Differentiating a Time-dependent CFD Solver

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Introduction

- Aim: Tangent and Adjoint of a numerical code simulating a 2D model of a synthetic jet actuator.
- Synthetic jet actuators [GWP+03] Synthetic jet actuators are small scale devices generating a jet-like motion by oscillating fluid in a chamber connected to the air flow via an orifice.
- Possible Applications
 - Embed into aircraft wing to control flow separation
 - Propulsion system for microfluid systems

Synthetic Jet



Mesh Movement Algorithm

- Time-dependent Navier-Stokes eqn.s on a moving mesh.
- Mesh movement for interior point $\mathbf{x}_i^{new} = \mathbf{x}_i + \Delta \mathbf{x}_i$ governed by forced boundary motion smoothed into interior mesh,

$$\Delta \mathbf{x}_{i} = \frac{1}{D_{i}} \sum_{j \in \mathsf{Nbr}(i)} \frac{1}{|\mathbf{x}_{i} - \mathbf{x}_{j}|} \Delta \mathbf{x}_{j}, \text{ with } D_{i} = \sum_{j \in \mathsf{Nbr}(i)} \frac{1}{|\mathbf{x}_{i} - \mathbf{x}_{j}|},$$

repeated 50 times - Gauss-Seidel smoothing/linear solve.

The Time-Dependent CFD Solver

Finite-volume semi-discretisation of N-S equations for cell i,

$$\frac{\partial V_i \mathbf{q}_i}{\partial t} = \mathbf{R}_i(\mathbf{q}, \mathbf{x}).$$

Backward Euler gives nonlinear system for q^{n+1} .

$$\frac{V_i^{n+1}\mathbf{q}_i^{n+1} - V_i^n \mathbf{q}_i^n}{\Delta t} = \mathbf{R}_i(\mathbf{q}_i^{n+1}, \mathbf{x}^n)$$
$$0 = \mathbf{R}_i(\mathbf{q}_i^{n+1}, \mathbf{x}^n) - \frac{V_i^{n+1}\mathbf{q}_i^{n+1} - V_i^n \mathbf{q}_i^n}{\Delta t}$$

Introduce pseudo-timestepping with pseudo-time τ ,

$$V_i^{n+1} \frac{\partial \mathbf{q}_i^{n+1}}{\partial \tau} = \mathbf{R}_i(\mathbf{q}_i^{n+1}, \mathbf{x}^n) - \frac{V_i^{n+1} \mathbf{q}_i^{n+1} - V_i^n \mathbf{q}_i^n}{\Delta t}.$$

Iterate to convergence using low-storage 4-stage Runge-Kutta scheme.

Schema of the Numerical Code

```
Read in mesh geometry X (nodes, cells, faces)
Initialise flow variables and boundary conditions
Read in design variables designvars: a, p
Read in number of time-steps N and celopt
Set F=0
For i from 0 to N
 Move the mesh boundary using a sin scheme a\sin(pX+\phi)
 Update interior mesh then cell and face information
 While (not converged) ! FIXPOINT
  Converge the flow variables using a RK4 solve:
   Compute residual R = r(Q, j) for each cell j
   Update the flow variables Q using R
 End While
Update F = F + \sum_{i=2,3} Q(i, celopt)^2
EndDo
```

Fortran 95 Features of the code

- The input code (4500 loc) uses dynamic allocation, modules, derived types and array operations
- A derived type example

```
type bound_type !define the boundary structure
integer(2)::uns !unsteady flag
integer(2)::dim !dimensional or not(1=Yes)
integer(2)::var !
real(8), allocatable::bQ(:,:)!primitive Q
character::TP*80 !type,
character*32::extra(2)!store extra information.
end type bound_type
```

Fortran 95 Features of the code

A Module Example

```
module mesh info
 use prop
 • • •
 integer(4)::nodenum ! number of nodes
 integer(4)::cellnum ! number of cells
 integer(4)::facenum ! number of faces
 integer(2)::nthread ! number of threads
 type(node_type), allocatable::node(:) !node set
 type(cell_type), allocatable::cell(:) !cell set
 type(face_type), allocatable::face(:) !face set
 type(thre_type), allocatable::thre(:) !thread set
end module mesh info
```

To differentiate this CFD solver, we used the AD tools TAF and TAPENADE.

Code Preparation

- TAF forward worked and gave consistent results with FD.
- TAF generated adjoint used to blow up at runtime (?)
- To further investigate the adjoint, we cleaned up the original code by using a sed script:
 - real(8) \rightarrow double precision (Portability)
 - integer(4) \rightarrow integer
 - Dynamic Allocation \longrightarrow Static Allocation
 - $\ \ \, \bullet \ \ \, Module \longrightarrow Common \ \ \, Block$
 - Derived Type \longrightarrow set of arrays

First Results

- Mesh size: 654 nodes, 582 cells, 1235 faces
- 2 independents (period & amplitude) and 1 dependent (kinetic energy per cell volume = 572.0564 for this run).

Method	Grac	# Sig. F	
TAF(fwd)	-3230806.74033	54833.2739837	11
TAF(rev)	-2990768.62366	51687.4932185	1
TAPENADE(fwd)	-3230806.74031	54833.2739834	11
Tapenade(rev)	-3230806.74033	54833.2739835	11

DEBUG: Can AD tools adopt optimisation options as compilers do?

Potential Debug Problem

Consider an array partially overwritten [Ralf Giering]

```
subroutine incompletarray(bval,ff,nx,ny)
double precision::ff(nx,ny), ... !declarations
ff = 2.d0
```

call boundary(bval,ff,nx,ny)!partially overwrites ff
end subroutine incompletarray

By default, TAF adjoint code will look as follows:

```
subroutine adincompletarray(bval,adbval,ff,adff,nx,ny
```

```
! declarations
call boundary (bval,ff,nx,ny)
!Recomputation of ff is wrong
call adboundary(adbval,adff,nx,ny)
end subroutine adincompletarray
```

TAF assumes boundary completely overwrites ff so recomputation algorithm omits ff=2.d0 line and ff has incorrect value.

Some Observations

- TAF adjoint, by default uses a recomputation strategy but provides a fair tradeoff off between storage/recomputation via directives.
- TAPENADE adjoint provides a recursive checkpointing strategy performed at subroutine levels to tradeoff off between storage and recomputation.
- TAPENADE's Stack may be insufficient in terms of memory requirement.
- We have coded Fortran 95 taping routines with RAM buffer (module array) and local disk files using direct access.

Exploiting Code Insights

Fixed Point Iteration (Rule 22 of [Gri00, p. 299]): Fixed point iterations can and should be adjoined by recording only single steps.

Method	$CPU(\nabla F)$ (s)	Tape_size	$\frac{CPU(\nabla F)}{CPU(F)}$
TAPENADE(fwd)	69		3.8
Tapenade(rev)	7755	1.585 GB	484.6
TAPENADE(rev,FP)	5751	0.182 GB	319.5
TAPENADE(rev, FP, Par.)	5715	0.180 GB	317.5

• The gradient $\nabla F = \begin{bmatrix} -3230835.9523 & 54833.2466 \end{bmatrix}$ (using the same number of iterations as for the forward pass) is up to 6 significant digits as compared to the gradient using the mechanical adjoining used by TAPENADE.

Optimisation

- Start Jet Animation
- Given a fixed amount of work $C(\mathbf{x})$ that the system cannot exceed, the objective is to maximise the kinetic energy $F(\mathbf{x})$ from a nominated cell in the upwards movement of the jet.

$$\begin{aligned} \max_{\mathbf{x}} F(\mathbf{x}) \\ C(\mathbf{x}) &\leq 1 \\ 10^{-3} &\leq p \leq 10^{-1} & \text{!p is the period} \\ 10^{-2} &\leq a \leq 10^{-1} & \text{!a is the amplitude} \end{aligned}$$

	Initial Guess		Optimun		
Method	Period	Ampl.	Period	Ampl.	Iter.
FMINCON	1.D-2	1.D-2	0.46D-2	0.45D-1	15
FMINCON(AD)	1.D-2	1.D-2	1.54D-2	1.05D-1	11

Velocity Profile at Convergence



On the Left [Right] is represented the upstream velocity profile of the jet before [after] the optimisation.

Concluding Remarks

- AD Adjoint mode performs better for applications with fairly large number of independents.
- For a given constraint, it is possible to choose the frequency and the amplitude of the fluid oscillation so as to maximise the kinetic energy of the jet's upwards movement.
- Improvements for the adjoint calculation (Fixpoint Iteration, Parallel Loops [HFH01]).
- Increase the number of the design variables in order to make the generated adjoint competitive.
- Run the adjoint for a finer mesh with (big number of nodes e.g., 20,000).
- It is safer to compile and run the original code on different platforms prior to differentiation!

References

References

- [Gri00] Andreas Griewank. *Evaluating Derivatives: Principles and Techniques of Algorithmic Differentiation*. Number 19 in Frontiers in Appl. Math. SIAM, Philadelphia, Penn., 2000.
- [GWP⁺03] Quentin Gallas, Guiquin Wang, Melih Papila, Mark Sheplak, and Louis Cattafesta. Optimization of synthetic jet actuators. *AIAA paper*, (0635), 2003.
- [HFH01] Laurent Hascoët, Stefka Fidanova, and Christophe Held. Adjoining independent computations. In George Corliss, Christèle Faure, Andreas Griewank, Laurent Hascoët, and Uwe Naumann, editors, *Automatic Differentiation: From Simulation to Optimization*, Computer and Information Science, chapter 35, pages 285–290. Springer, New York, 2001.