

Recursive maximum likelihood estimation for structural health monitoring: tangent filter implementations

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Abstract—Flutter monitoring can be handled by tracking the real time variations of the modal parameters of a specified civil structure, be it a bridge or an aircraft. Previous algorithmic attempts encompass automated batch identification and damage detection through hypothesis testing. Both approaches appear impractical, the first one because of computational time considerations and the difficulty to select a windows length with the best trade off between bias and variance, the second because of the difficulty to obtain reference data set close to flutter regime. Here, we investigate the capabilities of a sample wise recursive linear Kalman filter coupled with a tangent filter. We also consider the nonlinear case.

I. INTRODUCTION

A critical problem for mechanical structures exposed to unmeasured non stationary natural excitation (turbulence) is an instability phenomenon also known as *flutter*. It is formulated as the monitoring of the time varying complex eigenvalues associated to the discretized linear system corresponding to the monitored mechanical system. It has already been investigated through batch identification modal analysis using only output-only in-flight data has already been investigated. See Mevel *et al* [1] for a case study of monitored aircraft using subspace identification methods.

For improving the estimation of the parameters of interest, the collection of frequency and damping coefficients, and moreover for achieving this in real-time during flight tests, one possible route is to resort to tracking algorithms.

Frequency and damping coefficients are monitored by a recursive maximum likelihood (RML) procedure. The considered tracking procedure is a special case of adaptive algorithms where the gain is kept constant. The associated score function is evaluated by a joint Kalman filter and its derivative w.r.t. to the parameters (the tangent filter). In the nonlinear case, these filters can be approximated by particle filtering techniques [2]. Doucet & Tadić [3], and Guyader *et al* [4] already applied these techniques to RML estimation. The problem presented here was previously treated by Fichou *et al* [5] in a simpler framework.

Particle approximation for health monitoring was already proposed by Yoshida & Sato [6] in order to handle non-Gaussian noise. Modal characteristics monitoring is also considered by Ching *et al* [7]. In both cases authors use a state augmentation approach by including the unknown parameters in the state process. It seems preferable to directly identify these parameters by a likelihood approach.

In a first part the structural health monitoring problem is written in term of recursive maximum likelihood estimate (RMLE) in a state-space model. Then a Kalman filter expression of the score function is proposed together with an alternate particle filter approximation. Last part is devoted to a case study.

II. THE PROBLEM

A. Dynamical model and structural parameters

Let us consider observations sampled at a rate $1/\delta$

$$y_k = \mathbf{L} Z(k\delta) \quad (1)$$

of the state $Z(t)$ of a n -degrees of freedom mechanical system. These measurements are gathered through d sensors, i.e. y_k takes values in \mathbb{R}^d . The matrix \mathbf{L} indicates which components of the state vector are actually measured, i.e. where the sensors are located. The behavior of the mechanical system is described by

$$\mathbf{M} \ddot{Z}(t) + \mathbf{C} \dot{Z}(t) + \mathbf{K} Z(t) = \sigma \zeta(t) \quad (2)$$

where the (non measured) input force ζ is a non-stationary white Gaussian noise with time-varying covariance matrix $\mathcal{Q}^\zeta(t)$. \mathbf{M} , \mathbf{C} , \mathbf{K} are respectively the matrices of mass, damping and stiffness.

Now let us describe the structural characteristics of the system (2). The modes or eigenfrequencies μ and the associated eigenvectors Φ_μ of the system (2) are solutions of

$$\begin{aligned} \det[\mu^2 \mathbf{M} + \mu \mathbf{C} + \mathbf{K}] &= 0, \\ [\mu^2 \mathbf{M} + \mu \mathbf{C} + \mathbf{K}] \Phi_\mu &= 0. \end{aligned} \quad (3)$$

Then the mode-shapes are $\Psi_\mu = \mathbf{L} \Phi_\mu$. The frequency and damping coefficients are

$$\mathbf{f} = \frac{\mathbf{b}}{2\pi} \text{ (Hz)}, \quad \mathbf{d} = \frac{|\mathbf{a}|}{\sqrt{\mathbf{a}^2 + \mathbf{b}^2}} \in [0, 1] \quad (4)$$

with $\mathbf{a} = \Re(\mu)$ and $\mathbf{b} = \Im(\mu)$.

The monitored structure is defined by its modal characteristics: the collection of frequencies, dampings and mode shapes, as well as the covariances of the noises. The problem is to follow the slow evolutions of the structural characteristics of the mechanical system (2) by a recursive tracking method, whose starting values will be defined as the output of the data driven subspace method as described in Van Overschee & De Moor [8, Fig. 3.13 p. 90].

The tracking algorithm will focus on the frequencies and dampings, the mode shapes are assumed not to change significantly during the monitoring in regard to the changes in the eigenvalues. A change in the mode shapes would most likely be a local change in the structure, thus will indicate the presence of damage, whereas a change in the eigenvalues can still occur without presence of damage and not affect significantly the mode shapes (as for example the effect of temperature on the stiffness of the structure).

B. State–space model and canonical parameterization

We rewrite the preceding system (1)–(2) as a linear state–space model. Define

$$X_k \stackrel{\text{def}}{=} \begin{bmatrix} Z^{(k\delta)} \\ \dot{Z}^{(k\delta)} \end{bmatrix}$$

and $F \stackrel{\text{def}}{=} e^{\delta A}$ with $A \stackrel{\text{def}}{=} \begin{bmatrix} 0 & I \\ -M^{-1}K & -M^{-1}C \end{bmatrix} \in \mathbb{R}^{2n \times 2n}$.

From (2) we get

$$X_{k+1} = F X_k + \sigma \zeta_k \quad (5)$$

where $\zeta_k \stackrel{\text{def}}{=} \int_{(k-1)\delta}^{k\delta} e^{(k\delta-u)A} \begin{bmatrix} 0 \\ dB_u \end{bmatrix}$ and $B_t \stackrel{\text{def}}{=} \int_0^t \zeta(s) ds$ is a Brownian motion. Hence ζ_k is a (discrete–time) white Gaussian noise with covariance matrix

$$\int_{(k-1)\delta}^{k\delta} e^{(k\delta-u)A} \begin{bmatrix} 0 & 0 \\ 0 & M^{-1} Q_\zeta^{(u)} (M^{-1})^* \end{bmatrix} e^{(k\delta-u)A^*} du$$

which is approximated by δQ_k^ζ with

$$Q_k^\zeta \stackrel{\text{def}}{=} \begin{bmatrix} 0 & 0 \\ 0 & M^{-1} Q_\zeta^{(k\delta)} (M^{-1})^* \end{bmatrix}.$$

From (1) we get

$$y_k = [\mathbf{L} \ 0] X_k + \nu v_k \quad (6)$$

where $[\mathbf{L} \ 0] \in \mathbb{R}^{d \times 2n}$ and v_k is a $N(0, Q_k^v)$ white Gaussian noise which allows to take into account of the errors of modeling and the measurement noise. We suppose that the Hermitian matrix Q_k^v is positive definite.

Let (λ, Φ_λ) be the eigenstructure of the state transition matrix F , namely

$$\det(F - \lambda I) = 0, \quad (F - \lambda I) \Phi_\lambda = 0. \quad (7)$$

The parameters (μ, Φ_μ) in (3) can be deduced from the (λ, Φ_λ) 's using $e^{\delta\mu} = \lambda$ and $\Phi_\mu = \Phi_\lambda$. The frequency and damping coefficients (4) are recovered from a discrete eigenvalue λ through

$$\mathbf{a} = \frac{1}{\delta} \log |\lambda|, \quad \mathbf{b} = \frac{1}{\delta} \arctan \left[\frac{\Im(\lambda)}{\Re(\lambda)} \right].$$

Hypothesis: We suppose that F admits $2n$ pairwise complex conjugate distinct eigenvalues $\lambda_{1:n}, \bar{\lambda}_{1:n}$ with associated orthonormal set of eigenvectors $\Phi_{1:n}, \bar{\Phi}_{1:n}$ (¹). We also suppose that these eigenvalues have modulus less than one.

It turns out that this collection of modes forms a very natural parameterization for structural analysis. It is invariant w.r.t. changes in the state basis of system (5)–(6). In other words, the (λ, Φ_λ) 's form a canonical parameterization of the eigenstructure (or equivalently the pole part) of that system.

¹Notations: x^T is the transpose of x , \bar{x} is the complex conjugate, x^* is the transpose/conjugate, $|x|$ the modulus, j will denote $\sqrt{-1}$.

1) *Change of variables:* Define

$$\Phi \stackrel{\text{def}}{=} [\Phi_{1:n}], \quad \Psi \stackrel{\text{def}}{=} [\Psi_{1:n}], \quad \Lambda \stackrel{\text{def}}{=} \text{diag}(\lambda_{1:n}).$$

We introduce the following linear transformation

$$T \stackrel{\text{def}}{=} [\Phi \ \bar{\Phi}] \in \mathbb{C}^{2n \times 2n},$$

i.e. the matrix whose columns are the eigenvectors of F . It is a unitary matrix, i.e. $T^{-1} = T^*$. Then

$$\begin{bmatrix} \Lambda & (0) \\ (0) & \bar{\Lambda} \end{bmatrix} = T^* F T \in \mathbb{C}^{2n \times 2n}.$$

Define also

$$H \stackrel{\text{def}}{=} [\mathbf{L} \ 0] T = [\mathbf{L} \ 0] [\Phi \ \bar{\Phi}] = [\Psi \ \bar{\Psi}] \in \mathbb{C}^{d \times 2n},$$

Then after the change of variables $\tilde{X}_k \stackrel{\text{def}}{=} T^* X_k$, the vector \tilde{X}_k is of the form $\begin{bmatrix} x_k \\ \bar{x}_k \end{bmatrix}$ and (5) reduces to

$$x_{k+1} = \Lambda x_k + \sigma \Phi^* \zeta_k, \quad \zeta_k \stackrel{\text{iid}}{\sim} N(0, \delta Q_k^\zeta).$$

In practice we just have access to the mode shapes matrix $\Psi_{1:n}$ and not to the eigenvectors matrix $\Phi_{1:n}$, so in order to fully specify the state equation we suppose that the covariance matrix Q_k^ζ is of the form $[\mathbf{L} \ 0]^* Q_k [\mathbf{L} \ 0]$ for a given covariance matrix Q_k . Hence $w_k \stackrel{\text{def}}{=} \Phi^* \zeta_k$ is a white Gaussian noise with covariance matrix $Q_k^w \stackrel{\text{def}}{=} \delta \Psi^* Q_k \Psi$.

The observation equation (6) becomes

$$y_k = \Psi x_k + \bar{\Psi} \bar{x}_k + \nu v_k, \quad v_k \stackrel{\text{iid}}{\sim} N(0, Q_k^v).$$

Note that $\Psi x + \bar{\Psi} \bar{x} = 2 \Re\{\Psi x\}$ is a linear operator.

2) *The state/space system:* One obtains

$$x_{k+1} = \Lambda x_k + \sigma w_k, \quad w_k \stackrel{\text{iid}}{\sim} N(0, Q_k^w), \quad (8)$$

$$y_k = 2 \Re\{\Psi x_k\} + \nu v_k, \quad v_k \stackrel{\text{iid}}{\sim} N(0, Q_k^v). \quad (9)$$

All parameters are assumed known except the eigenvalues matrix $\Lambda \stackrel{\text{def}}{=} \text{diag}(\lambda_{1:n})$ and the noise intensities σ and ν . The mode shapes matrix $\Psi = [\Psi_{1:n}]$, the sampling period δ , and the covariance matrices Q_k and Q_k^v are given (then $Q_k^w = \delta \Psi^* Q_k \Psi$). From now on we suppose that $Q_k^v = I$.

C. The RMLE procedure

Let $L_k(\theta)$ be the likelihood function of θ for the observations $y_{1:k}$. We will see that $\ell_k(\theta) \stackrel{\text{def}}{=} \frac{1}{k} \log L_k(\theta)$ admits an incremental formulation

$$\ell_k(\theta) = \frac{1}{k} \sum_{l=1}^k r_l(\theta).$$

Then the score function is

$$\dot{\ell}_k(\theta) = \frac{1}{k} \sum_{l=1}^k \dot{r}_l(\theta)$$

and the RMLE procedure is

$$\theta_k \leftarrow \theta_{k-1} + \gamma_k \times \dot{r}_k(\theta_{k-1})$$

where γ_k is a non–increasing sequence of positive numbers.

In § III we present the Kalman filter–based approximation of the score increment $\dot{r}_k(\theta)$ and in § IV its particle filter–based counterpart. This last approximation, contrary to the first one, is valid in the nonlinear/non–Gaussian case.

III. KALMAN RMLE FOR A LINEAR SYSTEM

Consider the following linear system

$$\begin{aligned} x_{k+1} &= F(\theta) x_k + G(\theta) w_k, & w_k &\stackrel{\text{iid}}{\sim} N(0, Q_k^w), \\ y_k &= H(\theta) x_k + \Sigma(\theta) v_k, & v_k &\stackrel{\text{iid}}{\sim} N(0, Q_k^v), \end{aligned}$$

x_k takes values in \mathbb{C}^n and y_k in \mathbb{C}^d . The state initial law is $x_0 \sim N(\bar{x}_0, \mathcal{R}_0)$. Initial condition x_0 , state noise w_k and observation noise v_k are mutually independent.

Here $\theta \in \mathbb{R}$ is an unknown *real* parameter: the derivative w.r.t. this parameter will be denoted “.” or “ ∂_θ ”. Suppose that the system matrices are differentiable w.r.t. θ .

For every fixed θ , the conditional laws $\text{law}(x_k|y_{1:k-1}) = N(\hat{x}_{k-}^\theta, \mathcal{R}_{k-}^\theta)$ and $\text{law}(x_k|y_{1:k}) = N(\hat{x}_k^\theta, \mathcal{R}_k^\theta)$ are given

a – initialization: θ (initial guess), $\hat{x}_0^\theta = \bar{x}_0$, $\mathcal{R}_0^\theta = \mathcal{R}_0$
b – Kalman filter

$$\begin{aligned} \hat{x}_{k-}^\theta &= F(\theta) \hat{x}_{k-1}^\theta \\ \mathcal{R}_{k-}^\theta &= F(\theta) \mathcal{R}_{k-1}^\theta F(\theta)^* + G(\theta) Q_{k-1}^w G(\theta)^* \\ \hat{v}_k^\theta &= y_k - H(\theta) \hat{x}_{k-}^\theta \\ \mathcal{S}_k^\theta &= H(\theta) \mathcal{R}_{k-}^\theta H(\theta)^* + \Sigma(\theta) Q_k^v \Sigma(\theta)^* \\ K_k^\theta &= \mathcal{R}_{k-}^\theta H(\theta)^* [S_k^\theta]^{-1} \\ \hat{x}_k^\theta &= \hat{x}_{k-}^\theta + K_k^\theta \hat{v}_k^\theta \\ \mathcal{R}_k^\theta &= \{I - K_k^\theta H(\theta)\} \mathcal{R}_{k-}^\theta \end{aligned}$$

c – tangent Kalman filter

$$\begin{aligned} \dot{\hat{x}}_{k-}^\theta &= F(\theta) \dot{\hat{x}}_{k-1}^\theta + \dot{F}(\theta) \hat{x}_{k-1}^\theta \\ \dot{\mathcal{R}}_{k-}^\theta &= F(\theta) \dot{\mathcal{R}}_{k-1}^\theta F(\theta)^* \\ &\quad + \dot{F}(\theta) \mathcal{R}_{k-1}^\theta F(\theta)^* + F(\theta) \mathcal{R}_{k-1}^\theta \dot{F}(\theta)^* \\ &\quad + \dot{G}(\theta) Q_{k-1}^w G(\theta)^* + G(\theta) Q_{k-1}^w \dot{G}(\theta)^* \\ \dot{\hat{v}}_k^\theta &= -\dot{H}(\theta) \hat{x}_{k-}^\theta - H(\theta) \dot{\hat{x}}_{k-}^\theta \\ \dot{\mathcal{S}}_k^\theta &= H(\theta) \dot{\mathcal{R}}_{k-}^\theta H(\theta)^* \\ &\quad + \dot{H}(\theta) \mathcal{R}_{k-}^\theta H(\theta)^* + H(\theta) \mathcal{R}_{k-}^\theta \dot{H}(\theta)^* \\ &\quad + \dot{\Sigma}(\theta) Q_k^v \Sigma(\theta)^* + \Sigma(\theta) Q_k^v \dot{\Sigma}(\theta)^* \\ \dot{K}_k^\theta &= \dot{\mathcal{R}}_{k-}^\theta H(\theta)^* [S_k^\theta]^{-1} + \mathcal{R}_{k-}^\theta \dot{H}(\theta)^* [S_k^\theta]^{-1} \\ &\quad - \mathcal{R}_{k-}^\theta H(\theta)^* [S_k^\theta]^{-1} \dot{S}_k^\theta [S_k^\theta]^{-1} \\ \dot{\hat{x}}_k^\theta &= \dot{\hat{x}}_{k-}^\theta + \dot{K}_k^\theta \hat{v}_k^\theta + K_k^\theta \dot{\hat{v}}_k^\theta \\ \dot{\mathcal{R}}_k^\theta &= \{I - K_k^\theta H(\theta)\} \dot{\mathcal{R}}_{k-}^\theta \\ &\quad - \{K_k^\theta H(\theta) + K_k^\theta \dot{H}(\theta)\} \mathcal{R}_{k-}^\theta \end{aligned}$$

d – score increment

$$\begin{aligned} \hat{v}_k^\theta &= [S_k^\theta]^{-1} \hat{v}_k^\theta \\ \dot{r}_k(\theta) &= -\frac{1}{2} \text{trace}\{[S_k^\theta]^{-1} \dot{S}_k^\theta\} - \frac{1}{2} [\hat{v}_k^\theta]^* \dot{S}_k^\theta \hat{v}_k^\theta \\ &\quad + \Re\{[\hat{v}_k^\theta]^* \{H(\theta) \dot{\hat{x}}_{k-}^\theta + \dot{H}(\theta) \hat{x}_{k-}^\theta\}\} \end{aligned}$$

e – parameters update $\theta \leftarrow \theta + \gamma_k \times \dot{r}_k(\theta)$

recursively by the Kalman filter (see Part *b* in TABLE I).

A. Likelihood function

Define the innovation process

$$\hat{v}_k \stackrel{\text{def}}{=} y_k - \mathbb{E}_\theta[y_k|y_{1:k-1}] = y_k - H(\theta) \hat{x}_{k-}^\theta.$$

As $\mathbb{P}_\theta(y_{1:k} \in dy_{1:k}) = \prod_{l=1}^k \mathbb{P}_\theta(y_l \in dy_l|y_{1:l-1} = y_{1:l-1})$ and $\text{law}(y_k|y_{1:k-1}) = N(H(\theta) \hat{x}_{k-}^\theta, \mathcal{S}_k^\theta)$ where \mathcal{S}_k^θ is the covariance of the innovation process. We get

$$\mathbb{P}_\theta(y_{1:k} \in dy_{1:k}) = \prod_{l=1}^k g_l^\theta(y_l) dy_l$$

where $g_k^\theta(y)$ is the p.d.f. of the $N(H(\theta) \hat{x}_{k-}^\theta, \mathcal{S}_k^\theta)$ law. This means that $r_l(\theta) \stackrel{\text{def}}{=} \log g_l^\theta(y_l)$.

B. Score function

In order to calculate the score increment $\dot{r}_k(\theta)$, one sets an auxiliary result. Consider the p.d.f. $q^\theta(x)$ of the normal law $N(\mu(\theta), \mathcal{R}(\theta))$ on \mathbb{C}^n whose mean $\mu(\theta)$ and covariance matrix $\mathcal{R}(\theta) > 0$ are differentiable w.r.t. a scalar parameter $\theta \in \mathbb{R}$. Then the two classical identities

$$\begin{aligned} \partial_\theta \log |\mathcal{R}(\theta)| &= \frac{\partial_\theta |\mathcal{R}(\theta)|}{|\mathcal{R}(\theta)|} = \text{trace}\{[\mathcal{R}(\theta)]^{-1} \dot{\mathcal{R}}(\theta)\}, \\ \partial_\theta [\mathcal{R}(\theta)]^{-1} &= -[\mathcal{R}(\theta)]^{-1} \dot{\mathcal{R}}(\theta) [\mathcal{R}(\theta)]^{-1} \end{aligned}$$

applied to $\log q^\theta(x)$ give

$$\begin{aligned} \partial_\theta \log q^\theta(x) &= -\frac{1}{2} \text{trace}\{[\mathcal{R}(\theta)]^{-1} \dot{\mathcal{R}}(\theta)\} \\ &\quad + \Re\left\{\{x - \mu(\theta)\}^* [\mathcal{R}(\theta)]^{-1} \dot{\mu}(\theta)\right\} \\ &\quad - \frac{1}{2} \{x - \mu(\theta)\}^* [\mathcal{R}(\theta)]^{-1} \dot{\mathcal{R}}(\theta) [\mathcal{R}(\theta)]^{-1} \{x - \mu(\theta)\}. \end{aligned}$$

From this result the score increment is

$$\begin{aligned} \dot{r}_k(\theta) &= -\frac{1}{2} \text{trace}\{[S_k^\theta]^{-1} \dot{S}_k^\theta\} \\ &\quad + \Re\left\{\{y_k - H(\theta) \hat{x}_{k-}^\theta\}^* [S_k^\theta]^{-1} \{H(\theta) \dot{\hat{x}}_{k-}^\theta + \dot{H}(\theta) \hat{x}_{k-}^\theta\}\right\} \\ &\quad - \frac{1}{2} \{y_k - H(\theta) \hat{x}_{k-}^\theta\}^* [S_k^\theta]^{-1} \dot{S}_k^\theta [S_k^\theta]^{-1} \{y_k - H(\theta) \hat{x}_{k-}^\theta\}. \end{aligned}$$

IV. PARTICLE FILTER RMLE FOR A NONLINEAR SYSTEM

Most of real case studies do not meet the linear/Gaussian hypothesis. We present now a fully nonlinear model and its particle approximation.

A. The problem

Consider a state/observation process whose law depends on an unknown parameter $\theta \in \mathbb{R}$. The state process $x = \{x_k\}_{k \geq 0}$ takes values in \mathbb{R}^n , it is Markovian with transition kernel Q_k^θ and initial probability law μ_0 ,

$$Q_k^\theta(dx'|x) \stackrel{\text{def}}{=} \mathbb{P}_\theta(x_{k+1} \in dx'|x_k = x), \quad (10)$$

$$\mu_0(dx) \stackrel{\text{def}}{=} \mathbb{P}_\theta(x_0 \in dx). \quad (11)$$

This process describes the evolution of a non observed system. The observation process $y = \{y_k\}_{k \geq 1}$ takes values in \mathbb{R}^d . We suppose that (i) conditionally to the state process, the observations y_k are independent, and (ii) the observation y_k depends only on x_k (y_k is the observation of x_k), i.e.

$$\mathbb{P}_\theta(y_{1:k} \in dy_{1:k}|x_{0:k} = x_{0:k}) = \prod_{l=1}^k \mathbb{P}_\theta(y_l \in dy_l|x_l = x_l).$$

TABLE I

Kalman recursive maximum likelihood procedure.

The law of the process (x, y) is now completely specified. We assume moreover that the conditional law of y_k given x_k admits a density w.r.t. the Lebesgue measure:

$$\psi_k^\theta(y|x) dy \stackrel{\text{def}}{=} \mathbb{P}_\theta(y_k \in dy | x_k = x). \quad (12)$$

Then the law of the process (x, y) can be expressed explicitly according to the terms (10), (11) and (12), see § IV-C.

The system depends on the parameter θ through the kernel Q_k^θ and the local likelihood function ψ_k^θ . For simplicity we suppose that the initial law does not depend on θ . Like in Doucet & Tadić [3], we consider the case where the Markov kernel Q_k^θ admits a density w.r.t. the Lebesgue measure

$$Q_k^\theta(dx'|x) = q_k^\theta(x'|x) dx.$$

B. Nonlinear filter

Define the nonlinear filter and the predicted nonlinear filter

$$\begin{aligned} \pi_k^\theta(dx|y_{1:k}) &\stackrel{\text{def}}{=} \mathbb{P}_\theta(x_k \in dx | y_{1:k} = y_{1:k}), \\ \pi_{k-}^\theta(dx|y_{1:k-1}) &\stackrel{\text{def}}{=} \mathbb{P}_\theta(x_k \in dx | y_{1:k-1} = y_{1:k-1}). \end{aligned}$$

We also use the notation $\pi_k^\theta(dx) \stackrel{\text{def}}{=} \pi_k^\theta(dx|y_{1:k})$, $\pi_{k-}^\theta(dx) \stackrel{\text{def}}{=} \pi_{k-}^\theta(dx|y_{1:k-1})$ and $\psi_k^\theta(x) \stackrel{\text{def}}{=} \psi_k^\theta(y_k|x)$. These conditional densities can be recursively obtained through the classical two steps procedure:

$$(13)$$

where the prediction (linear) operator Q_{k-1}^θ and the correction (nonlinear) operator Ψ_k^θ , which act on the space of probability measures, are defined by

$$\begin{aligned} \pi Q_{k-1}^\theta(dx') &\stackrel{\text{def}}{=} \int Q_{k-1}^\theta(dx'|x) \pi(dx), \\ \Psi_k^\theta[\pi](dx) &\stackrel{\text{def}}{=} \psi_k^\theta(x) \pi(dx) / \langle \pi, \psi_k^\theta \rangle \end{aligned} \quad (14)$$

$$(15)$$

where $\langle \pi, \psi \rangle \stackrel{\text{def}}{=} \int_{\mathbb{R}^n} \psi(x) \pi(dx)$. Q_k^θ is the transition kernel of the Markov chain x_k and the first step in (13) is the Chapman–Kolmogorov equation. The second step in (13) is a Bayes formula. The initial condition in (13) is $\pi_0^\theta = \mu_0$.

C. Likelihood and score functions

According to the previous section, the joint law of the state and observation processes is

$$\begin{aligned} \mathbb{P}_\theta(x_{0:k} \in dx_{0:k}, y_{1:k} \in dy_{1:k}) \\ = \mu_0(dx_0) \prod_{l=1}^k \{ \psi_l^\theta(y_l|x_l) Q_{l-1}^\theta(dx_l|x_{l-1}) \} dy_{1:k}. \end{aligned}$$

This proves that this statistical model is dominated and

$$L_k(\theta) = \int_{x_{0:k}} \mu_0(dx_0) \prod_{l=1}^k \{ \psi_l^\theta(x_l) Q_{l-1}^\theta(dx_l|x_{l-1}) \}.$$

It's well known that

$$\mathbb{P}^\theta(y_{1:k} \in dy_{1:k}) = \prod_{l=1}^k \int_{x_l} \psi_l^\theta(y_l|x_l) \pi_{l-}^\theta(dx_l|y_{1:l-1}) dy_{1:k}$$

which leads to the other formulation

$$L_k(\theta) = \prod_{l=1}^k \langle \pi_{l-}^\theta, \psi_l^\theta \rangle \quad \text{and} \quad r_l(\theta) \stackrel{\text{def}}{=} \log \langle \pi_{l-}^\theta, \psi_l^\theta \rangle$$

and the score increment is

$$\dot{r}_k(\theta) = \frac{\langle \dot{\pi}_{k-}^\theta, \psi_k^\theta \rangle + \langle \pi_{k-}^\theta, [\partial_\theta \log \psi_k^\theta] \psi_k^\theta \rangle}{\langle \pi_{k-}^\theta, \psi_k^\theta \rangle}. \quad (16)$$

D. Tangent filter

Let $\mathcal{M}(\mathbb{R}^n)$ the set of finite (signed) measures on $(\mathbb{R}^n, \mathcal{B}(\mathbb{R}^n))$, $\mathcal{M}_1^+(\mathbb{R}^n)$ that of probability measures on $(\mathbb{R}^n, \mathcal{B}(\mathbb{R}^n))$, and $\mathcal{M}^0(\mathbb{R}^n)$ that of null mass. Then $\pi_{k-}^\theta \in \mathcal{M}_1(\mathbb{R}^n)$, $\dot{\pi}_{k-}^\theta \in \mathcal{M}^0(\mathbb{R}^n)$ and $\dot{\pi}_{k-}^\theta \ll \pi_{k-}^\theta$.

We now establish a recursive formulation for $\dot{\pi}_{k-}^\theta$ and $\dot{\pi}_k^\theta$.
1) *Prediction step*: The derivative \dot{Q}_{k-1}^θ of the Markov kernel Q_{k-1}^θ w.r.t. the parameter θ is

$$\dot{Q}_{k-1}^\theta(dx'|x) = [\partial_\theta \log q_{k-1}^\theta(x'|x)] Q_{k-1}^\theta(dx'|x). \quad (17)$$

\dot{Q}_{k-1}^θ is a transition kernel on $\mathcal{M}^0(\mathbb{R}^n)$. Then, the derivative of the nonlinear filter w.r.t. the parameter θ is

$$\dot{\pi}_{k-}^\theta = \partial_\theta \{ \pi_{k-1}^\theta Q_{k-1}^\theta \} = \dot{\pi}_{k-1}^\theta Q_{k-1}^\theta + \pi_{k-1}^\theta \dot{Q}_{k-1}^\theta. \quad (18)$$

2) *Correction step*: One introduces $D\Psi_k^\theta[\pi] \nu \in \mathcal{M}^0(\mathbb{R}^n)$ the derivative of the operator $\pi \mapsto \Psi_k^\theta[\pi]$ at the point $\pi \in \mathcal{M}_1^+(\mathbb{R}^n)$ in the direction $\nu \in \mathcal{M}^0(\mathbb{R}^n)$

$$D\Psi_k^\theta[\pi] \nu \stackrel{\text{def}}{=} \frac{\psi_k^\theta \nu}{\langle \pi, \psi_k^\theta \rangle} - \frac{\langle \nu, \psi_k^\theta \rangle}{\langle \pi, \psi_k^\theta \rangle} \frac{\psi_k^\theta \pi}{\langle \pi, \psi_k^\theta \rangle}.$$

If $\nu \ll \pi$ and $\nu(dx) = \varrho(x) \pi(dx)$ then

$$D\Psi_k^\theta[\pi] \nu = \{ \varrho - \langle \Psi_k^\theta[\pi], \varrho \rangle \} \Psi_k^\theta[\pi].$$

Moreover, one has

$$\begin{aligned} \partial_\theta \Psi_k^\theta[\pi] &= \{ \partial_\theta \log \psi_k^\theta - \langle \Psi_k^\theta[\pi], \partial_\theta \log \psi_k^\theta \rangle \} \Psi_k^\theta[\pi] \\ &= D\Psi_k^\theta[\pi]([\partial_\theta \log \psi_k^\theta] \pi). \end{aligned}$$

Finally

$$\dot{\pi}_k^\theta = \partial_\theta \{ \Psi_k^\theta[\pi_{k-}^\theta] \} = D\Psi_k^\theta[\pi_{k-}^\theta](\dot{\pi}_{k-}^\theta + [\partial_\theta \log \psi_k^\theta] \pi_{k-}^\theta).$$

Hence we can prove recursively that the tangent filter is absolutely continuous w.r.t. the nonlinear filter, i.e. $\dot{\pi}_{k-}^\theta \ll \pi_{k-}^\theta$ and $\dot{\pi}_k^\theta \ll \pi_k^\theta$. Let

$$\varrho_{k-}^\theta(x) \stackrel{\text{def}}{=} \frac{d\dot{\pi}_{k-}^\theta}{d\pi_{k-}^\theta}(x), \quad \varrho_k^\theta(x) \stackrel{\text{def}}{=} \frac{d\dot{\pi}_k^\theta}{d\pi_k^\theta}(x).$$

This leads to

$$\dot{\pi}_k^\theta = \left\{ \varrho_{k-}^\theta + \partial_\theta \log \psi_k^\theta - \langle \pi_k^\theta, \varrho_{k-}^\theta + \partial_\theta \log \psi_k^\theta \rangle \right\} \pi_k^\theta. \quad (19)$$

3) *Score increment*: Expression (16) becomes

$$\dot{r}_k(\theta) = \langle \pi_k^\theta, \varrho_{k-}^\theta + \partial_\theta \log \psi_k^\theta \rangle \quad (20)$$

which is exactly the centering term in (19).

E. Particle approximation of the nonlinear/tangent filters

We describe the simple ‘‘bootstrap’’ particle approximation. Suppose that at time $k-1$ we have particle approximation of the nonlinear and tangent filters

$$\begin{aligned} \pi_{k-1}^\theta &\simeq \pi_{k-1}^N \stackrel{\text{def}}{=} \frac{1}{N} \sum_{i=1}^N \delta_{\xi_{k-1}^i}, \\ \dot{\pi}_{k-1}^\theta &\simeq \dot{\pi}_{k-1}^N \stackrel{\text{def}}{=} \frac{1}{N} \sum_{i=1}^N \rho_{k-1}^i \delta_{\xi_{k-1}^i}. \end{aligned}$$

Note that $\sum_{i=1}^N \rho_{k-1}^i = 0$, i.e. $\dot{\pi}_{k-1}^N \in \mathcal{M}^0(\mathbb{R}^n)$. The idea of this approximation is to assure that $\dot{\pi}_{k-1}^N \ll \pi_{k-1}^N$, indeed

$$\varrho_{k-1}^N(\xi_{k-1}^i) \stackrel{\text{def}}{=} \frac{d\dot{\pi}_{k-1}^N}{d\pi_{k-1}^N}(\xi_{k-1}^i) = \frac{\sum_{i': \xi_{k-1}^{i'} = \xi_{k-1}^i} \rho_{k-1}^{i'}}{\sum_{i': \xi_{k-1}^{i'} = \xi_{k-1}^i} 1} \quad (21)$$

for $i = 1 \dots N$ and $\varrho_{k-1}^N(x) = 0$ if $x \notin \{ \xi_{k-1}^i; i = 1 \dots N \}$.

1) *Prediction/sampling step*: From (14),

$$\pi_{k-1}^N Q_{k-1}^\theta(dx') = \frac{1}{N} \sum_{i=1}^N Q_{k-1}^\theta(dx'|\xi_{k-1}^i).$$

The approximation $Q_{k-1}^\theta(dx'|\xi_{k-1}^i) \simeq \delta_{\xi_{k-}^i}(dx')$ where $\xi_{k-}^i \sim Q_{k-1}^\theta(dx'|\xi_{k-1}^i)$ (independently) gives

$$\pi_{k-}^N = \frac{1}{N} \sum_{i=1}^N \delta_{\xi_{k-}^i} \quad \text{where } \xi_{k-}^i \sim Q_{k-1}^\theta(dx'|\xi_{k-1}^i). \quad (22)$$

From the tangent filter prediction (18) and (17)

$$\begin{aligned} & \dot{\pi}_{k-1}^N Q_{k-1}^\theta(dx') + \pi_{k-1}^N \dot{Q}_{k-1}^\theta(dx') \\ &= \frac{1}{N} \sum_{i=1}^N \{ \rho_{k-1}^i + \partial_\theta \log q_{k-1}^\theta(x'|\xi_{k-1}^i) \} Q_{k-1}^\theta(dx'|\xi_{k-1}^i). \end{aligned}$$

Again let $Q_{k-1}^\theta(dx'|\xi_{k-1}^i) \simeq \delta_{\xi_{k-}^i}(dx')$ so that

$$\dot{\pi}_{k-}^N = \frac{1}{N} \sum_{i=1}^N \rho_{k-}^i \delta_{\xi_{k-}^i}$$

with $\rho_{k-}^i \stackrel{\text{def}}{=} \rho_{k-1}^i + \partial_\theta \log q_{k-1}^\theta(\xi_{k-}^i|\xi_{k-1}^i)$. This approximation $\dot{\pi}_{k-}^N$ is not of null mass, it will be ‘‘centered’’ in the correction step. Again $\varrho_{k-}^N(x)$ can be computed like in (21), but almost surely the particle positions ξ_{k-}^i are all distinct, so we have

$$\varrho_{k-}^N(\xi_{k-}^i) = \rho_{k-}^i, \quad i = 1 \cdots N.$$

2) *Correction/resampling step*: Plugging the approximation (22) in (15) gives exactly

$$\Psi_k^\theta[\pi_{k-}^N] = \sum_{i=1}^N \omega_k^i \delta_{\xi_{k-}^i}$$

where $\omega_k^i \stackrel{\text{def}}{=} \Psi_k^\theta(\xi_{k-}^i) / \sum_{i'=1}^N \Psi_k^\theta(\xi_{k-}^{i'})$.

The resampling step is the following: we multiply/discard particles $\{\xi_{k-}^i\}_{i=1:N}$ according to the high/low weights $\{\omega_k^i\}_{i=1:N}$, i.e. $\xi_{k-}^i = \xi_{k-}^{\mathbf{s}[i]}$ where $\mathbf{s}[i]$ is the resampling mechanism associated with the weights $\{\omega_k^i\}_{i=1:N}$. The updated particle approximation is then

$$\pi_k^N = \frac{1}{N} \sum_{i=1}^N \delta_{\xi_{k-}^{\mathbf{s}[i]}} \quad \text{with } \xi_{k-}^i = \xi_{k-}^{\mathbf{s}[i]} \quad (23)$$

and \mathbf{s} is the resampling scheme associated with $\{\omega_k^i\}_{i=1:N}$.

Substituting π_k^θ in (19) by its approximation (23) gives

$$\dot{\pi}_k^N = \frac{1}{N} \sum_{i=1}^N \rho_k^i \delta_{\xi_{k-}^{\mathbf{s}[i]}}$$

where ⁽²⁾

$$\begin{aligned} \rho_k^i &= \varrho_{k-}^\theta(\xi_{k-}^{\mathbf{s}[i]}) + \partial_\theta \log \psi_k^\theta(\xi_{k-}^{\mathbf{s}[i]}) - \text{centering term} \\ &= \rho_{k-}^{\mathbf{s}[i]} + \partial_\theta \log \psi_k^\theta(\xi_{k-}^{\mathbf{s}[i]}) - \text{centering term}. \end{aligned} \quad (24)$$

This last centering operation ensures that $\dot{\pi}_k^N \in \mathcal{M}^0(\mathbb{R}^n)$.

3) *Score increment*: Approximation (23) in (20) leads to

$$r_k^N(\theta) = \frac{1}{N} \sum_{i=1}^N \{ \rho_{k-}^{\mathbf{s}[i]} + \partial_\theta \log \psi_k^\theta(\xi_{k-}^{\mathbf{s}[i]}) \}$$

which is, like noticed in § IV-D.3, the centering term of (24).

²‘‘ $\alpha_i = \beta_i - \text{centering term}$ ’’ means that $\alpha_i = \beta_i - \sum_{i'=1}^N \beta_{i'}$

V. APPLICATION

In (8)–(9) there are two alternate parameterizations. The first one is in terms of real/imaginary part of the λ 's (7)

$$\theta \stackrel{\text{def}}{=} (\alpha_{1:n}, \beta_{1:n}, \sigma, \nu) \in \mathbb{R}^{2n} \times \mathbb{R}_+^2 \quad (25)$$

where $\alpha_p \stackrel{\text{def}}{=} \Re(\lambda_p)$ and $\beta_p \stackrel{\text{def}}{=} \Im(\lambda_p)$ for $p = 1 \cdots n$. The second one is in terms of frequency/damping coefficients (4)

$$\theta \stackrel{\text{def}}{=} (\mathbf{f}_{1:n}, \mathbf{d}_{1:n}, \sigma, \nu) \in \mathbb{R}_+^n \times (0, 1)^n \times \mathbb{R}_+^2. \quad (26)$$

If the behavior of the filter is quite equivalent in both parameterizations, the second is much simpler to use for the tuning of the parameters of the RMLE procedure.

Kalman filter formulation

Practical implementation of the algorithm describes in § III requires some adaptations. To prevent the degeneracy of the innovation covariance matrix it is necessary to reinforce the diagonal terms if \mathcal{S}_k^θ in Part *b* of TABLE I.

RMLE implementation

For each component θ_p of the parameter, the RMLE iteration used in practice is

$$\theta_p \leftarrow \theta_p + \left\{ \frac{\gamma}{k} + \gamma^{\min} \right\} \times \partial_{\theta_p} r_k(\theta) \Big|_{[-r_p^{\max}, r_p^{\max}]}$$

where $\partial_{\theta_p} r_k(\theta) \Big|_{[-r_p^{\max}, r_p^{\max}]} \stackrel{\text{def}}{=} \times \{ \partial_{\theta_p} r_k(\theta) \wedge r_p^{\max} \} \vee (-r_p^{\max})$. The gain decreases toward a minimal positive value in order to track the possible evolutions of the parameters. In addition, the size of the gradient steps is limited.

A case study

The results presented in this paper are based on some simulated data. The numerical values are representative of the first two modes of a real civil structure, and more, the parameter values were estimated on the structure using a batch subspace identification procedure.

Looking at two modes allows us to study parameter variations, which are characteristic of the flutter problem, which drives the application we are interested in. The parameter variations include frequencies crossing and abrupt changes in the damping. Those scenarios are illustrated in Fig. 1. Notice that, whereas we know what change scenarios we can expect from the frequency and damping in term of trend and amplitude, the associated eigenvalues variations have no real physical meaning.

The algorithm was preliminary initialized with some guessed starting values, then the filter was computed for a few hundred samples to initialize the tracking algorithm with correct estimates for the filter, then the tracking algorithm was processed on the time varying data.

The data samples were simulated with a sampling rate of 128Hz. The estimation plots are displayed with time (in sec.) on the x -coordinate. The simulated changes include for the first mode a slow increase in the frequency as well as a slow decrease in its damping value and for the second mode a slow decrease of the frequency and a abrupt increase in the damping. Let $n = 2$ and $d = 4$.

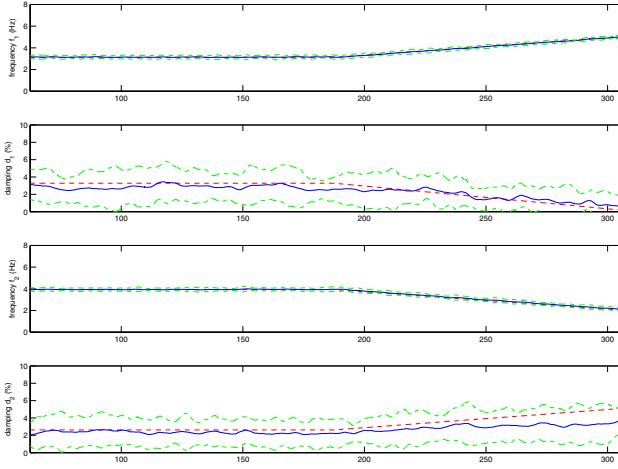


Fig. 1. Kalman RMLE procedure: monitoring of the frequency and damping parameters ($\mathbf{f}_i; \mathbf{d}_i$), $i = 1, 2$. Result of 20 Monte Carlo trials: true value (red/dashed line), empirical mean of the estimated value (blue/continuous line) $\pm 2 \times$ the empirical standard deviation (green/dashed line).

- mode 1 : $\lambda_1 = 0.9832823 + j 0.1520823$, $\mathbf{d}_1 = 0.032818$, $\mathbf{f}_1 = 3.1261001$

$$\psi_1 = \begin{bmatrix} -0.110149857 \\ 0.003170271 \\ -0.238437343 \\ 0.011789335 \end{bmatrix} + j \begin{bmatrix} -0.001391672 \\ -0.000642400 \\ 0.002764028 \\ -0.000028845 \end{bmatrix}$$

- mode 2 : $\lambda_2 = 0.9765406 + j 0.1905859$, $\mathbf{d}_2 = 0.0261820$, $\mathbf{f}_2 = 3.9265001$

$$\psi_2 = \begin{bmatrix} -0.005535022 \\ -0.116521290 \\ -0.010837860 \\ -0.219088797 \end{bmatrix} + j \begin{bmatrix} -0.000479459 \\ -0.000719393 \\ -0.000364371 \\ 0.005224397 \end{bmatrix}$$

We run 20 Monte Carlo trials: we compute the empirical mean of the estimated value and the confidence interval given by $\pm 2 \times$ the empirical standard deviation.

In Fig. 1 we plot both estimated and true variations for both frequency and damping coefficients. The two frequencies are crossing each other. Nonetheless both frequency estimates stay very close to their expected value, whereas the damping estimates do exhibit worse behavior, but still react to the small changes in their nominal values. Considering the variations in the damping, it would be wise to associate a detection procedure to the tracking algorithm to decide whether the damping has changed or not.

Looking at Fig. 2, one can see that the large variations in damping d_2 do reflect in a bad estimation for α_2 , whereas the slightly large variations in damping d_1 in Fig. 1 can not be inferred from the estimation of α_1 and β_1 in Fig. 2. This pleads in favor of parametrization (26).

VI. PERSPECTIVES

We have investigated the merits of the Kalman filtering for structural health monitoring. The current case study is a simulation experiment.

It appears that frequency/damping parameterization (26) yields to an algorithm much simpler to tune than using the alternate parameterization (25). Moreover focusing on

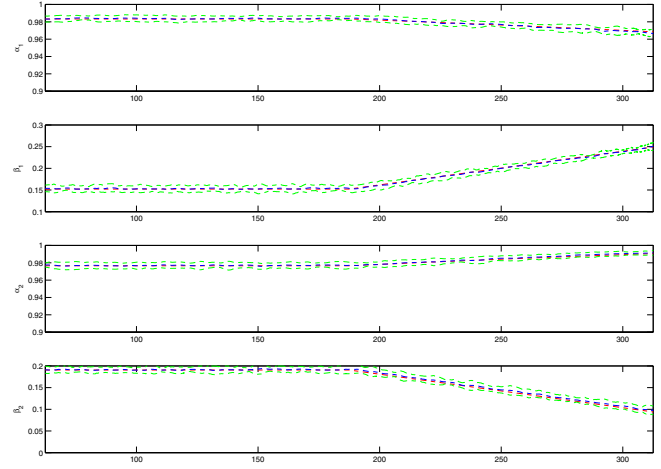


Fig. 2. Kalman RMLE procedure: monitoring of the eigenvalues $\alpha_i = \Re(\lambda_i)$ and $\beta_i = \Im(\lambda_i)$, $i = 1, 2$. Result of 20 Monte Carlo trials: true value (red/dashed line), empirical mean of the estimated value (blue/continuous line) $\pm 2 \times$ the empirical standard deviation (green/dashed line).

eigenvalues hide the uncertainties on the damping, which may be badly estimated whereas the associated eigenvalue estimation does not exhibit large variations.

Simulated data are well treated by the Kalman/tangent filters. Still the computations of the gain matrix and its derived terms presented in Table I are time consuming and can be numerically instable. For real data applications, it could be interesting to develop a so called *Kalman Ensemble filters* (see Evensen [9]) where the computations of the covariance matrices are done through empirical procedures over a few state particles. For more sophisticated (nonlinear) models, we can use the nonlinear model and particle approximation proposed in § IV-E though it could be more difficult to meet the real-time constraint.

The numerical tests were achieved by the authors and Nimish Sharma during his internship at Irisa.

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