  $\mathcal{I}$  and are identified in  $\mathcal{I}^*$ . Let  $\mathcal{P}$  be a set of points lying on one of these landmarks  $\mathcal{L}$  in  $\mathcal{I}$ , and  $\mathcal{P}^*$  the set of corresponding points in  $\mathcal{I}^*$ .  $\mathbf{p}_i = [u_i \ v_i \ 1]^\top$ , and  $\mathbf{p}_i^* = [u_i^* \ v_i^* \ 1]^\top$  denote the homogeneous coordinates in pixel of each point lying on  $\mathcal{P}$  and  $\mathcal{P}^*$  respectively.  $\mathbf{m}_i = [x_i \ y_i \ 1]^\top$  and  $\mathbf{m}_i^* = [x_i^* \ y_i^* \ 1]^\top$  are the corresponding homogeneous coordinates in meter. A projective homography matrix  $\mathbf{G}$  related to  $\Pi$  maps the points  $\mathbf{p}_i$  and  $\mathbf{p}_i^*$ :

$$\alpha \mathbf{p}_i = \mathbf{G} \mathbf{p}_i^* \quad (1)$$

where  $\alpha$  is a non zero scalar. If at least  $i \geq 4$ , it is well known that  $\mathbf{G}$  can be estimated by solving a linear system. In the remainder of this paper, the internal parameters matrix  $\mathbf{K}$  of the camera is assumed to be known. Then the Euclidean

homography can be computed up to a non zero scalar factor  $\alpha$ :

$$\alpha \mathbf{H} = \mathbf{K}^{-1} \mathbf{G} \mathbf{K} \quad (2)$$

Let us define  $\Pi$  in  $\mathcal{F}_c^*$  by  $\begin{bmatrix} \mathbf{n}^{*\top} & d^* \end{bmatrix}$  where  $d$  is a constant distance from  $\Pi$  to the origin of  $\mathcal{F}_c^*$ , and  $\mathbf{n}^{*\top}$  is the unitary normal vector to  $\Pi$  in  $\mathcal{F}_c$ . The Euclidean homography matrix  $\mathbf{H}$  can be decomposed into a rotation and a rank 1 matrix:

$$\mathbf{H} = \mathbf{R} + \mathbf{t} \frac{\mathbf{n}^{*\top}}{d^*} \quad (3)$$

$\mathbf{R}$  and  $\mathbf{t}$  are the rotation matrix and the translation vector that compose the homogeneous rigid transformation between  $\mathcal{F}_c$  and  $\mathcal{F}_c^*$ . Note that when  $\mathcal{F}_c$  is confounded with  $\mathcal{F}_c^*$ ,  $\mathbf{H}$  is proportional to the identity matrix. Finally, let us note that it is possible to compute the homography matrix in the more general case where at least the projection of eight 3D points are matched in  $\mathcal{I}$  and  $\mathcal{I}^*$ .

### B. Canonical camera configuration

First, consider that the camera frame  $\mathcal{F}_c$  is confounded with the control frame. In this configuration, which is named canonical in the sequel, the camera optical axis coincides with the rotation axis of the mobile robot and the camera optical center is the axle midpoint of the mobile robot. The camera frame and the mobile robot are thus subjected to the same kinematic nonholonomic constraints. Considering that the robot is moving on a perfect horizontal plane without any incidence on the image of the dynamics of the mechanical structure, what can be assumed if the robot moves enough slowly, the  $\mathbf{R}$  matrix is reduced to a simple rotation matrix around the optical axis, and  $\mathbf{t}$  has only two degrees of freedom on the ground plane. As exposed in [7], it is possible from  $\mathbf{H}$  to determine the camera motion parameters, it means the rotation  $\mathbf{R}$  and the scalar translation vector  $\frac{\mathbf{t}}{d^*}$ . The normal vector  $\mathbf{n}^*$  can also be determined, but the results are better if  $\mathbf{n}^*$  has been previously well estimated, as in the case of indoor navigation with a camera looking at the ceiling.

### C. General camera configuration

Of course, in real cases the camera frame  $\mathcal{F}_c$  often presents a 6 degrees of freedom rigid transformation with respect to the robot frame  $\mathcal{F}_m$ . However we will show that it is possible to come down to the simple configuration previously described where  $\mathcal{F}_c$  and  $\mathcal{F}_m$  are coincident (refer to II-B). Consider a virtual camera in the previously canonical camera configuration and let us note  $\mathcal{F}_v = \mathcal{F}_m$  a frame attached on it, and  $\mathcal{I}_v$  its image plane. Let  $\mathbf{R}_m$  and  $\mathbf{t}_m$  be the rotation matrix and the translation vector between  $\mathcal{F}_c$  and  $\mathcal{F}_v = \mathcal{F}_m$ . They are mechanically fixed and represent the hand-eye camera parameters. As exposed in section II-A, an homography related to  $\Pi$  ties up  $\mathcal{I}$  and  $\mathcal{I}_v$ . The points  $\mathbf{p}_i$  and  $\mathbf{p}_i^*$  can thus be projected in the virtual camera image through the constant homography  $\mathbf{H}_m$  from the knowledge of  $\mathbf{R}_m$ ,  $\mathbf{t}_m$  and  $\mathbf{n}^*$ . The problem of controlling the motions of the mobile robot using features extracted from the image of the real camera can thus be reformulated as the control of the virtual camera.

Therefore, in the remainder of this paper, we deal with the canonical configuration of the camera, where  $\mathcal{F}_c$  is in fact the frame  $\mathcal{F}_v$  above-mentioned.

## III. CONTROL LAW DESIGN

Our aim is to generate robot motion in order to superimpose  $\mathcal{I}$  and  $\mathcal{I}^*$ , what reverts to move  $\mathcal{F}_c$  to  $\mathcal{F}_c^*$  with respect to the unicycle-like nonholomic constraints assigned to  $\mathcal{F}_c$ . The kinematic screw of  $\mathcal{F}_c$  is assumed to consist only of a longitudinal speed  $V$  along the  $\mathbf{X}_c$  axis and a rotational velocity  $\omega_c$  around  $\mathbf{Z}_c$ .

### A. Design principle

In the previous section, we have seen that from the knowledge of matched points in a target image  $\mathcal{I}^*$  and the current image  $\mathcal{I}$ , the relative displacement between  $\mathcal{F}_c^*$  and  $\mathcal{F}_c$  can be extracted as a rotation matrix  $\mathbf{R}$  and a scaled translation vector  $\frac{\mathbf{t}}{d^*}$ . Since  $\mathbf{X}_c \mathbf{Y}_c$ -axis of  $\mathcal{F}_c$  and  $\mathcal{F}_c^*$  are supposed to span a plane parallel to the ground plane, an estimation of the angular deviation  $\theta$  between  $\mathcal{F}_c^*$  and  $\mathcal{F}_c$  can be directly extracted from  $\mathbf{R}$ . Consider a straight line  $\Gamma$ , parametrized according to the position  $\mathcal{F}_c^*$  and the  $\mathbf{Y}_c^*$  axis, as represented on Figure 3. We can get out from  $\frac{\mathbf{t}}{d^*}$  the lateral deviation  $y$  up to a scale factor between the origin of  $\mathcal{F}_c$  and a straight line  $\Gamma$ . As a consequence, the control problem can be formulated as following  $\Gamma$  in regulating to zero  $y$  and  $\theta$  before the origin of  $\mathcal{F}_c$  reaches the origin of  $\mathcal{F}_c^*$  (see Figure 3).

To achieve this control objective, chained systems properties are very interesting. A chained system results from a conversion of a mobile robot non linear model into an almost linear one [15]. As long as the robot longitudinal velocity  $V$  is non zero, the performances of path following can be determined in terms of settling distance [16]. In the considered cases, such a settling distance can be directly determined by the observed relative translations between  $\mathcal{F}_c^*$  and  $\mathcal{F}_c$  at the initial configuration. This property is exploited to ensure that  $\mathcal{I}$  and  $\mathcal{I}^*$  could be superimposed during the robot motion.

### B. Control law design

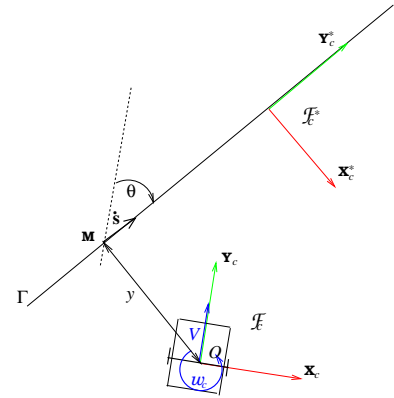


Fig. 3. Modelisation for control law design

In this part, a control law for straight line following is designed for cart-like vehicle moving on a perfect horizontal

plane under the conditions of pure rolling and non-slipping. Let us note  $\omega_v$  the cart angular velocity around the center of its rear axle. We also define the point  $\mathbf{M}$  as the orthogonal projection on  $\Gamma$  of the origin of  $\mathcal{F}_c$ . A curvilinear coordinate  $s$  is associated to  $\mathbf{M}$  on  $\Gamma$ . The state of the cart in its plane of evolution is given by  $\mathbf{X}_v = [s \ y \ \theta]^\top$  (refer to Figure 3). The cart control vector is  $\mathbf{U} = [V \ \omega_c]^\top$ . These two vectors are related by the following state space model:

$$\begin{cases} \dot{s} = V \cos \theta \\ \dot{y} = V \sin \theta \\ \dot{\theta} = \omega_c \end{cases} \quad (4)$$

Of course this state description is derivated from the more general case where the robot is following a geometric path (see [15], and [16] for an applicative example). Let us now convert the state space model (4) into a chained system of dimension 3  $[a_1 \ a_2 \ a_3]^\top$  with a 2 dimensional control vector  $[m_1 \ m_2]^\top$ . The derivative of such a chained form with respect to time is:

$$\begin{cases} \dot{a}_1 = m_1 \\ \dot{a}_2 = a_3 m_1 \\ \dot{a}_3 = m_2 \end{cases} \quad (5)$$

The almost linearity of this system is then viewable when the chained system is derivated with respect to  $a_1$ , with  $m_3 = \frac{m_2}{m_1}$ :

$$\begin{cases} a_1' = 1 \\ a_2' = a_3 \\ a_3' = m_3 \end{cases} \quad (6)$$

Choosing  $a_1 = s$ , the linear system (6) is independent from  $V$ , since it is driven by a variable homogeneous to the distance covered by the robot. The input variable  $m_1$  is given by (refer to equations (4) and (5)):

$$m_1 = \dot{s} = V \cos \theta \quad (7)$$

Let us now define  $a_2 = y$ . Then it comes:

$$\dot{a}_2 = V \sin \theta = a_3 m_1 \quad (8)$$

Therefore  $a_3$  must be chosen as:

$$a_3 = \tan \theta \quad (9)$$

Consequently,  $a_3$  is not defined for  $\theta = \frac{\pi}{2} [\pi]$ . In the general case of geometric path following, this condition is avoided by planning an appropriate path to follow. In our application, this can be avoided by choosing judiciously the relay images during the off-line learning step.

Finally, we deduce  $m_2$  from  $m_2 = \dot{a}_3$ :

$$m_2 = \frac{\omega_c}{\cos^2 \theta} \quad (10)$$

Thanks to the linearity of the chained system (6), a natural and simple expression for the control law is:

$$m_3 = -K_d a_3 - K_p a_2 \quad (K_p, K_d) \in \mathbb{R}^{+2} \quad (11)$$

This last relation combined to (6) leads to:

$$a_2'' + K_d a_2' + K_p a_2 = 0 \quad (12)$$

Consequently, both  $a_2$  and  $a_3$  converge to zero, independently of the longitudinal velocity of the robot as long as  $V \neq 0$ . In view of  $a_2 = y$  and  $a_3 = \tan \theta$ , (11) ensures that both  $y$  and  $\theta$  converge to zero. Taking into account that  $V$  can be negative, the expression of  $m_2 = m_3 m_1$  can be obtained from (11) and it is given by:

$$m_2 = -|m_1| K_d a_3 - m_1 K_p a_2 \quad (13)$$

Therefore,  $\omega_c$  is extracted from (10) in which (13) is inserted:

$$\omega_c(y, \theta) = -V \cos^3 \theta K_p y - |V \cos^3 \theta| K_d \tan \theta \quad (14)$$

The expression of the control vector  $\mathbf{U} = [V \ \omega_c]^\top$  can thus be computed. The guidance control law given by equation (14) has been designed independently of the longitudinal speed  $V$ . As highlighted with equation (11), only  $K_p$  and  $K_d$  theoretically set the performances of the control law. Then  $V$  can be set to a constant value during all the motion or be time-varying, seeing that  $V$  has to be non-zero.

The chained form consists in a double integrator (refer to (6)) and then the asymptotic stability of the control law (14) is guaranteed. In practice, the success of this control law relies on the gains  $K_p$  and  $K_d$ . Indeed,  $K_p$  and  $K_d$  determine the dynamics of the second order system (12), i.e the impulse response of  $y$  with respect to the covered distance by the point  $\mathbf{M}$  on  $\Gamma$ . An appropriate settling distance  $s_r$  for the system (12) can be set to a typical one for the considered application. The convergence of  $y$  and  $\theta$  to zero before  $\mathcal{F}_c$  reaches the desired attitude  $\mathcal{F}_c^*$  should be ensured if the settling distance is chosen smaller than the distance between two shots of two consecutive images of the database.

#### IV. APPLICATION TO INDOOR NAVIGATION

Indoor environments abound in planes. Thus our framework should be well adapted to this kind of workspace. In this section, we address the particular application where  $\Pi$  is the ceiling, supposed to be parallel to the ground plane. In this case, the unitary normal vector  $\mathbf{n}^*$  to  $\Pi$  expressed in the canonical camera frame at a goal point of view  $\mathcal{F}_c^*$  is known to be  $\mathbf{n}^{*\top} = [0 \ 0 \ 1]$ . The Euclidean homography matrix  $\mathbf{H}$  has thus a very simple expression (refer to equation (3)). Indeed, as the displacement between  $\mathcal{F}_c^*$  and  $\mathcal{F}_c$  only consists of one rotation  $\theta \mathbf{Z}_c$  and two translations  $t_{X_c} \mathbf{X}_c$  and  $t_{Y_c} \mathbf{Y}_c$ ,  $\mathbf{H}$  is given by (refer to equation (3)):

$$\mathbf{H} = \begin{bmatrix} \cos \theta & -\sin \theta & t_{X_c} \\ \sin \theta & \cos \theta & t_{Y_c} \\ 0 & 0 & 1 \end{bmatrix} \quad (15)$$

Therefore,  $\mathbf{H}$  has only three degrees of freedom. Only two points lying on  $\Pi$  and matched in  $\mathcal{I}^*$  and  $\mathcal{I}$  are theoretically necessary to estimate  $\mathbf{H}$ . From the computation of  $\mathbf{H}$ , one can extract directly  $\theta$  which is the angular deviation with respect to  $\Gamma$  introduced in section III. The lateral deviation  $y$  can also be estimated since it is the  $\mathbf{X}_c^*$  coordinate of the origin of  $\mathcal{F}_c$ :

$$y = -t_{X_c} \cos \theta - t_{Y_c} \sin \theta \quad (16)$$

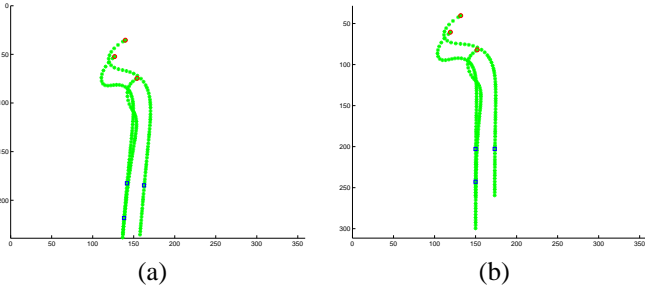


Fig. 4. Visual features trajectories: (a) in the real camera image, (b) in the virtual camera image. Rounds are the initial features, squares are the desired ones.

Thus, from the computation of the Euclidean homography  $\mathbf{H}$ , the state of  $\mathcal{F}_c$  with respect to the straight line  $\Gamma$  can easily be determined. The guidance control law designed in section III for a nonholonomic vehicle is then supplied. The next section illustrate and validate our approach with simulations and experimental results.

## V. RESULTS

The proposed approach has been first tested in a simulation environment. In these simulations, both the vision system and the robotic platform are assumed to be time-continuous, with a view to validating our approach from a theoretical point of view. The robotic task consists of moving the robot to a certain pose with respect to features in the desired image. The camera is embedded on the mobile robot and its optical center is positioned vertically with respect to the rear axle midpoint. A tilt angle of  $0.1\text{rad}$  and a pan one of  $0.01\text{rad}$  are introduced between the optical axis and the vertical axis of the frame attached to the mobile robot. The coordinates of the camera optical center with respect to  $\mathcal{F}_m$  are  $0.01m$ ,  $0.01m$  and  $0.1m$  along  $\mathbf{X}_m$ ,  $\mathbf{Y}_m$  and  $\mathbf{Z}_m$  respectively. The camera is looking at three points. The control law presented in Section III is used to control the mobile robot. Figure 4 presents the visual features trajectories in the image plane: (a) curves are plotted in the real image plane, (b) curves are plotted in the virtual image plane.

We first note that the paths described by the features converge to the desired positions. As can be shown in the Figure 5, the corresponding camera path confirms the validity of the control law. We can also notice that the mobile robot joins a straight line in the ground plane before passing through its desired attitude. As shown in Figure 6 (a) and (b), angular and lateral deviations of the robot are well regulated to zero. When the straight line is joined, the mobile robot stops rotating and follows straightly the path (Figure 6 (c)). However, we state that the mobile robot runs with a constant value of longitudinal velocity and it is not stopped-dead on the desired configuration. This is an inherent issue to the chained systems, which impose  $V \neq 0$ . That explains why the error in image points coordinates increases after having converged to zero (See Figure 6 (d)). Nevertheless, we do not mind this point when the reached configuration corresponds to a relay image. It is more cumbersome for the last step of stabilisation on the

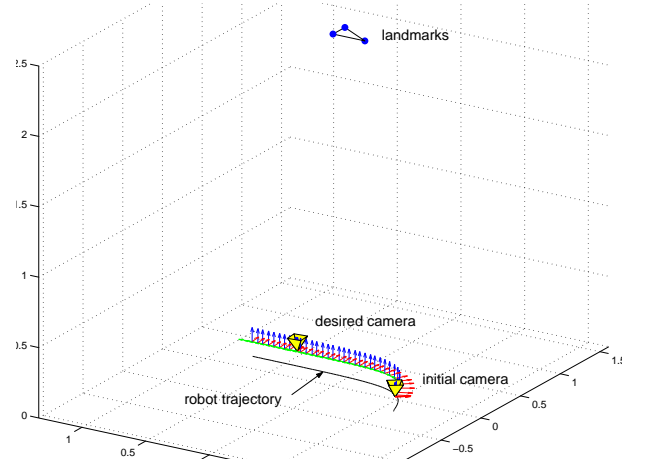


Fig. 5. 3D trajectory of the camera

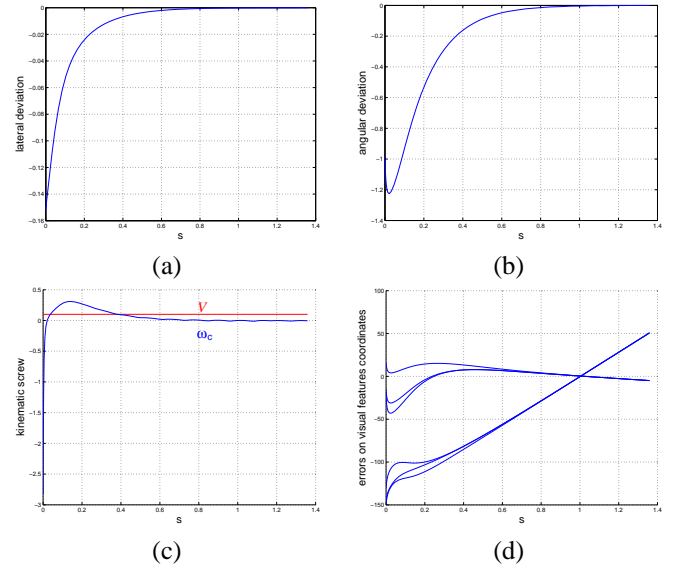


Fig. 6. Signals with respect to  $s$ : (a) lateral deviation ( $m$ ), (b) angular deviation ( $rad$ ), (c) mobile robot kinematic screw ( $V$  in  $m.sec^{-1}$ ,  $\omega_c$  in  $rad.sec^{-1}$ ), (d) behavior of the landmark points coordinates relatively to their desired position ( $m$ )

goal image. Indeed, we ought to have an open loop step to stop the robot, what can not ensures an accurate final pose. In view of these results, the proposed approach has been tested on a Pekee<sup>TM</sup> robot from Wany Robotics. A  $1/3''$  CMOS embedded camera is turned to the ceiling and is approximatively placed on the canonical configuration exposed in subsection II-B. Only a motors speed regulation runs on the main electronic card of the robot. The whole application, from image acquisition to the control law computation, is processed at the rate of  $25\text{Hz}$  on a external  $1.8\text{GHz}$  PC. Thanks to a robust tracking based on particular filter (see [4]), a set of four points lying on the ceiling is available at each image acquisition. The desired positions of these points are extracted from the relay image to reach. The two wheels driven robot is modeled as a unicycle. The length of the total displacement done on the ground plane is about  $1.5m$ . The real initial



3D angular and lateral deviations, with respect to the desired attitude of the robot are respectively  $0.5rad$  and  $0.6m$ . The control gains  $Kp$  and  $Kd$  have been chosen for a settling distance of  $0.7m$  (refer to equation (11)).

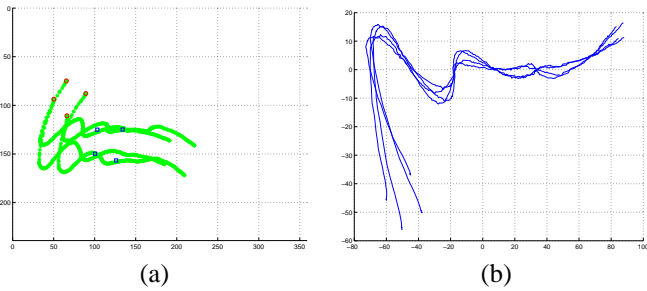


Fig. 7. (a) Tracked points trajectories in the image. Rounds are the initial features, squares are the desired ones. (b) behavior of the tracked points coordinates relatively to their desired position.

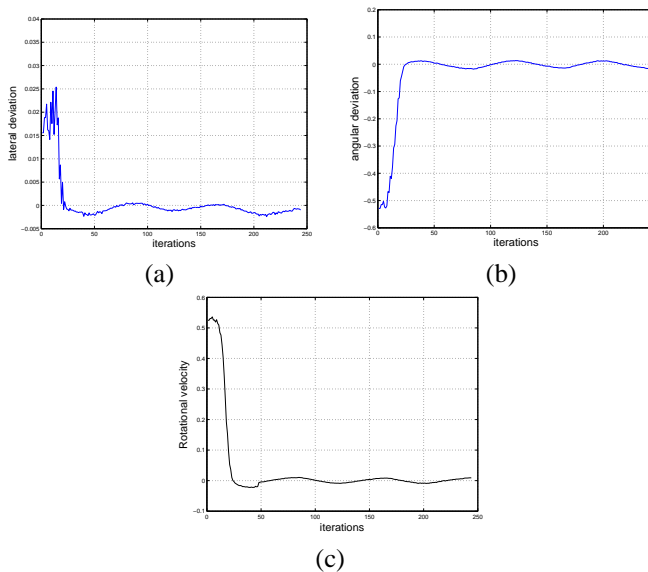


Fig. 8. Errors measures: (a) Lateral deviation  $y$ , (b) Angular deviation  $\theta$ ; (c) Rotation speed order to the robot.

The Figure 7(a) shows that the control law has prevailed the task on its objective. The tracked points reach their desired positions in the image plane, and then they follow a straight line. The Figure 7(b) confirms the good behavior of the visual features. As illustrated by Figures 8(a) and 8(b), lateral and angular deviations are regulated to zero, and the rotational velocity of the robot tends to be null (refer to Figure 8(c)). We observe very small oscillations around the desired state of the robot due to the robot internal control loop on velocities. However, they do not disturb the global task of path following, which objective is reached.

## VI. CONCLUSION AND FUTURE WORKS

Our works deal with the topic of wheeled mobile robots navigation, using only one embedded camera. Given an ordered set of relay images, we aim to move the camera from a relay image to the next one, and so on until the desired

image. In this paper, we have more especially addressed the problem of controlling the robot in order to bring an initial image to a desired one. The presented vision-based control law consists on the computation of an Euclidean homography between the current image and the desired one, from which we extract an error vector on the state of the mobile robot with respect to an adequately chosen straight line. The control law objective is thus formulated as a straight line following. However, the controller is designed so that the line is joined before reaching the desired relay image. We have validated our framework through simulations and experimental results on a Peekee<sup>TM</sup> robot. Future works will be devoted to the analysis of relay images switching, keeping the velocities continuous.

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