



University of
Zurich ^{UZH}

I·Math Institute of Mathematics

SCHÉMAS NUMÉRIQUES ET MÉCANIQUE DES FLUIDES

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April 10, 2015



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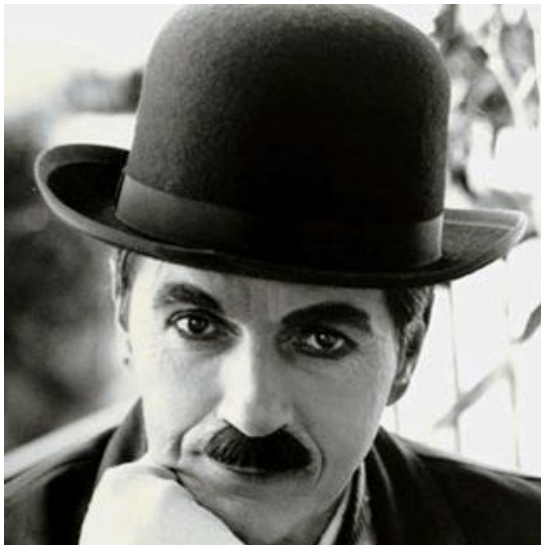


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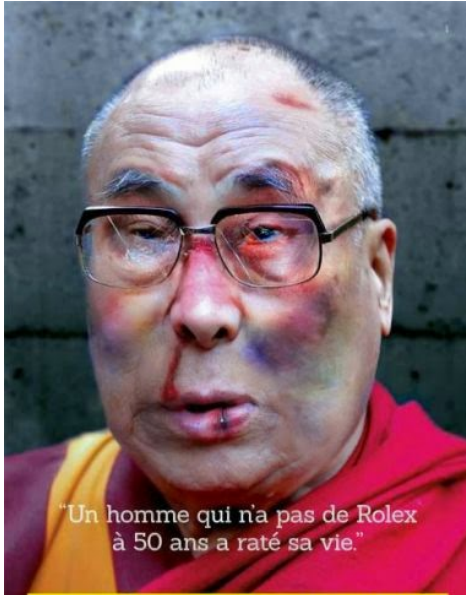
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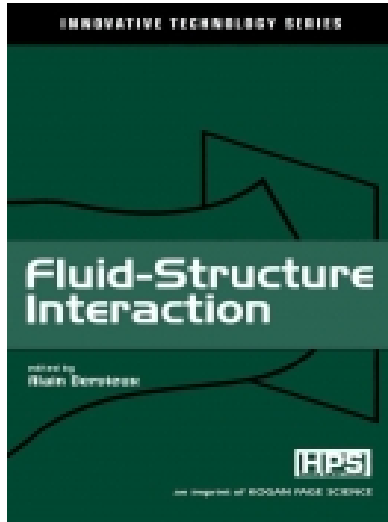


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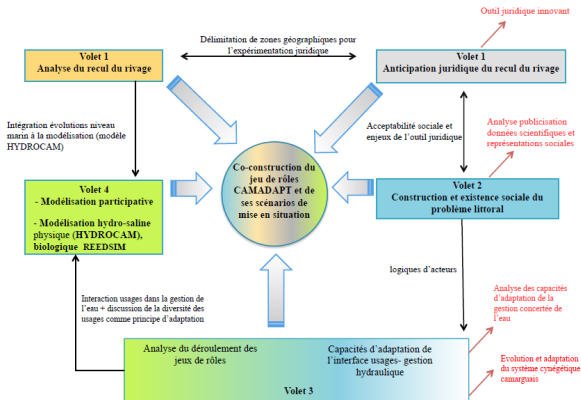


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Merci Alain !



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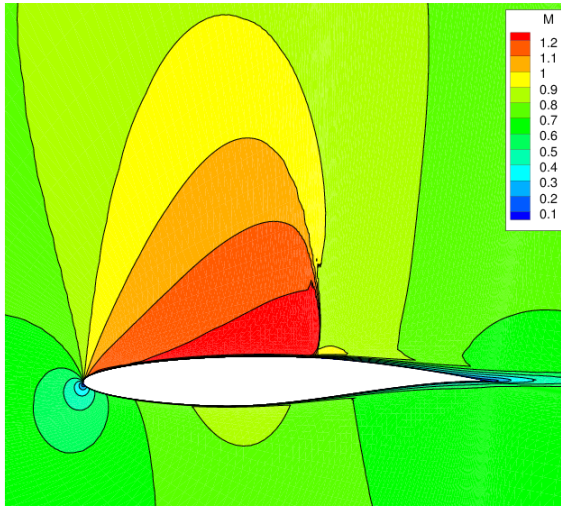
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RAE2822 AIRFOIL, TURBULENT

$M=0.734$, $Re=6.5 \cdot 10^6$, $AOA=2.79^\circ$





GOALS

$$\frac{\partial W}{\partial t} + \operatorname{div} (F(W) - F_v(W, \nabla W)) = S(\mathbf{x}, W)$$

- Emphasis on the structure of the operators: multidimensional, symmetries, structure of differential operators, equilibriums, etc: role of conservation in the large
- Easy implementation:
very local structures (geometrical+memory-wise) \rightarrow compact stencil
- Truly high order
- Stable and parameter free, including for strong shocks



GOALS

$$\frac{\partial W}{\partial t} + \operatorname{div} (F(W) - F_v(W, \nabla W)) - S(\mathbf{x}, W) = 0$$

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COLLABORATIVE WORK

- INRIA: M. Ricchiuto, M. Mezine, A. Larat, D. de Santis, A. Froehly, L. Nouveau, P. Jacq, etc
- U. Bordeaux: K. Mer-Nkonga, H. Beaugendre
- VKI: H. Deconinck,
- U. Michigan: P.L. Roe
- Curved meshes: C. Dobrzynski (U. Bordeaux), A. Froehly (Inria)



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OUTLINE

FORMULATIONS: CONSERVATION AND ACCURACY ISSUES

RESIDUAL DISTRIBUTION FRAMEWORK

APPLICATION TO STEADY TURBULENT FLOW PROBLEMS

EXTENSIONS: SHALLOW WATER

CONCLUSION



OVERVIEW

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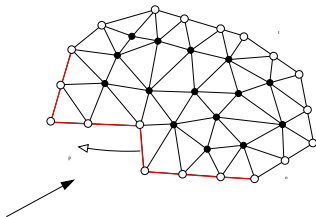
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MODEL PROBLEM, FRAMEWORK FOR STEADY SCALAR CONSERVATION LAWS.

$$\begin{aligned} \operatorname{div} f(u) &= 0 & \text{in } \Omega \\ u &= g & \text{on } \Gamma^- \end{aligned}$$



SOME NOTATIONS...

- Consider \mathcal{T}_h triangulation of Ω (can do with quads...)
- Unknowns (Degrees of Freedom, DoF) : $u_i \approx u(M_i)$
- $M_i \in \mathcal{T}_h$ a given set of nodes (vertices + other dofs)
- Denote by u_h continuous piecewise approximation (for example P^k Lagrange triangles/quads)



VARIATIONAL FORMULATION OF CONVECTED DOMINATED PROBLEMS, 1

Continuous finite elements: Galerkin+stabilisation.: Choose

$$V^h = U^h = \bigoplus \{u_K^h \in \mathbb{P}^k(K) \text{ and globally continuous}\}$$

STREAMLINE DIFFUSION (HUGHES ET AL.)

$$\sum_K \left(- \int_K \nabla v^h \cdot f(u^h) dx + \int_{\partial K} v^h f(u^h) \cdot \mathbf{n} \right. \\ \left. + h_K \int_K (\nabla f_u(u^h) \cdot \nabla v^h) \mathcal{T}(\nabla f_u(u^h) \cdot \nabla u^h) dx \right) = 0, \quad \mathcal{T} \geq 0.$$

JUMP OPERATOR (BURMAN ET AL.)

$$\sum_K \left(- \int_K \nabla v^h \cdot f(u^h) dx + \int_{\partial K} v^h f(u^h) \cdot \mathbf{n} \right) \\ + \sum_{\text{edges}} \Gamma h_e^2 \int_e \|\nabla_u f(u^h)\| |[\nabla u^h][\nabla v^h]| = 0, \quad \Gamma \geq 0$$



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REMARK

for all degree of freedom, $\sum_{K \ni i} \phi_i^K = 0$

SUPG

$$\sum_{i \in K} \left(- \int_K \nabla \varphi_i \cdot f(u^h) dx + \int_{\partial K} \varphi_i f(u^h) \cdot \mathbf{n} + h_K \int_K (\nabla f_u(u^h) \cdot \nabla \varphi_i) \mathcal{T}(\nabla f_u(u^h) \cdot \nabla u^h) \right) \phi_i^K$$

$$= \int_{\partial K} f(u^h) \cdot \mathbf{n}$$

Jump stabilisation

$$\sum_{i \in K} \left(- \int_K \nabla \varphi_i \cdot f(u^h) dx + \int_{\partial K} \varphi_i f(u^h) \cdot \mathbf{n} + \sum_{\text{edges} \subset K} \Gamma h_e^2 \int_e \|\nabla_u f(u^h)\| |[\nabla u^h][\nabla \varphi_i] \right) \phi_i^K$$

$$= \int_{\partial K} f(u^h) \cdot \mathbf{n}$$

because $\sum_{i \in K} \varphi_i = 1 \rightarrow \sum_{i \in K} \nabla \varphi_i = 0$



VARIATIONAL FORMULATION OF CONVECTED DOMINATED PROBLEMS,2

Discontinuous finite elements: Stabilisation via the jumps across edges $V^h = U^h = \bigoplus \{u|_K \in \mathbb{P}^k(K)\}$

$$\sum_K \left(- \int_K \nabla v^h \cdot f(u^h) dx + \int_{\partial K} \hat{f}(u_+^h, u_-^h, \mathbf{n}) v^h dl \right) = 0$$

Choice of numerical flux \hat{f} : E-scheme implies entropy stability.



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DG

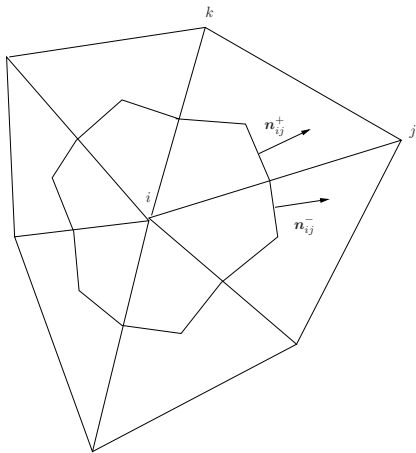
$$\sum_{i \in K} \left(\overbrace{- \int_K \nabla \varphi_i \cdot f(u^h) dx + \int_{\partial K} \hat{f}(u_+^h, u_-^h, \mathbf{n}) \varphi_i dl}^{\phi_i^K} \right) \\ = \int_{\partial K} \hat{f}(u_+^h, u_-^h, \mathbf{n}) dl$$

because again $\sum_{i \in K} \varphi_i = 1 \rightarrow \sum_{i \in K} \nabla \varphi_i = 0$



CASE OF FINITE VOLUME FORMULATION

$$\operatorname{div} \mathbf{f}(u) = 0$$

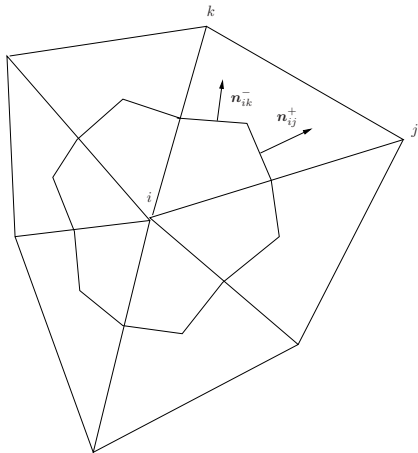


$$\sum_{j \in V(i)} \left[\hat{f}(u_i, u_j, \mathbf{n}_{ij}^+) + \hat{f}(u_i, u_j, \mathbf{n}_{ij}^-) \right] = 0$$



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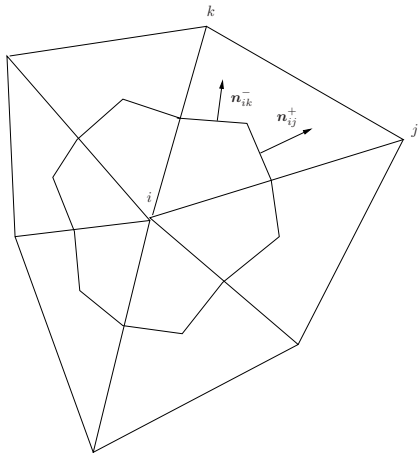


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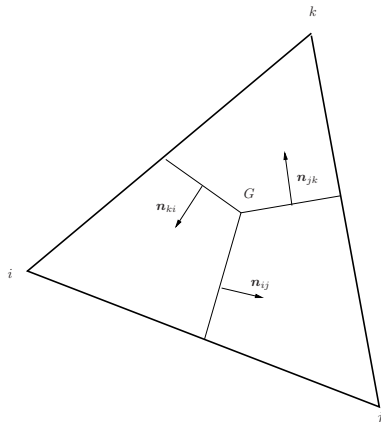
$$\sum_{K \ni i} \left[\hat{f}(u_i, u_j, \mathbf{n}_{ij}^+) + \hat{f}(u_i, u_k, \mathbf{n}_{ik}^-) - \mathbf{f}(u_i) \cdot (\mathbf{n}_{ij}^+ + \mathbf{n}_{ik}^-) \right] = 0$$

$\underbrace{\hspace{10em}}_{\Phi_i^k}$



CASE OF FINITE VOLUME FORMULATION

$$\operatorname{div} \mathbf{f}(u) = 0$$



Again, we have

$$\sum_{K \ni i} \Phi_i^K = 0$$

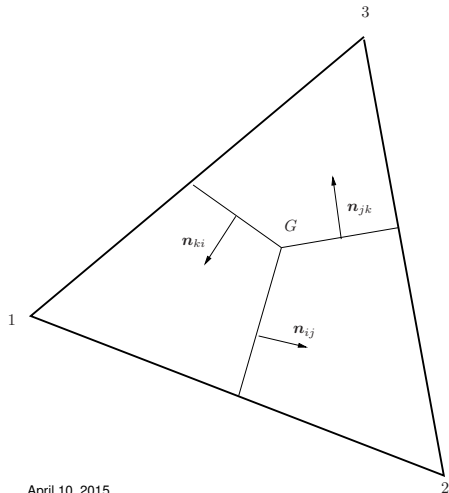
with

$$\begin{aligned} \Phi_i &:= \hat{f}(u_i, u_j, \mathbf{n}_{ij}^+) + \hat{f}(u_i, u_k, \mathbf{n}_{ik}^-) \\ &\quad - \mathbf{f}(u_i) \cdot (\mathbf{n}_{ij}^+ + \mathbf{n}_{ik}^-) \\ &= \hat{f}(u_i, u_j, \mathbf{n}_{ij}^+) + \hat{f}(u_i, u_k, \mathbf{n}_{ik}^-) \\ &\quad - \mathbf{f}(u_i) \cdot \frac{\mathbf{n}_i}{2} \end{aligned}$$



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$$\operatorname{div} \mathbf{f}(u) = 0$$



$$\Phi_i := \hat{f}(u_i, u_j, \mathbf{n}_{ij}^+) + \hat{f}(u_i, u_k, \mathbf{n}_{ik}^-) - \mathbf{f}(u_i) \cdot \frac{\mathbf{n}_i}{2}$$

$$\begin{aligned} \sum_{i \in K} \Phi_i &= - \sum_i \mathbf{f}(u_i) \cdot \frac{\mathbf{n}_i}{2} \\ &= \int_{\partial K} \mathbf{f}^h \cdot \mathbf{n} \end{aligned}$$



PARTIAL CONCLUSION:

We can rephrase many/all known schemes as:

$$\sum_{K \ni i} \Phi_i^K(u^h) = 0$$

where

- The $\Phi_i^K(u^h)$ are residuals, i.e. basically difference of fluxes,
- They all satisfy a conservation relation:

$$\sum_{i \in K} \Phi_i^K(u^h) = \int_{\partial K} \hat{f}(u^+, u^-, \mathbf{n})$$

\hat{f} numerical flux, take into account continuous/discontinuous element



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Can we exploit this to design schemes: yes !



FURTHER REMARKS ON THE TRUNCATION ERROR

Consider for example the residuals of SUPG for **Steady problem**

- $\operatorname{div} \mathbf{f}(u^{\text{ex}}) = 0$ and assume u^{ex} smooth enough.
- Call u^h some interpolant of u^{ex} , $u^h - u^{\text{ex}} = O(h_K^{r+1})$, $u^h \in \Phi^r(K)$
- Denote $\delta \mathbf{f} = \mathbf{f}(u^h) - \mathbf{f}(u^{\text{ex}})$

$$\begin{aligned}\Phi_i^K(u^h) &= - \int_K \nabla \varphi_i \cdot \mathbf{f}(u^h) d\mathbf{x} + \int_{\partial K} \varphi_i \mathbf{f}(u^h) \\ &\quad h_K \int_K (\nabla f_u(u^h) \cdot \nabla \varphi_i) \mathcal{T}(\nabla f_u(u^h) \cdot \nabla u^h) d\mathbf{x} \\ &= - \int_K \nabla \varphi_i \cdot \delta \mathbf{f} d\mathbf{x} + \int_{\partial K} \varphi_i \delta \mathbf{f} \\ &\quad h_K \int_K (\nabla f_u(u^h) \cdot \nabla \varphi_i) \mathcal{T}(\operatorname{div} \delta \mathbf{f}) d\mathbf{x} \\ &= O(h^{k+1+d-1}) + O(h^{k+1+d-1}) + O(h^{1+d-1+k}) = O(h^{k+d})\end{aligned}$$



FURTHER REMARKS ON THE TRUNCATION ERROR

ASSUMPTIONS AND FACTS:

Under steady problem+ smooth solution approximated in $\Phi^k(K)$

$$\Phi_i^K(u^h) = O(k^{k+d}).$$

- Same true for stabilisation with jumps
- Same true for DG (thanks to flux consistency) BUT violated when limiting: extrema problem.
- Wrong in general for FV, or difficult to achieve (very large stencils)
- Can be shown as the basis of a systematic truncation error analysis.



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NEXT STEP

Dual situation

- Combine the conservation relation

$$\sum_{i \in K} \Phi_i^K(u^h) = 0$$

- and the residual property

$$\Phi_i^K(u^h) = O(k^{k+d}).$$

to construct compact, stable, accurate, non oscillatory schemes: Residual distribution scheme



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FORMULATIONS: CONSERVATION AND ACCURACY ISSUES

RESIDUAL DISTRIBUTION FRAMEWORK

APPLICATION TO STEADY TURBULENT FLOW PROBLEMS

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RESIDUAL DISTRIBUTION SCHEMES

HISTORY

- Ni scheme, 1981. Engineer at Bombardier
- Roe, 1981 ($-x$)-today
- Deconinck, Ricchiuto, Nishikawa, Caraeni, ...
- Strong connections with stabilized FEM methods for convection-diffusion problems.
- ...

AIMS

- Combine ideas from finite volume schemes (non oscillatory, L^∞ stability, upwinding with finite element methods
- Simple implementation: no fancy limiters, no Riemann solvers, compact stencil, no tunable parameters



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- Simple implementation: no fancy limiters, no Riemann solvers, compact stencil, no tunable parameters
- Try something else than DG and high order finite volume



MODEL EQUATION: SCALAR STEADY CONVECTION-DIFFUSION

$\operatorname{div} \mathbf{f}(u) - \operatorname{div} (\mathbb{K} \nabla u) = 0$ on $\Omega \subset \mathbb{R}^d$ boundary conditions on $\partial\Omega$

- $\mathbf{f}(u) = (f_1(u), \dots, f_d(u))$, f_i smooth enough.
- Boundary conditions: Dirichlet or inflow/outflow depending on \mathbb{K}
- Scalar problem



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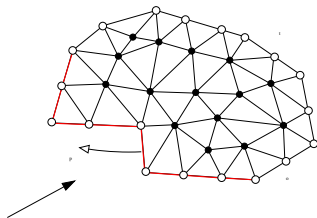
- $\mathbf{f}(u) = (f_1(u), \dots, f_d(u))$, f_i smooth enough.
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Analysis done for non viscous problems first



MODEL PROBLEM, FRAMEWORK FOR SCALAR CONSERVATION LAWS.

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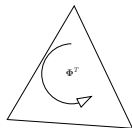
SOME NOTATIONS...

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$$u_h = \sum_i \varphi_i u_i$$

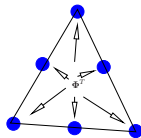
PRINCIPLE FOR HIGHER ORDER

1. $\forall K \in \mathcal{T}_h$ compute : $\Phi^K = \int_{\partial K} f_h(u_h) \cdot \mathbf{n}$



2. Distribution :

$$\Phi^K(u^h) = \sum_{i \in K} \Phi_i^K$$



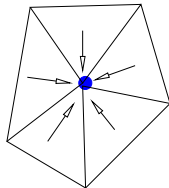
Distribution
coeff.s :

$$\Phi_i^K(u^h) = \text{sub-residuals}$$

3. Compute nodal values :
solve algebraic system

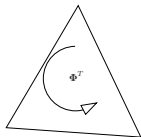
\forall degree of freedom i

$$\sum_{K|i \in K} \Phi_i^K(u^h) = 0,$$

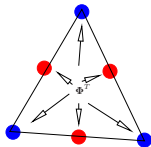


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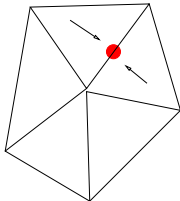


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Solved by some iterative technique.



DESIGN PROPERTIES

STRUCTURAL CONDITIONS, BASIC PROPERTIES

Under which conditions on the Φ_j^K s we get

- Correct weak solutions (if convergent with h)
- Formal k^{th} order of accuracy
- Monotonicity (discrete max principle)
- Convergence



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Notation: DOF: σ_i or M_i or simply i



CONDITION 1 : CONSERVATION

CONSERVATION PRINCIPLE

If there is a f_h , continuous approximation of f such that

$$\Phi^K = \sum_{j \in K} \Phi_j^K = \oint_{\partial K} \mathbf{f}(u^h) \cdot \mathbf{n}$$

Implies convergence to a (weak) solution of the problem
 $\operatorname{div} \mathbf{f}(u) = 0$

under standard stability conditions



CONDITION 2 : ACCURACY.

$u^{ex,h}$ interpolant of exact sol. assumed smooth

Truncation error

$$\mathcal{E}(u^{ex,h}; v) := \sum_{i \in \mathcal{T}_h} v_i \left(\sum_{K | i \in K} \Phi_i^K(u^{ex,h}) \right)$$

GUIDING PRINCIPLE

$$\mathcal{E}(u^{ex,h}; v) = \overbrace{\int_{\Omega} \nabla v_h \cdot f_h(u^{ex,h})}^{I \equiv \mathcal{E}^{\text{Galerkin}}} + \overbrace{\sum_{K \in \mathcal{T}_h} \frac{1}{N_K} \sum_{i,j \in K} (v_i - v_j)(\Phi_i^K - \Phi_i^{\text{Gal}})(u^{ex,h})}^{II}$$

$$\Phi_i^{\text{Gal},K} = \int_K \Phi_i \operatorname{div} f(u^h) dx = - \int_K \nabla \Phi_i \cdot \mathbf{f}(u^h) dx + \int_{\partial K} \Phi_i \mathbf{f}(u^h) \cdot \mathbf{n} d\sigma$$



CONDITION 2 : ACCURACY.

KEY REMARK

$$\operatorname{div} \mathbf{f}(w) = 0 \implies \Phi_i^{\text{Gal}, K}(u^{\text{ex}, h}) = \int_T \nabla \psi_i \cdot \mathbf{f}_h(u^{\text{ex}, h}) dx - \int_{\partial K} \Phi_i \mathbf{f}_h(u^{\text{ex}, h}) \cdot \mathbf{n} = O(h^{k+d})$$



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FINAL RESULT

$$\text{Truncation error : } |\mathcal{E}(u^{\text{ex}, h}; v)| \leq C'(\mathcal{T}_h, u^{\text{ex}}) \|\nabla v\|_{\infty} h^{k+1}$$

$$\text{if (in d-D) } |\Phi_i^K(u^{\text{ex}, h})| \leq C''(\mathcal{T}_h, u^{\text{ex}}) h^{k+d} = \mathcal{O}(h^{k+d})$$



CONDITION 2 : ACCURACY

“LINEARITY” (ACCURACY) PRESERVING SCHEMES

Since $\Phi^K(u^h) = \int_{\partial K} f^h(u^h) \cdot \mathbf{n} = \mathcal{O}(h^{k+d})$ schemes for which

$$\Phi_i^K = \beta_i^K \Phi^K \quad \text{with } \beta_i^K \text{ uniformly bounded distribution coeff.s}$$

are formally $k + 1^{\text{th}}$ order accurate (for $k + 1^{\text{th}}$ order spatial interpolation)



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The β_i^K must depend on the solution : *A scheme cannot be both high order accurate and linear for a linear problem.*



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SOLUTION METHOD

- Start from a monotone scheme
- Use a 'limiter' that produce a set of residuals that enables the residual property for any elements and any degree of freedom



ONE EXAMPLE OF MONOTONE SCHEME: THE RUSANOV SCHEME (LOCAL LAX FRIEDRICHS)

First order distribution :

$$\Phi_i^{\text{Rv}} = \frac{\Phi^K}{n_K} + \frac{\alpha}{n_K} \sum_{\substack{j \in K \\ j \neq i}} (u_i - u_j), \quad \alpha \geq \max_{j \in K} \left| \int_K \nabla_u f(u^h) \cdot \nabla \psi_j \right|$$

- n_K number of DoF per element
- φ_j Lagrange basis fcn. relative to node j

WHY THIS SCHEME ?

1. The Rv scheme is cheap and has general formulation
2. The Rv scheme is monotone and energy stable in the P^1 case.
3. By far one of the most dissipative ones



ONE EXAMPLE OF MONOTONE SCHEME: THE RUSANOV SCHEME (LOCAL LAX FRIEDRICHS)

Choice of Rusanov : not essential at all !

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SOLUTION METHOD SUMMARY

- For any K
- Start from Rusanov' residuals,
- Use Struijs' limiter

$$\beta_i^H = \frac{\max(0, \phi_i^{Rv} / \phi^K)}{\sum_{j \in K} \max(0, \phi_j^{Rv} / \phi^K)}$$

- Define: $\phi_i^H = \beta_i^H \phi^K$.
- $\theta = 0$ is u_i is a local extrema, $u_i = 1$ else
- This scheme satisfies a local maximum/minimum property and is formally k -th order accurate



SOLUTION METHOD

SUMMARY

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- Define:
$$\Phi_i^H = \beta_i^H \Phi^K + \theta(u^h) \times h_K \int_K (\nabla \mathbf{f}_u(u^h) \cdot \nabla \varphi_i)_T (\nabla \mathbf{f}_u(u^h) \cdot \nabla u^h) dx$$
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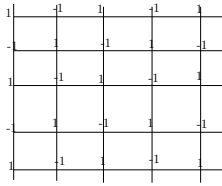
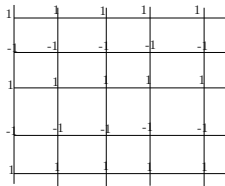
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MOTIVATION FOR THIS TERM

SOLVE $\frac{\partial u}{\partial x} = 0$ ON $[0, 1]^2$



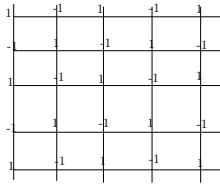
- In both cases, $\Phi^K = 0$: these are steady solutions when $\Phi_i^H = \beta_i^K \Phi^K$.
- Cure :

$$\Phi_i^{H,K} = \beta_i^K \Phi^K \longrightarrow \beta_i^K \Phi^K + \theta(u^h) \times h_K \int_K (\nabla f_u(u^h) \cdot \nabla \varphi_i) \tau (\nabla f_u(u^h) \cdot \nabla u^h) dx$$



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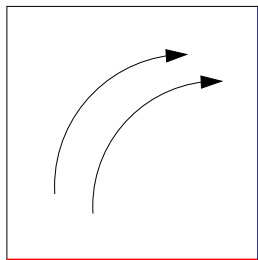


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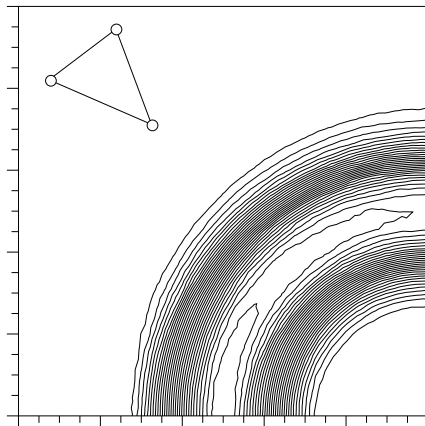
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NUMERICAL EXAMPLE : ROTATION

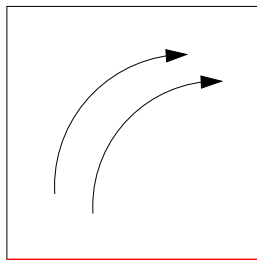


u
v

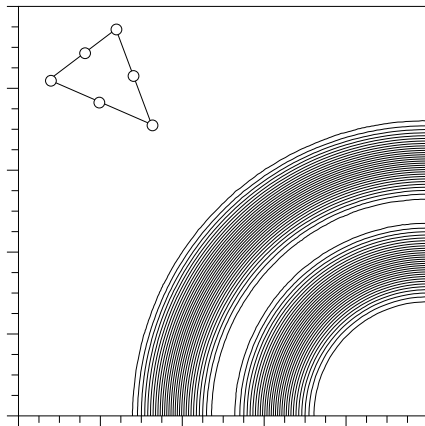




NUMERICAL EXAMPLE : ROTATION

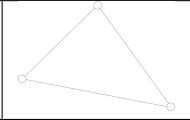
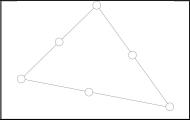
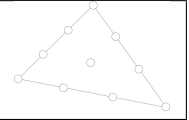


u
v





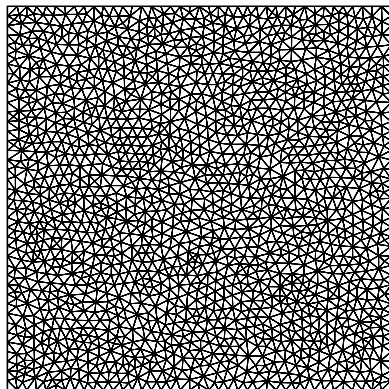
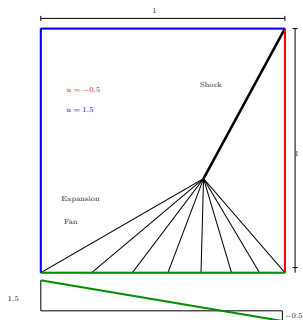
GRID CONVERGENCE

			
h	$\epsilon_{L^2}(P^1)$	$\epsilon_{L^2}(P^2)$	$\epsilon_{L^2}(P^3)$
1/25	0.50493E-02	0.32612E-04	0.12071E-05
1/50	0.14684E-02	0.48741E-05	0.90642E-07
1/75	0.74684E-03	0.13334E-05	0.16245E-07
1/100	0.41019E-03	0.66019E-06	0.53860E-08
	$\mathcal{O}_{L^2}^{1s} = 1.790$	$\mathcal{O}_{L^2}^{1s} = 2.848$	$\mathcal{O}_{L^2}^{1s} = 3.920$



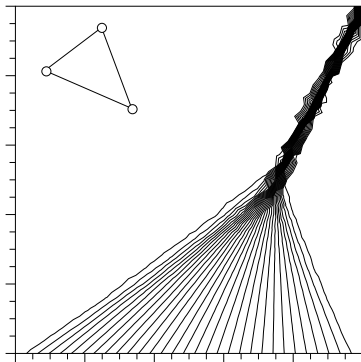
NUMERICAL EXAMPLE : BURGER'S EQ.N

$$\nabla \cdot \left(\frac{u^2}{2}, u \right) = 0$$

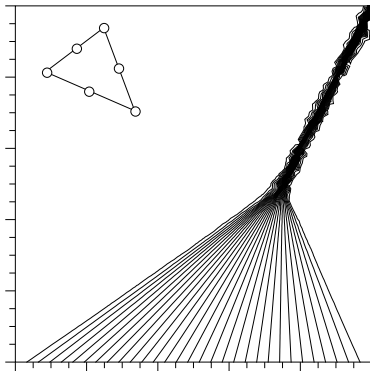




NUMERICAL EXAMPLE : BURGER'S EQ.N



LxF+PSI+Filter scheme, P^1 interpolation



LxF+PSI+filter scheme, P^2 interpolation

Shock captured in 1 or 2 cells



ALGORITHM

The scheme consists in 4 steps :

1. Evaluate the total residual, local (continuous interpolant)
2. Evaluate monotone residual (Rusanov) : local,
3. Evaluate high order residual : local
4. Gather residual : indirections, importance of good numbering of the degrees of freedom

The scheme is local and easy to parallelise

SOLUTION METHOD

Jacobian free + LUSGS-ILU



RD WITH VISCOUS TERMS: WHAT ARE THE PROBLEMS?

$$\operatorname{div} \mathbf{f}^a(\mathbf{u}) - \operatorname{div} (\mathbb{K}(\mathbf{u}) \cdot \nabla \mathbf{u}) = \operatorname{div} (\mathbf{f}^a(\mathbf{u}) - \mathbb{K}(\mathbf{u}) \cdot \nabla \mathbf{u}) = 0$$

- Accuracy: coupling of convection and diffusion: one single operator
- Total residual:

$$\Phi^K(u^h) = \int_{\partial K} (\mathbf{f}^a(\mathbf{u}) - \mathbb{K}(\mathbf{u}^h) \nabla u^h) \cdot \mathbf{n} d\partial K.$$

- Major issue: ∇u^h not single valued on edges.
- Reconstruct the gradients using out-of-element information, and keeping the compactness of the stencil
- experimental fact: ∇u^h should be reconstructed with the same accuracy as $u^h \dots$



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GRADIENT RECOVERY

IDEA

- Obtained from super-convergent patch recovery introduced by O. C. Zienkiewicz and J. Z. Zhu, *Int. J. Numer. Meth. Eng.*, 33, 1992:
Use of superconvergent points: $\nabla u^h(x_q) - \nabla u(x_q) = O(h^{k+1})$
instead of $O(h^k)$ as it should be
- Local least square to get high order ($O(h^{k+1})$) approximations of ∇u at Lagrange points
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LINEAR ADVECTION-DIFFUSION EQUATION

$$\mathbf{a} \cdot \nabla \mathbf{u} = \nu \operatorname{div} (\nabla \mathbf{u}), \quad \text{on } \Omega = [0, 1]^2,$$

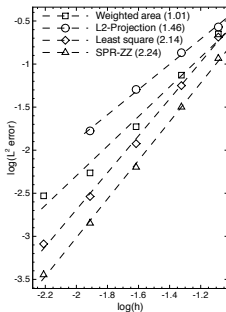
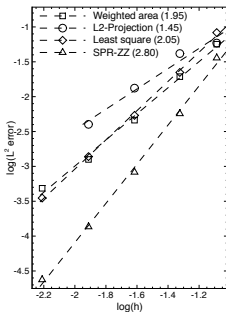
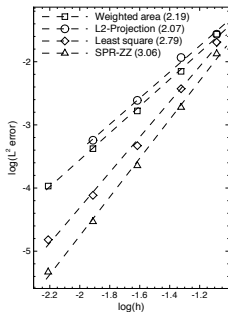
the exact solution of the problem reads

$$u = -\cos(2\pi\eta) \exp\left(\frac{\xi \left(1 - \sqrt{1 + 16\pi^2\nu^2}\right)}{2\nu}\right),$$

with $\eta = a_y x - a_x y$ and $\xi = a_x x + a_y y$. Here $\mathbf{a} = (0, 1)^K$ and $\nu = 0.01$



LINEAR ADVECTION-DIFFUSION EQUATION



L^2 error in the solution of the linear advection-diffusion problem on triangular grids with quadratic elements. Error of the solution (first column), error of the x -component of the gradient (second column) error of the y -component of the gradient (third column).



ANISOTROPIC PURE DIFFUSION

$$-\operatorname{div}(\mathbb{K}\nabla \mathbf{u}) = 0, \quad \text{on } \Omega = [0, 1]^2,$$

with

$$\mathbb{K} = \begin{pmatrix} 1 & 0 \\ 0 & \delta \end{pmatrix},$$

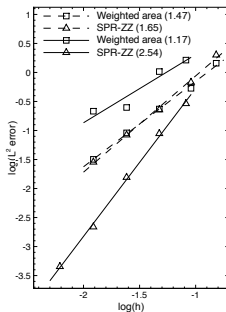
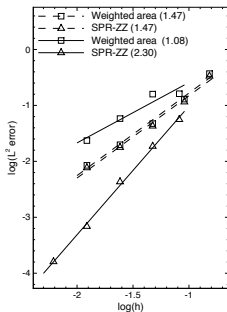
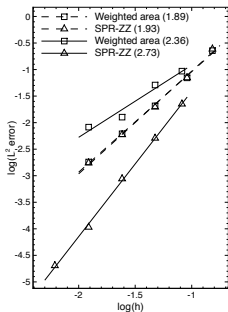
the problem has the following exact solution

$$\mathbf{u} = \sin(2\pi x) e^{-2\pi y \sqrt{1/\delta}},$$

and in the numerical simulations $\delta = 10^3$.



ANISOTROPIC DIFFUSION



L^2 error in the solution of the anisotropic diffusion problem on triangular grids with linear (dashed lines) and quadratic (solid lines) elements. Error of the solution (first column), error of the x-component of the gradient (second column) error of the y-component of the gradient (third column).



OVERVIEW

FORMULATIONS: CONSERVATION AND ACCURACY ISSUES

RESIDUAL DISTRIBUTION FRAMEWORK

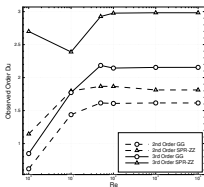
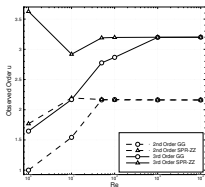
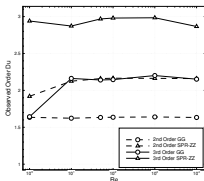
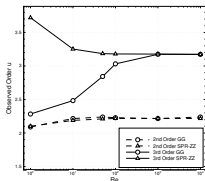
APPLICATION TO STEADY TURBULENT FLOW PROBLEMS

EXTENSIONS: SHALLOW WATER

CONCLUSION



MANUFACTURED SOLNS: ACCURACY TEST SOL MADE OF TRIGS FUNCTIONS

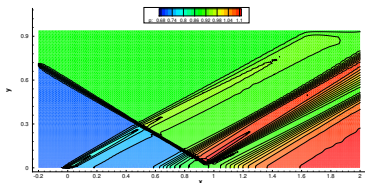


Observed order

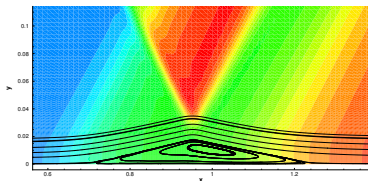
- Top: linear scheme;
- Bottom: non linear scheme
- Left: error on solution;
- Right: error on gradients

SHOCK-WAVE/LAMINAR BOUNDARY LAYER INTERACTION

$M=2.15$, $\theta = 30, 8^\circ$, $Re = 10^5$



(a)



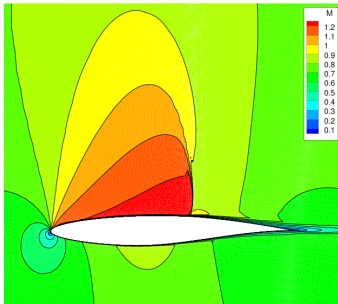
(b)

FIGURE : Left: contours of the pressure obtained with the third order scheme for the shock/boundary layer interaction. Right: zoom of the solution near the impinging point of the shock with the boundary layer, streamlines are also reported to show the separation bubble.

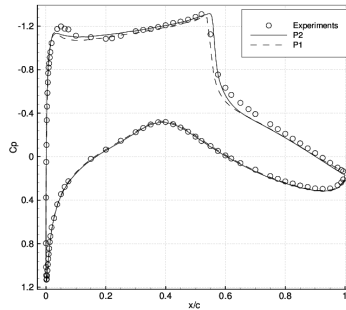


RAE2822 AIRFOIL, TURBULENT

$M=0.734$, $Re=6.5 \cdot 10^6$, $AOA=2.79^\circ$



Mach

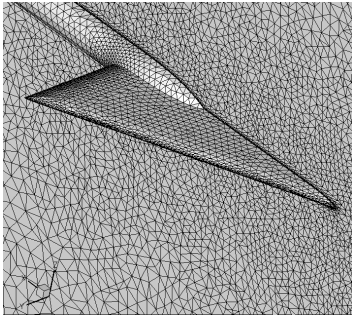


Pressure

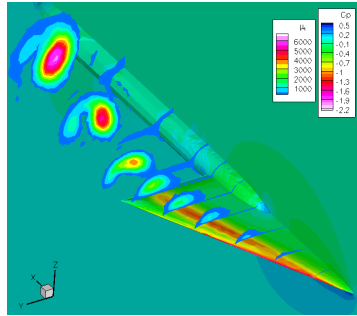


DELTA WING, TURBULENT, IDIHOM PROJECT

$M=0.734$, $Re=6.5 \cdot 10^6$, $AOA=2.79^\circ$



Mesh

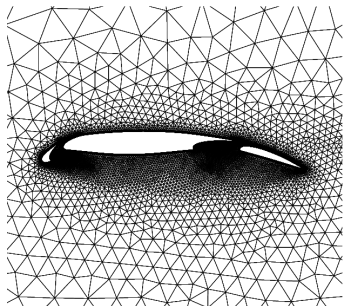


Pressure

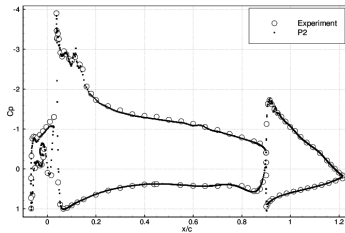


L1T2 AIRFOIL, TURBULENT

$M=0.197$, $Re=3.52 \cdot 10^6$, $AoA=4.01^\circ$



Mesh

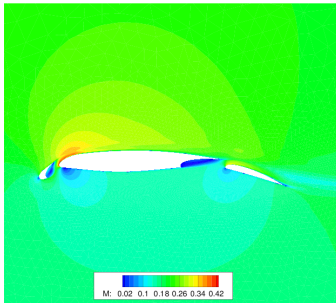


Mach

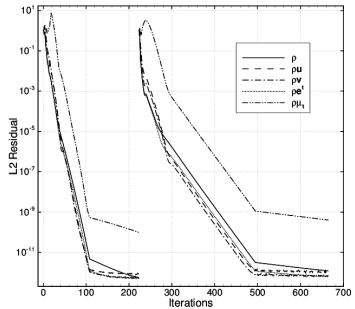


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$M=0.197$, $Re=3.52 \cdot 10^6$, $AoA=4.01^\circ$



Mach

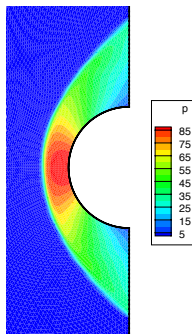


convergence history



HYPERSONICS

$$M = 10, Re = 3 \times 10^5, T_{wall}, \mathbb{P}^2$$

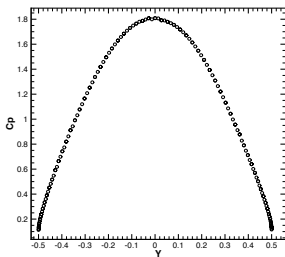


Pressure contour

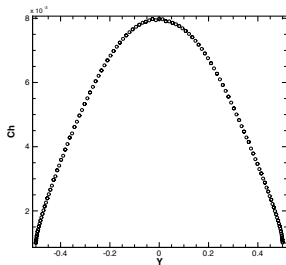


HYPERSONICS

$M = 10, Re = 3 \times 10^5, T_{wall}, \mathbb{P}^2$



C_p



heat transfert



OVERVIEW

FORMULATIONS: CONSERVATION AND ACCURACY ISSUES

RESIDUAL DISTRIBUTION FRAMEWORK

APPLICATION TO STEADY TURBULENT FLOW PROBLEMS

EXTENSIONS: SHALLOW WATER

CONCLUSION



SHALLOW WATER, MODEL

$$\frac{\partial W}{\partial t} + \operatorname{div} \mathbf{f}(W) - S(x, W) = 0$$

- $W = (h, h\mathbf{u})$, $S(x, W)$ depends on the bathymetry and W
- issues:
 - “lake at rest problem”, i.e. and coupling between $\operatorname{div} \mathbf{f}$ and S
 - $h \geq 0$: dry bed

Shallow water: Mario Ricchiuto (INRIA)



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Total residual to be distributed:

$$\Phi^K = \int_{\partial K} \mathbf{f}(u^h) \cdot \mathbf{n} - \int_K S(x, u^h)$$

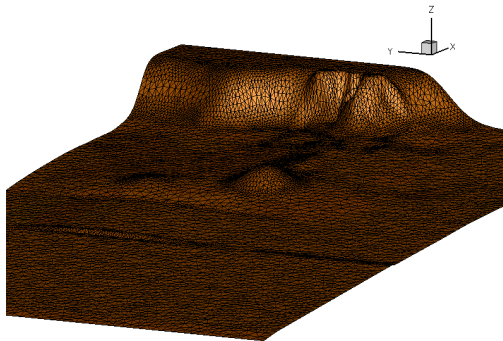
plus coherent integration formula for accuracy

Shallow water: Mario Ricchiuto (INRIA)



OKUSHIRI TSUNAMI EXPERIMENT

3rd Int. workshop on long-wave run-up models. Bathymetry, inlet wave profile, experimental data on the workshop web.



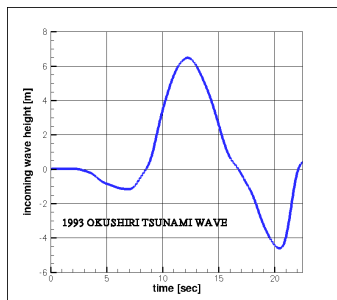


OKUSHIRI TSUNAMI EXPERIMENT

3rd Int. workshop on long-wave run-up models. Bathymetry, inlet wave profile, experimental data on the workshop web.

Parameters :

- Amplitude : $\pm 10\%$, uniform PDF
- Manning coefficient : $\pm 50\%$, uniform PDF
- Wave phase : $\pm 10\%$, uniform PDF



UQ: Pietro-Marco Congédo (INRIA)



OKUSHIRI TSUNAMI EXPERIMENT

Deterministic result (parameters prescribed in the workshop)

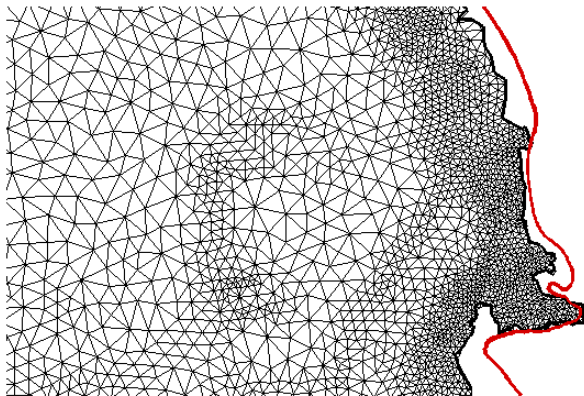


OKUSHIRI TSUNAMI EXPERIMENT

Deterministic result (parameters prescribed in the workshop)



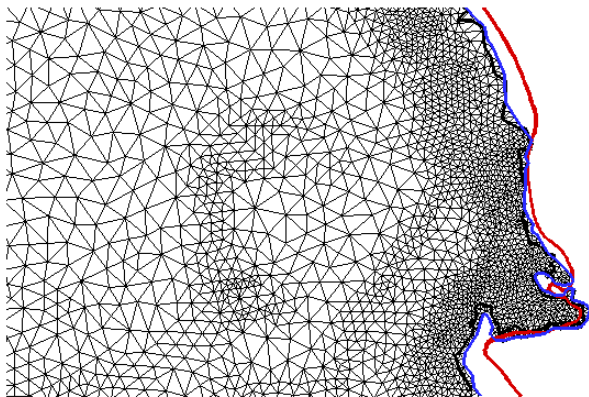
OKUSHIRI TSUNAMI EXPERIMENT



Deterministic result : run-up plot



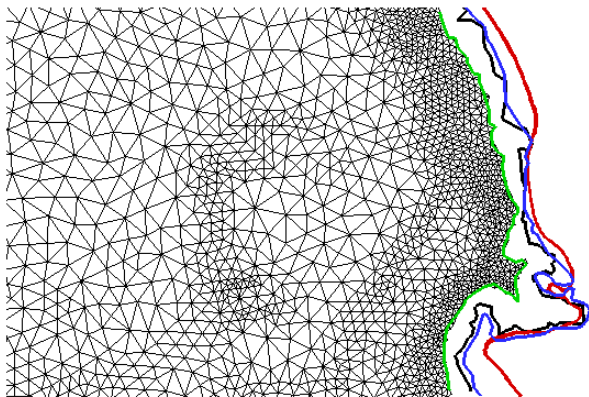
OKUSHIRI TSUNAMI EXPERIMENT



Deterministic run-up vs statistical average (mesh) plus deviation



OKUSHIRI TSUNAMI EXPERIMENT



Deterministic run-up vs statistical average (mesh) minus deviation



UNSTEADY SHOCK CALCULATION

Image !



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CONCLUSIONS

- High order finite element like method
- All see from the discrete point of view: no natural variational formulation
- in the scalar case: L^∞ and L^2 /entropy stable, and still formally high order
- Applications for compressible flows, turbulent, shallow water, ...
- Some perspective on $h - p$ adaption (in progress)
- Unsteady high order: in progress.

