

Sinus For Ever

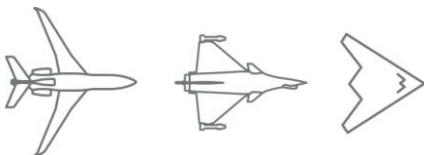
30 ans de simulation et optimisation aérodynamique

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HIGHER TOGETHER™



Aerodynamics Optimisation: Gradient computation



State equation $E(\mu, W(\mu)) = 0$

Cost function $j(\mu) = J(\mu, W(\mu))$

Constraints functions $g(\mu) = G(\mu, W(\mu))$

Minimizing $j(\mu)$ while respecting constraints $g_i(\mu) \leq 0$

We observe

$$f(\mu) = F(\mu, W(\mu)) = (J(\mu, W(\mu)), G(\mu, W(\mu)))$$

$$\mu = (v, l)$$

with l = aerodynamic parameters

and v = geometric parameters (CAD modeler)

*PDE control theory
J-L Lions
Dunod, 1968*

Aerodynamics Optimisation: Gradient computation



To estimate

$$\delta f = \frac{df(\mu)}{d\mu} \cdot \delta\mu = \frac{dF(\mu, W(\mu))}{d\mu} \cdot \delta\mu$$

$\mu = (v, l)$

$$\delta f = \frac{\partial F}{\partial W} \frac{\partial W}{\partial l} \cdot \delta l + \frac{\partial F}{\partial W} \frac{\partial W}{\partial v} \cdot \delta v + \frac{\partial F}{\partial l} \cdot \delta l + \frac{\partial F}{\partial v} \cdot \delta v$$

□ Thanks to the state equation

$$E(\mu, W(\mu)) = 0$$

□ and then

$$\delta E(\mu, W(\mu)) = \frac{\partial E}{\partial W} \cdot \delta W + \frac{\partial E}{\partial \mu} \cdot \delta\mu = 0$$

□ Thanks to the mesh deformation equation

$$L(d(v), D(v)) = 0$$

□ and then

$$\delta L(d(v), D(v)) = \frac{\partial L}{\partial d} \cdot \delta d + \frac{\partial L}{\partial D} \cdot \delta D = 0$$

Aerodynamics Optimisation: Gradient computation



□ Evaluate variations of the Lagrangian $\delta f^* = \delta f - \Psi(\mu)^T \delta E - \Phi(v)^T \delta L$

□ with

$$\left(\frac{\partial E}{\partial W}(l, D(v), W(\mu)) \right)^T \Psi(\mu) = \left[\frac{\partial F}{\partial W}(\mu, W(\mu)) \right]^T$$

$$\frac{\partial F}{\partial D}(l, D(v), W(\mu)) - \Psi^T \frac{\partial E}{\partial D}(l, D(v), W(\mu)) = \Phi^T \frac{\partial L}{\partial D}(d(v), D(v))$$

□ to obtain

$$\begin{cases} \frac{dF}{dl} = \frac{\partial F}{\partial l} - \Psi^T \left[\frac{\partial E}{\partial l} \right] \\ \frac{dF}{dv} = -\Phi^T \left[\frac{\partial L}{\partial d} \frac{\partial d}{\partial v} \right] \end{cases}$$

Aerodynamics Optimisation: Optimization techniques



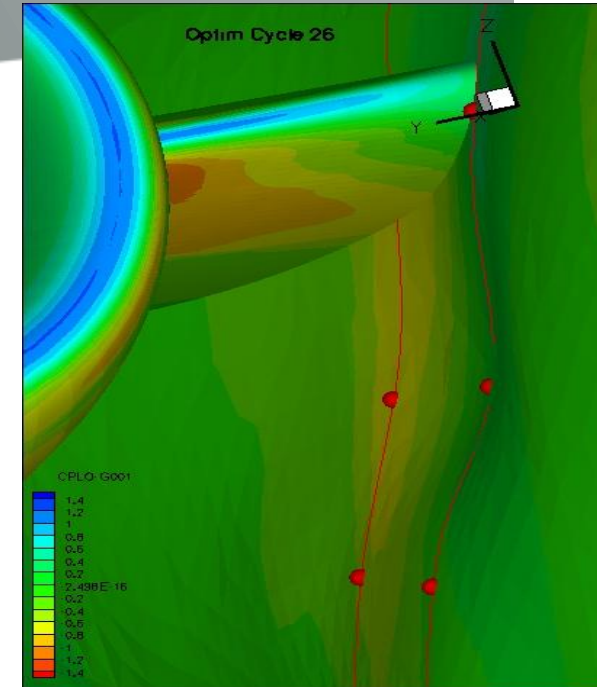
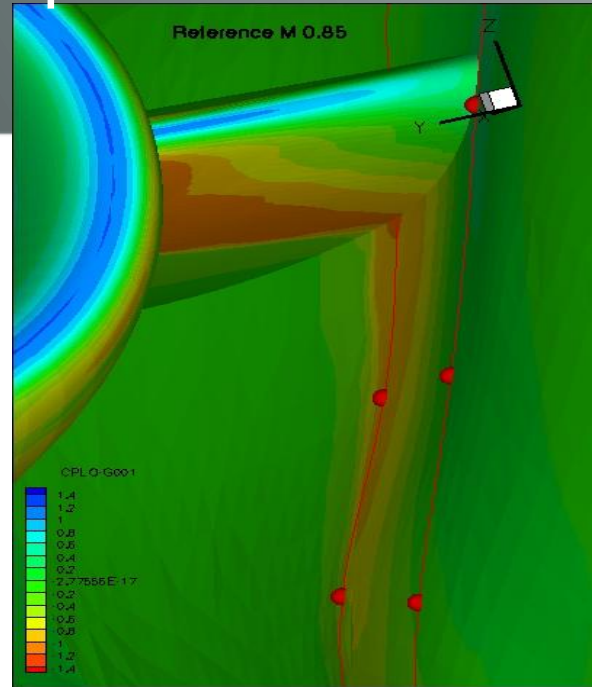
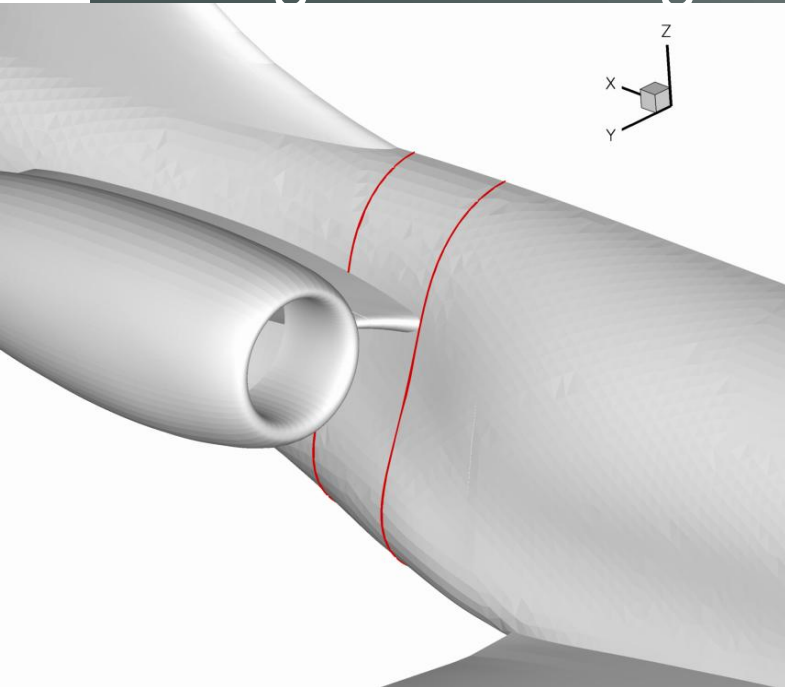
Automatic Differentiation software Tapenade (INRIA-Sophia-Antipolis).

Gradient-based optimization

Feasible (direction) Sequential Quadratic Programming

Feasible Arc Interior Point Algorithm (FAIPA) developed by Prof. J.N. Herskovits & co-workers

Aerodynamics Optimisation: Design of fuselage shape



Optimization based on 3D Navier-Stokes

Large degree of automatisisation required for the design of a complex area

Complex aerodynamics

Fully 3D shape design

Trade off with internal layout

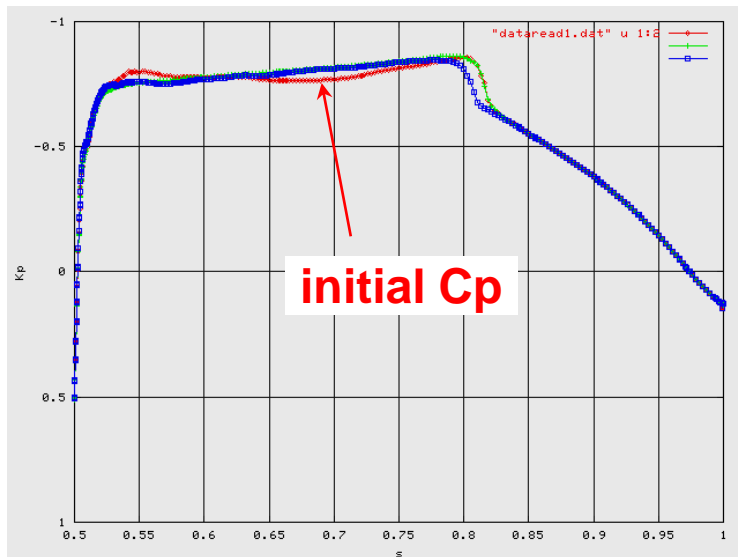
Automatic shape optimization

(2/5)

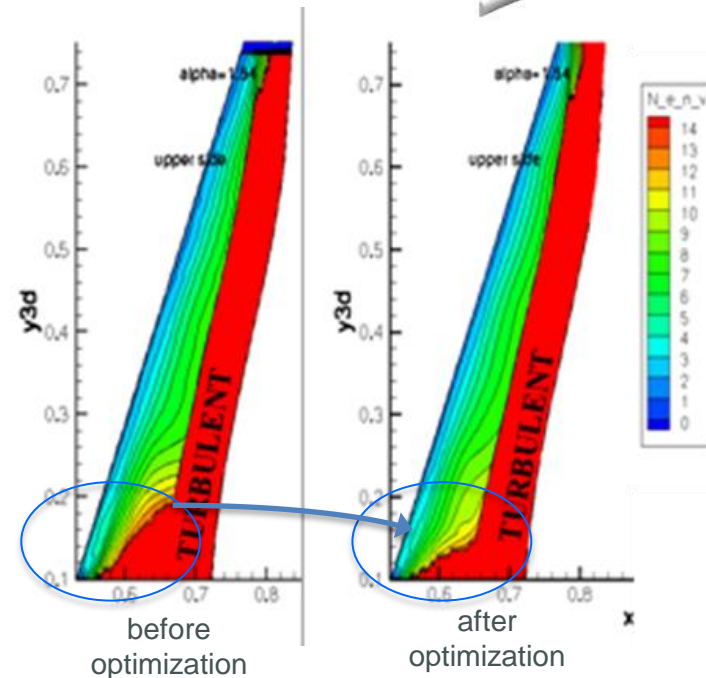


Laminar wing optimization to increase laminar area on wing next to the fuselage

- Laminar wing, $\Phi = 20^\circ$
- Mach = 0.75, angle of attack = 3°
- Objective : increase laminar area on wing next to the fuselage $\rightarrow C_p$ & $\delta C_p / \delta x$ target locally
- Leeward wing section profile
- Navier-Stokes with adjoint



Cp(x/c) – Laminar wing



Transition line on leeward side of ECO2 wing

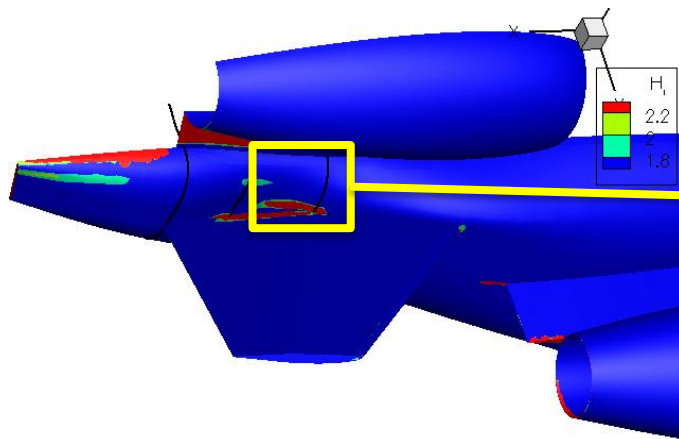
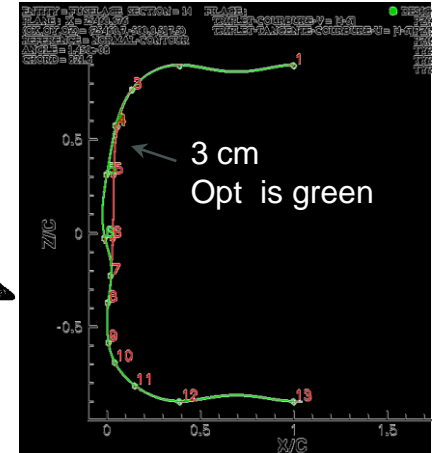
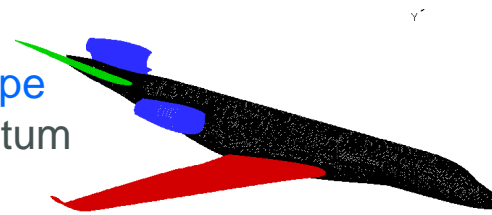
Automatic shape optimization (3/5)

Afterbody optimization of innovative configuration

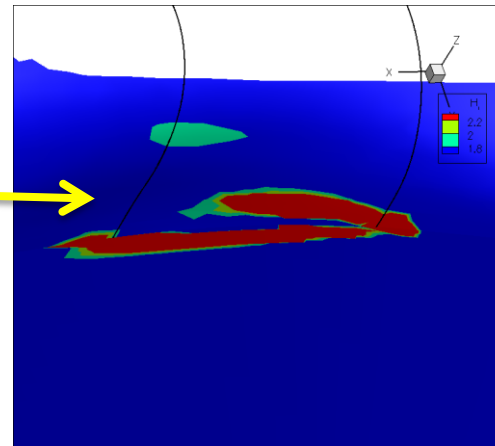
Example of complex objective functions



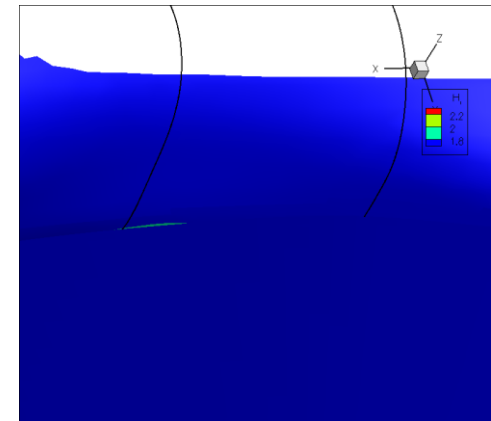
- Mach = 0.85, angle of attack = 1.5°
- Cost function is based on the boundary layer shape parameter H_i (ratio of displacement and momentum thickness)
- fuselage shape: 10 variables
- Adjoint approach - Convergence requires about 20 NS computations



Recirculation zone ($H_i > 2.2$) red

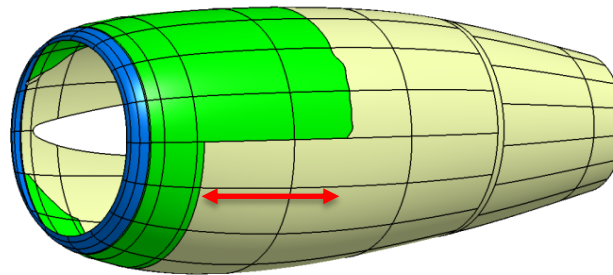


H_i before optimization

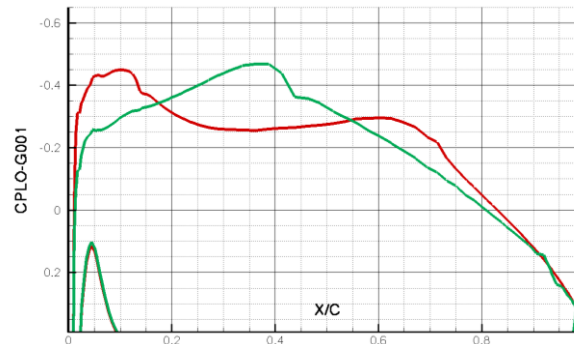


H_i after optimization

Optimisation nacelle laminaire



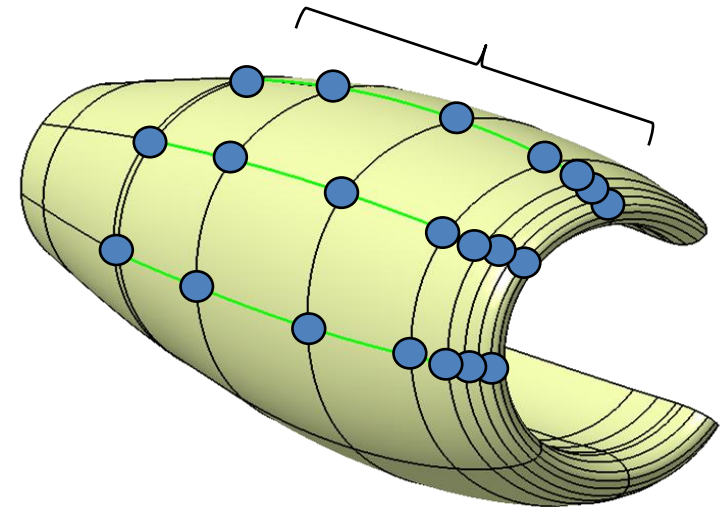
**M=0.85, Cz milieu croisière
Gain 1.2% traînée avion**



Laminarité ~ 40%

Extension de laminarité sur la partie supérieure d'une nacelle

Triplets libérés



Automatic shape optimization (4/5)

Low speed – high speed wing tip optimization

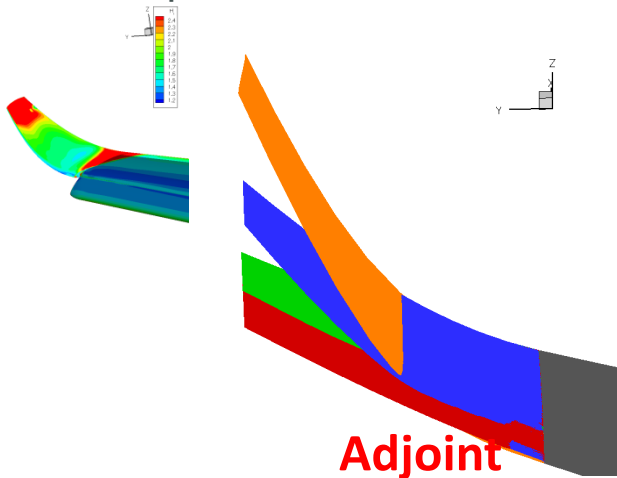
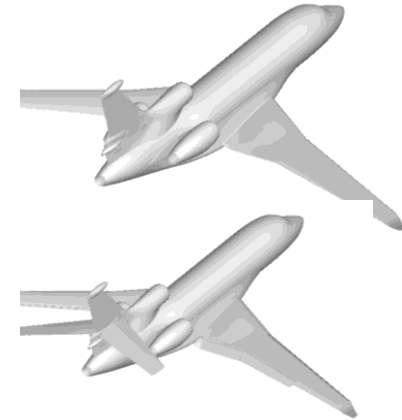


Multipoint optimization : low speed (Mach = 0.18, high lift configuration) – high speed (Mach = 0.8, cruise configuration)

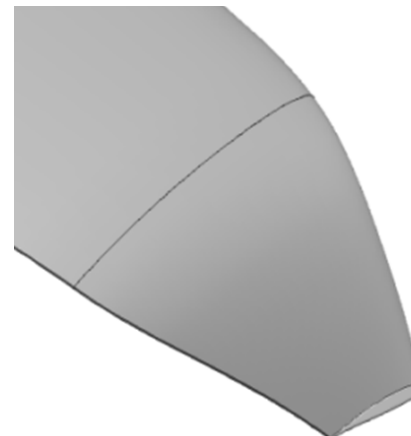
Minimize

- drag at high speed (constraints on lift +trimmed+ bending moment at $y = 8 \text{ m}$)
- surface $H_i > 2$ at low speed

Parameters: aoa (at High speed), twist, sweep angle, dihedral, thickness, span

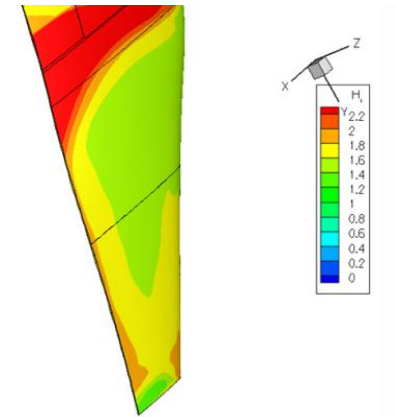


Adjoint



winglet shape proposed by multipoint optimization

1 % reduction of drag



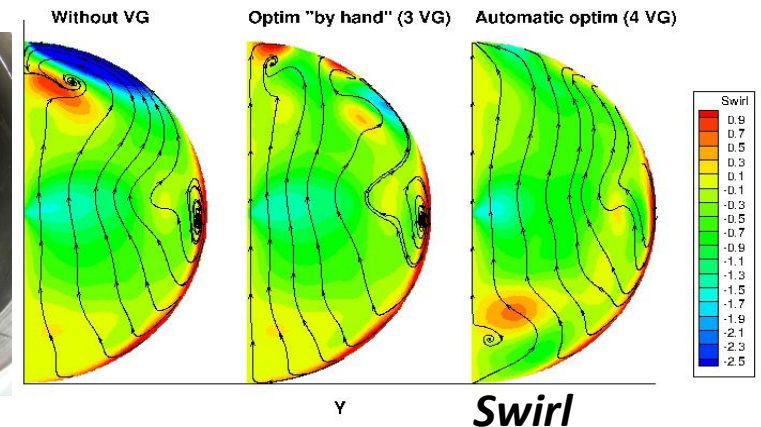
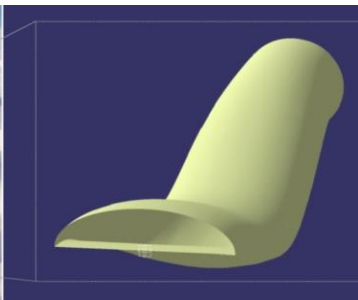
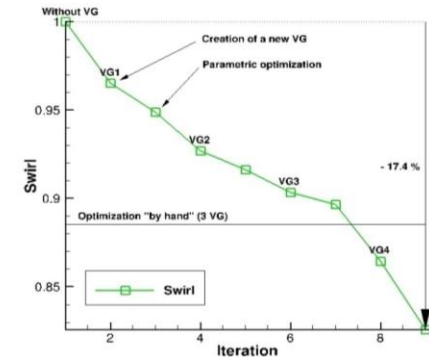
Boundary layer shape factor on the optimized winglet – high lift configuration

Automatic shape optimization (5/5)

Control and optimization of separated flows



- PhD thesis J. Chetboun : Dassault Aviation / Ecole Polytechnique / DGA.
- Development of automated methods for the control and the optimization of separated flows.
- Application to curved air ducts for UCAV.
- Use of mechanical or fluidic vortex generators (VG)
- Optimization: **topological** + shape

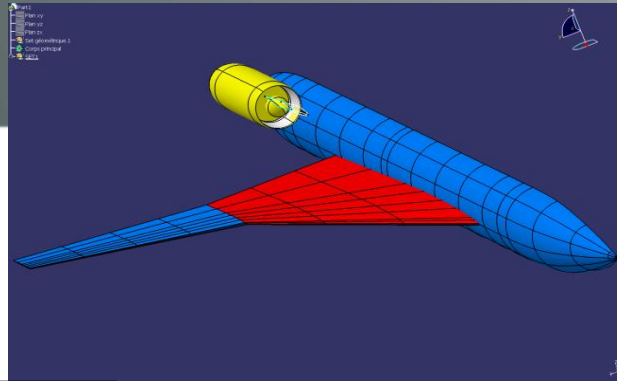


Engine integration optimization

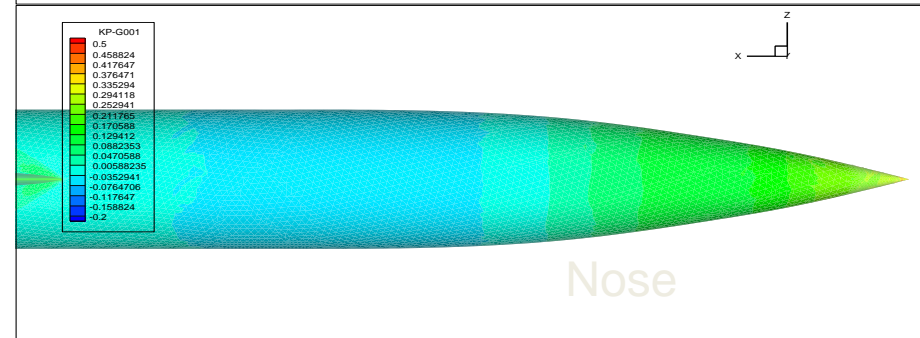
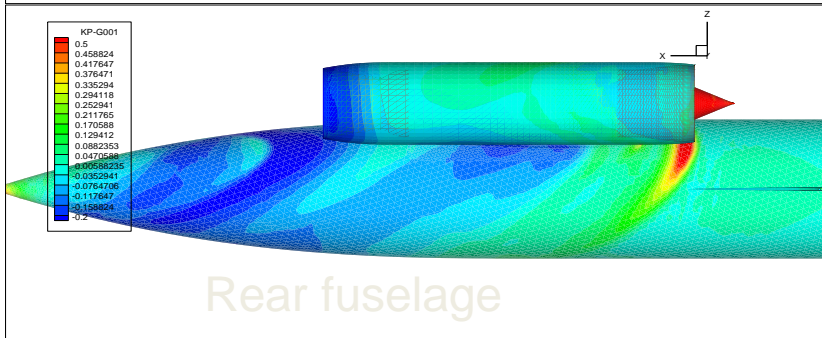
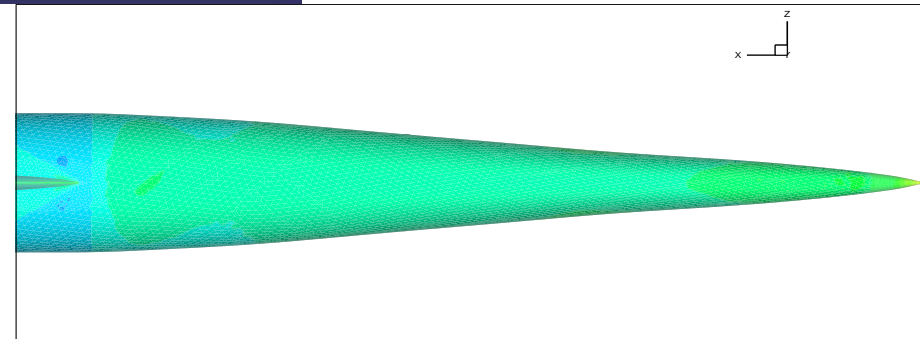
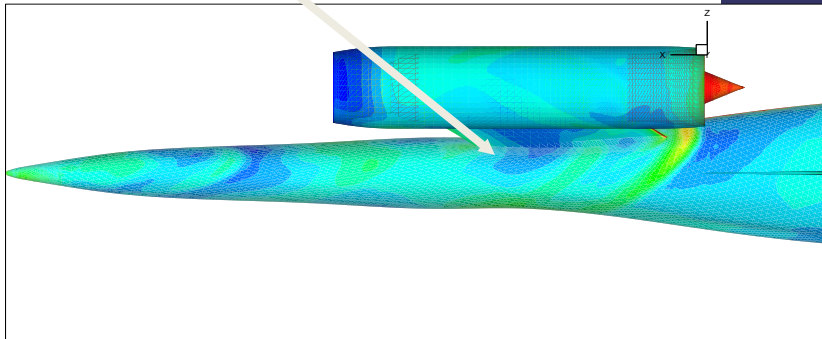


L'optimiseur ne devine pas les contraintes oubliées

HISAC project (IP - 6th FP)



Gain: 60 %
on zero-lift drag
Sears-Haack ...



Rear fuselage

Nose

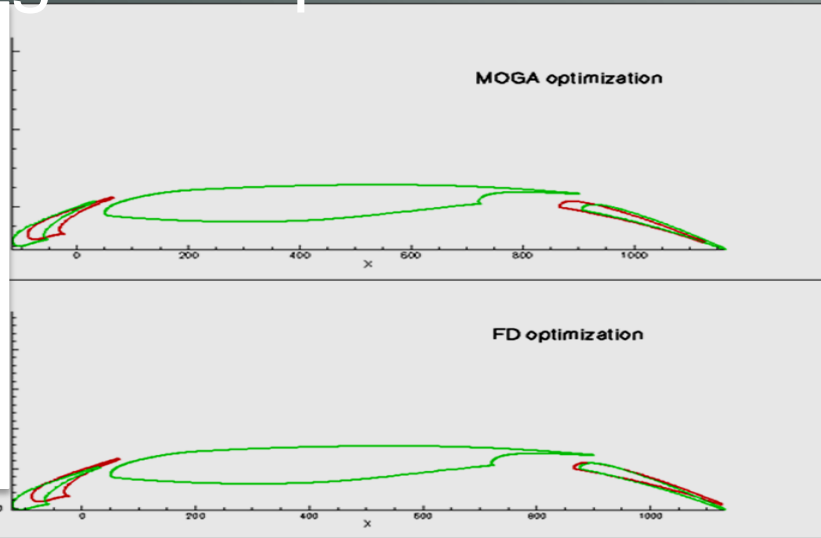
Optimization of High Lift configuration within European project DESIREH

(Design, Simulation and Flight Reynolds Number testing for advanced High Lift
Solutions)

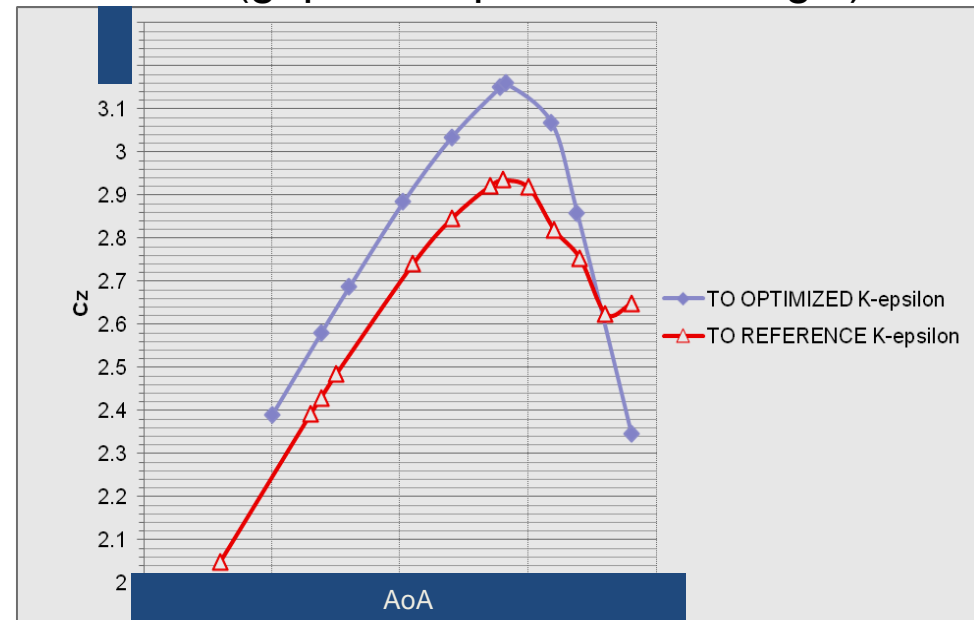
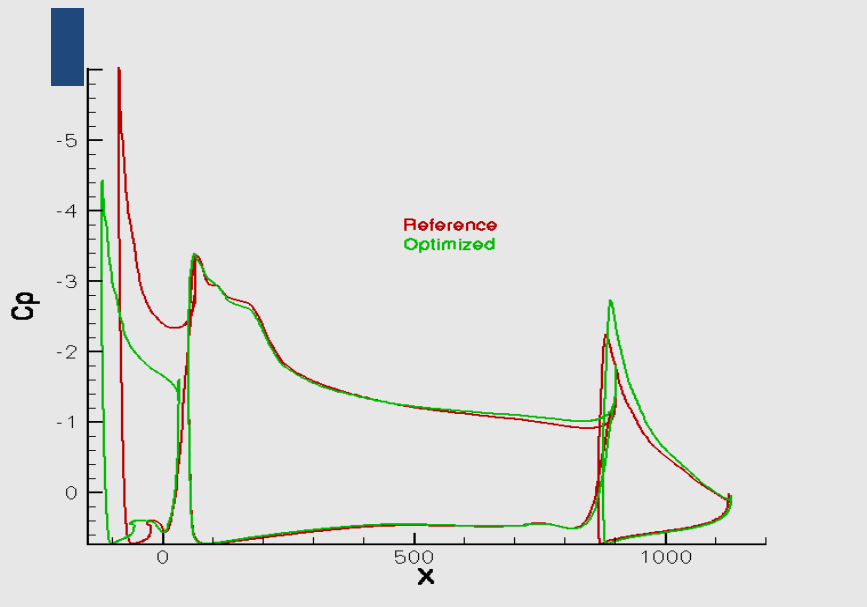
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EC – Grant Agreement N° ACP8-GA-2009-233607

Steven Kleinveld

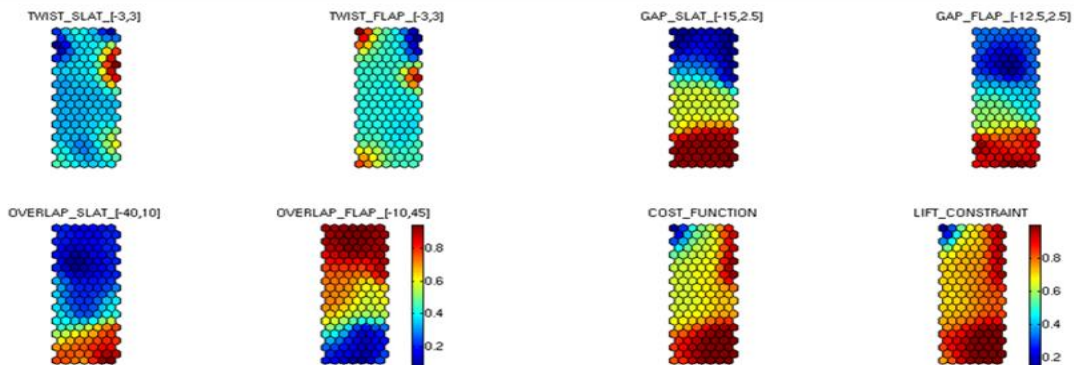
2.5D High Lift optimization



Example of performance improvement through optimization at Take-Off conditions for classical high lift configuration using setting variables (gap, overlap, deflection angle)



2.5D High Lift optimization



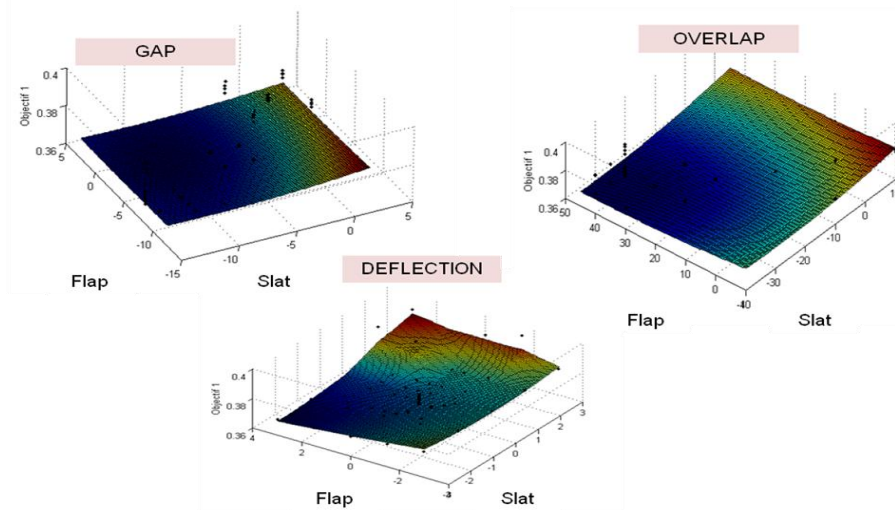
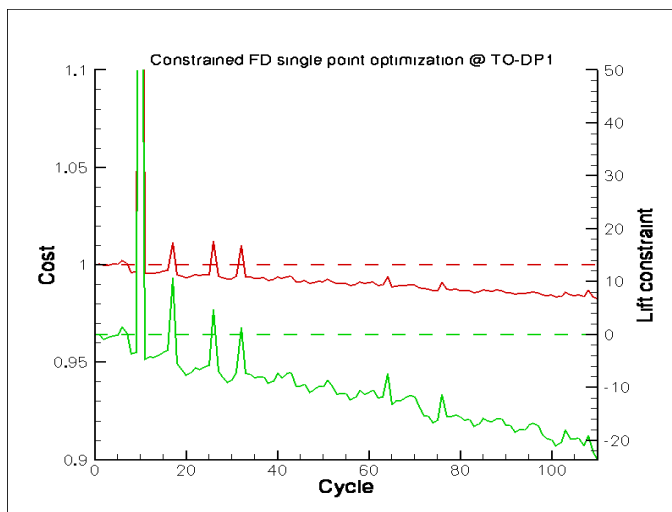
SOM

Use of various techniques to search for improved performance at take-off and landing

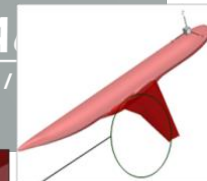
FD

$$\text{Cost Function } F(x) = F_{\text{reference}}(x) \quad [\equiv 1]$$

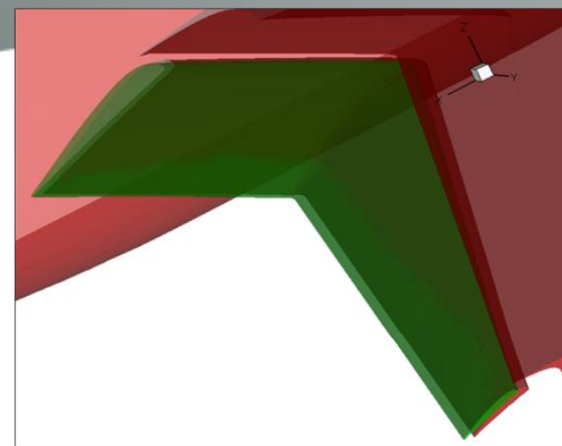
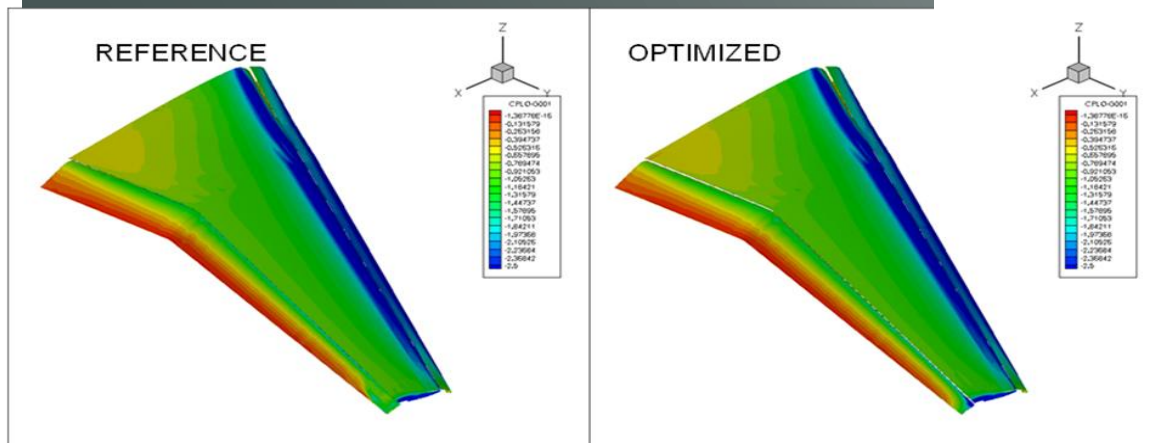
$$\text{Lift Constraint } g(x) = 0 \quad [\equiv 1]$$



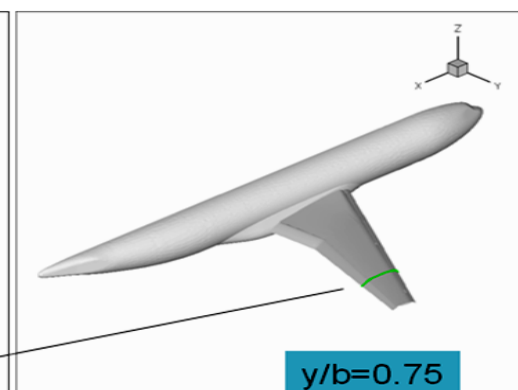
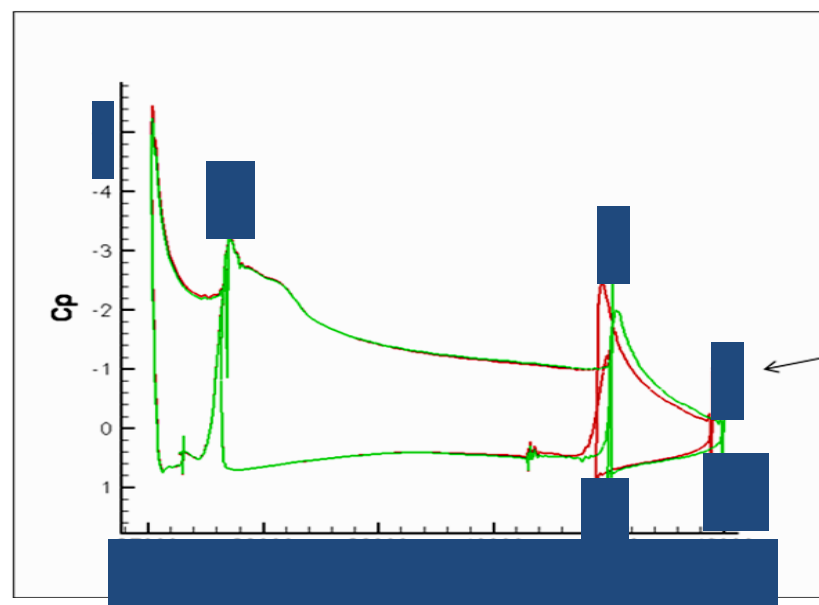
MOGA



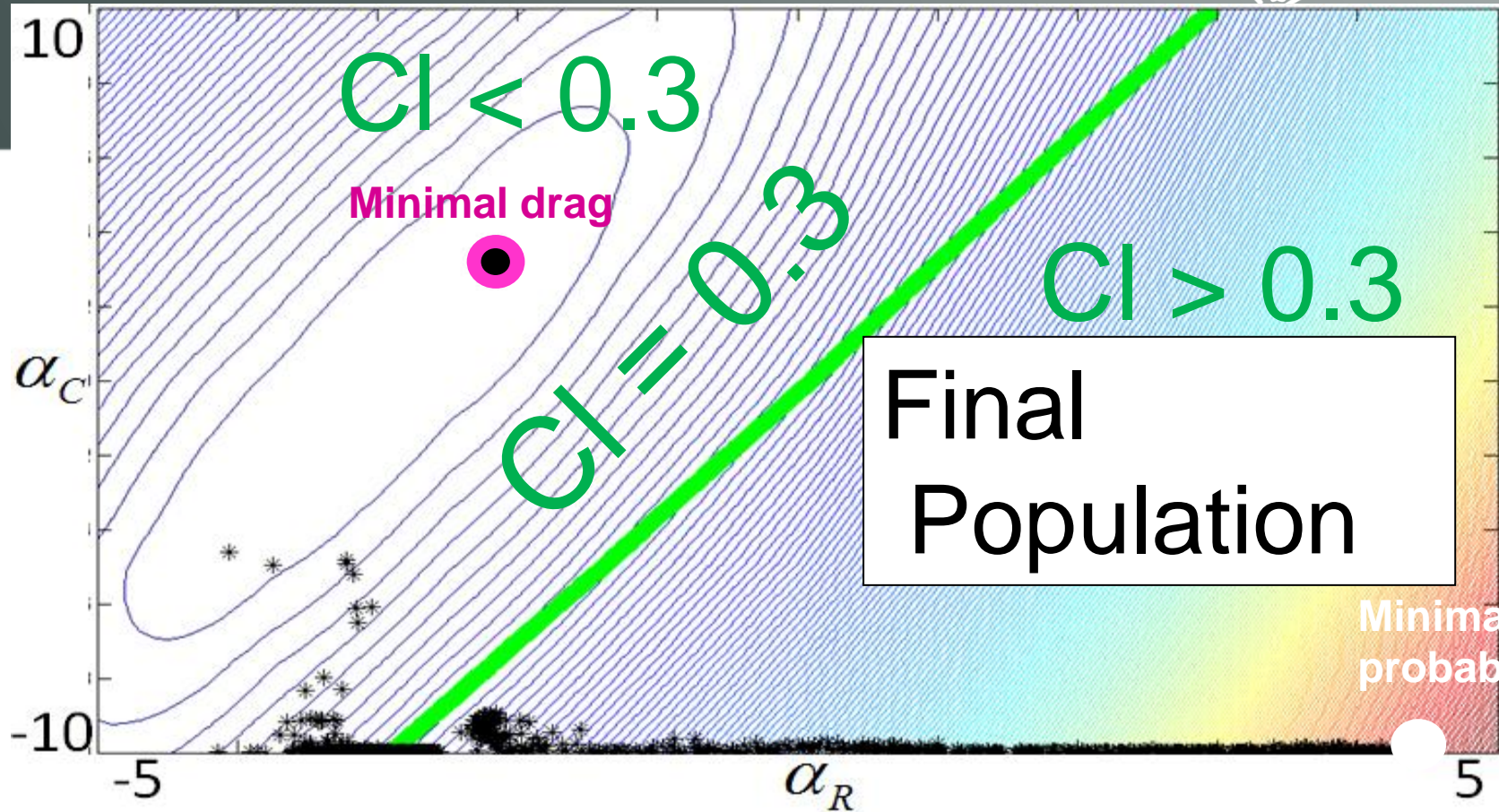
3D High Lift optimization



Example of flap position optimization at Take-Off conditions of 3D configuration taking into account variations of the intersection with fuselage

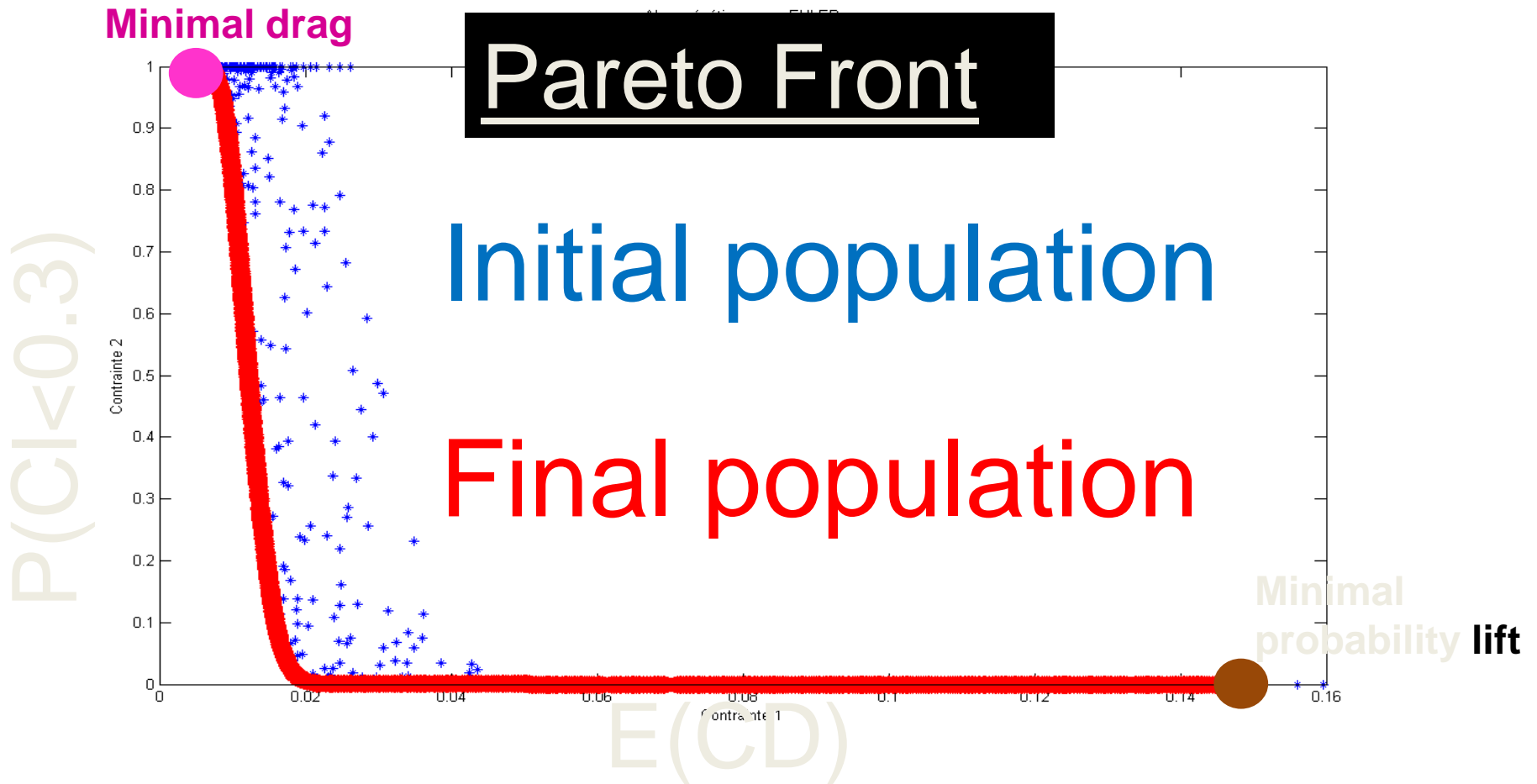


Robust Design (1)



ONERA M6 wing, 2 design parameters: twist and TE camber angles
Euler, RSM RBF like but with 1st and 2nd derivatives (original approach, Duchon extension)
MOGA, Robust design. Objectives: to control Drag and $P(Cl < 0.3)$

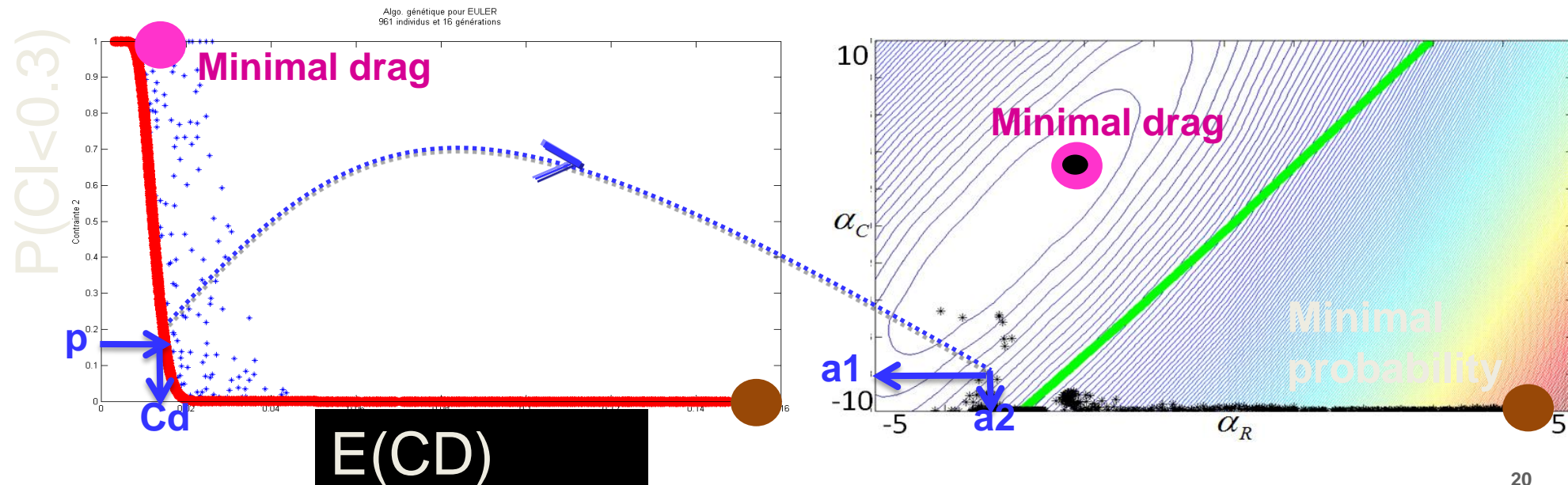
Robust Design (2)



Robust Design (3)

Decision: we accept a probability lift of $p = x\%$ with minimal drag

- Determination of drag mean **CD** (Pareto front)
- Determination of nominal values of geometrical parameters **a1** and **a2** (camber and twist angles)

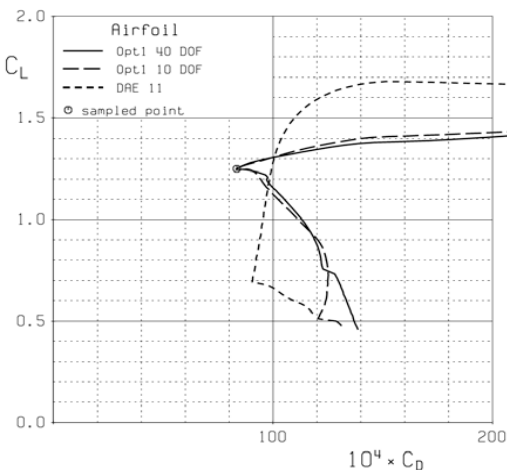


Robustesse – optimisation multipoints

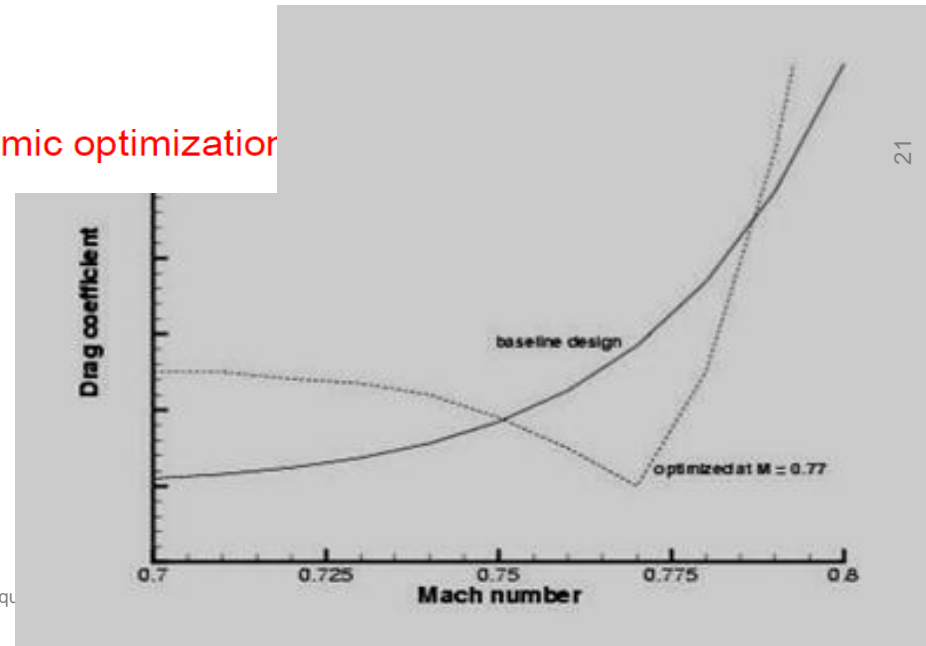
Need for a multi-mission approach

- The aircraft flies **multiple missions**, which implies
 - Multiple Mach numbers
 - Multiple Reynolds numbers
 - Large mass variations and then CI variations
- At the aerodynamic design phase, missions are not precisely known
- We know at this step the expected lift, Mach and Reynolds variation ranges

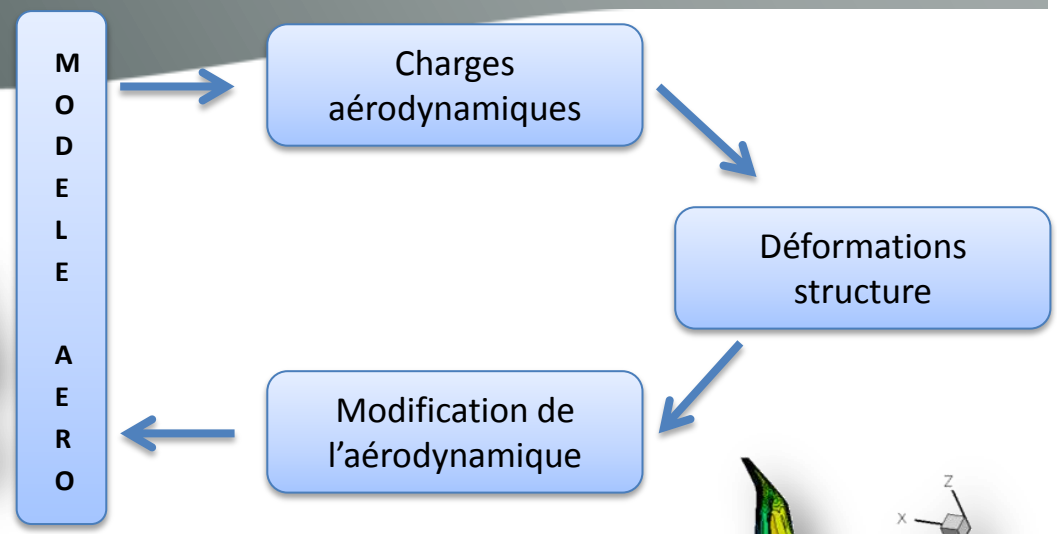
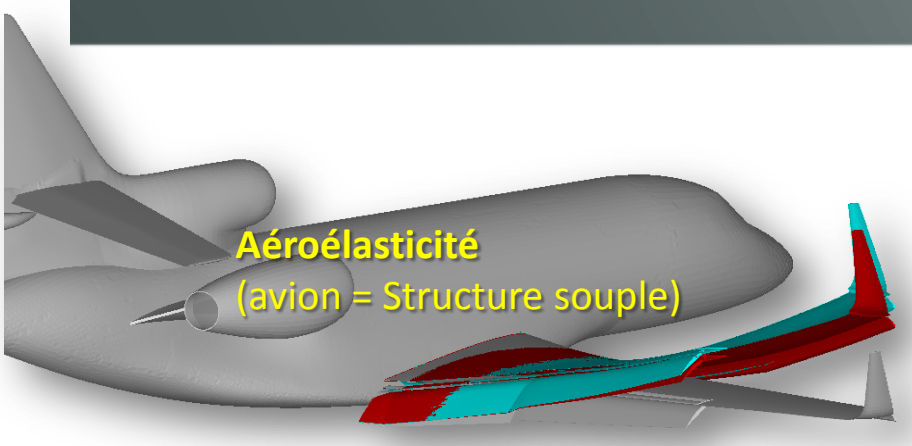
Need for a multi-lift, multi-Mach, multi-Reynolds aerodynamic optimization



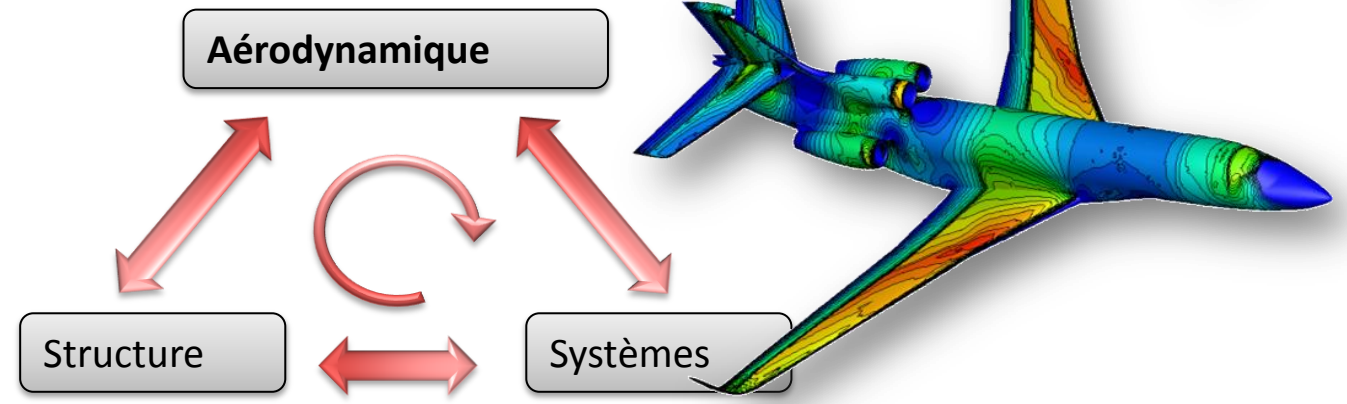
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Un domaine en interaction avec les autres disciplines



Boucle de conception



Analyse / Optimisation



Euler, Navier-Stokes,
Maxwell,
élastodynamique

Couplage fluide-
structure
(aéroelasticité),
aéroacoustique, ...



Analyse
Monodisciplinaire

Analyse avec
couplage entre 2
disciplines

Analyse
Multidisciplinaire
(MDA)



Optimisation
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