

Numerical approaches to singularity analysis, singularity index and new concepts J-P. Merlet





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• an algebraic approach to singularity analysis





You have already seen:

- an algebraic approach to singularity analysis
- a geometrical approach to singularity analysis









• a numerical approach of singularity analysis





- a numerical approach of singularity analysis
- what should not be used as "distance" to singularity





- a numerical approach of singularity analysis
- what should not be used as "distance" to singularity
- another approach to singularity analysis

want to see a motion from one solution of the forward kinematics to another one without singularity crossing ?









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- a function f(x)
- interval evaluation of f when $x \in \mathcal{X}$: a range $[\underline{F},\overline{F}]$ such that

$$\forall x \in \mathcal{X} \text{ we have } : \underline{F} \leq f(x) \leq \overline{F}$$





How to construct an interval evaluation ? the simplest one is the natural evaluation:

substitute each mathematical operator by its interval equivalent





Example: $F = x^2 + \cos(x)$, $x \in [0, 1]$ **Problem: find** [A, B] such that: $A \leq F(x) \leq B \forall x \in [0, 1]$





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- 0 not included in [0.54,2] $\Rightarrow F \neq 0 \forall x \in [0,1]$
- $F > 0 \quad \forall \ x \in [0, 1]$
- $\forall x \in [0, 1]$ we have $0.54 \le F \le 2$ (global optimization)





$$F = [0,1]^2 + \cos([0,1]) = [0,1]+[0.54,1] = [0.54,2]$$

We have calculated an interval evaluation of F for the range [0,1]





Properties





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• can be implemented to take into account round-off errors



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- can be implemented to take into account round-off errors
- Overestimation of $\underline{F}, \overline{F}$ but decreases with the size of the ranges





A crucial problem for parallel robot: no singularity in a given workspace \mathcal{W}







- τ : force/torque in the actuated joints
- \mathcal{F} : external forces/torques applied on the platform





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Mechanical equilibrium: $\mathcal{F}=\mathbf{J}(\mathbf{X},\mathbf{P})\tau$ linear system in τ

$$\tau_i = \frac{|\dots|}{|\mathbf{J}|}$$

if $|\mathbf{J}| \to 0$ possibly $\tau_i \to \infty$





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then any path from $\mathbf{M_1}$ to $\mathbf{M_2}$ crosses a singularity

 \downarrow





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 ${\cal W}$ includes a singularity

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- minor expansion
- Gaussian elimination





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Ingredients of the algorithm:

- a box: a set of ranges for $x, y, z, \psi, \theta, \phi$
- a list S = {B₁, B₂, ...} of boxes. Initially S = {W} but boxes will be added
- an *index* i to indicate which box in S is processed





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- 3. $\overline{F} < 0$: for all **x** in B_i negative determinant, SINGULARITY
- 4. $\underline{F} < 0, \overline{F} > 0$: split the box in two, add the 2 new boxes at the end of the list, i = i + 1, goto 1





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Extremal matrices: all scalar matrices with as elements either the lower or upper bound of the corresponding elements in J





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Rohn test can be used as a filter









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• \pm 0.1 uncertainties on the location of the anchor points: |5155



meaning that ALL robots in this family are singularity-free









How can can we define a singularity index ?





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• that is invariant with units choice





How can can we define a singularity index ?

- that is invariant with units choice
- that has a physical meaning









Classical indices rely on the jacobian of the robot





Example: manipulability ellipsoid







possible accuracy index I: σ_{max}





In fact $\Delta \Theta$ bounded means: $|\Delta \Theta_i| \leq 1$

- each $\Delta \Theta_i$ is independent
- the possible region for $\Delta \Theta$ is a square
- the linear mapping induced by J⁻¹ transforms this square into a tilted rectangle





• σ_{max} is not the maximal positioning error





Another example: condition number





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$$\mathbf{J^{-1}}(\mathbf{X})\mathbf{\Delta X} = \mathbf{\Delta \Theta}$$

$$\frac{||\Delta \mathbf{X}||}{||\mathbf{X}||} \le ||\mathbf{J}^{-1}||||\mathbf{J}||\frac{||\Delta \Theta||}{||\Theta||}$$

condition number κ : $||\mathbf{J}^{-1}||||\mathbf{J}|| \Rightarrow$ relative amplification factor





Condition number:

- local index
- has usually no closed-form
- value changes with the norm choice
- usual norms: 2-norm, Frobenius norm $\Rightarrow \kappa \in [1,\infty]$
- $1/\kappa$ often used, $1/\kappa \in [0,1]$, 0 at a singularity
- meaning when the robot has both translation and orientation d.o.f. ?





Validity of the condition number Xľ V Ζ V X

3 reference poses P_1, P_2, P_3

 $\left|\Delta\Theta^a\right| \le 1$

$$\Delta X_{x,y,z,\theta_x,\theta_y,\theta_z} = \sum_{k=1}^{k=6} |J_{x,y,z,\theta_x,\theta_y,\theta_z}^k|$$

ranking according to accuracy: $P_1 \gg P_2 > P_3$








Not really consistent with accuracy ranking !



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Global conditioning indices

To characterize the dexterity over a given workspace \boldsymbol{W}

$$GCI = \frac{\int_{W} \left(\frac{1}{\kappa} \right) dW}{\int_{W} dW}$$

Problem: how to compute it ?





- sample each W axis, step $l \to m$ poses, GCI = $\frac{\sum \kappa_i}{m}$,
- computation time: $O(l^6)$, error ?
- assumption: if $\frac{\operatorname{GCI}(m+50) \operatorname{GCI}(m)}{\operatorname{GCI}(m+50)} \leq 0.5\%$, then $\frac{|\operatorname{GCI} \operatorname{GCI}(m+50)|}{\operatorname{GCI}} \leq 0.5\%$ wrong!





Counter example: planar 2R robot



condition number only function of θ_2 :

GCI can be calculated exactly

 $\frac{{\rm GCI}(60)-{\rm GCI}(50)}{{\rm GCI}(60)}=0.3768\%$ while

$$rac{|\text{GCI}-\text{GCI}(60)|}{\text{GCI}} = 1.7514\%$$









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Hence we have to consider also the vicinity of a singularity





• we define a maximal force/torque τ_{max} for the kinematic chains





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closeness is unit invariant, has a physical meaning



Static workspace









Static workspace: location of the EE such that $d \ge 0$



Static workspace



Static workspace: location of the EE such that $d \ge 0$ \downarrow no breakdown of the mechanism







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How can we compute the static workspace ?



Static workspace



Static workspace: location of the EE such that $d \ge 0$

How can we compute the static workspace ?

- for a given load
- for a set of loads









- for a 2 dof robot
- for a given load





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we can calculate in closed-form part of analytic curves that will be part of the border of the static workspace

















- for a *n* dof robot
- for a set of loads
- with uncertainties on the robot's geometry





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Interval analysis algorithm allows to obtain an accurate approximation of the static workspace





Example: cross-section of a 6D static workspace







Conclusion

- checking if a singularity is present in a given workspace is feasible efficiently
- just forget about so-called singularity, dexterity indices
- the best singularity index is the one that will prohibit your robot to do its job

