## Discontinuous Galerkin methods for solving Helmholtz isotropic wave equations for seismic applications <u>Advisors:</u> Stéphane Lanteri, INRIA, *Nachos* Julien Diaz, INRIA, *Magique 3D*

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2D Helmholtz isotropic elastic equations DG formulation of the equations Numerical results Conclusion-Perspectives



### Examples of the seismic applications



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#### Imaging method : the full wave inversion

• Quantitative high resolution images of the subsurface physical parameters

#### Forward problem of the inversion process

• Elastic waves propagation in harmonic domain : Helmholtz equation

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#### Seismic imaging in heterogeneous complex media

- Complex topography
- High heterogeneities

#### DG method

- Use of triangular unstructured meshes
- Flexible choice of interpolation orders (*p adaptativity*)

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- Flexible choice of interpolation orders (*p adaptativity*)

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#### Drawback of DG method

• Important computational cost

#### Main objective of the thesis

- Development of an hybridizable DG (HDG) method
- Development of a reference method, a classical DG method

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- Circular diffraction
  - Results for various frequencies
  - Results with the p adaptativity



Motivation 2D Helmholtz isotropic elastic equations DG formulation of the equations Numerical results





## 1 2D Helmholtz isotropic elastic equations

## 2D Helmholtz elastic equations

First order formulation of Helmoltz wave equations

 $\mathbf{x} = (x,y) \in \Omega \subset \mathbb{R}^2$  ,

$$\begin{cases} i\omega\rho(\mathbf{x})\mathbf{v}(\mathbf{x}) = \nabla \cdot \underline{\underline{\sigma}}(\mathbf{x}) + f_s(\mathbf{x}) \\ i\omega\underline{\underline{\sigma}}(\mathbf{x}) = \underline{\underline{C}}(\mathbf{x}) \underline{\underline{\varepsilon}}(\mathbf{v}(\mathbf{x})) \end{cases}$$

- Free surface condition :  $\underline{\sigma}\mathbf{n} = 0$  on  $\Gamma_I$
- Absorbing boundary condition :  $\underline{\sigma} \mathbf{n} = v_{\rho}(\mathbf{v} \cdot \mathbf{n})\mathbf{n} + v_{s}(\mathbf{v} \cdot \mathbf{t})\mathbf{t}$  on  $\Gamma_{a}$
- v : velocity vector
- $\underline{\sigma}$  : stress tensor
- $\underline{\varepsilon}$  : strain tensor

## 2D Helmholtz elastic equations

First order formulation of Helmoltz wave equations

 $\mathbf{x} = (x, y) \in \Omega \subset \mathbb{R}^2$  ,

$$\begin{cases} i\omega\rho(\mathbf{x})\mathbf{v}(\mathbf{x}) = \nabla \cdot \underline{\underline{\sigma}}(\mathbf{x}) + f_s(\mathbf{x}) \\ i\omega\underline{\underline{\sigma}}(\mathbf{x}) = \underline{\underline{C}}(\mathbf{x}) \underline{\underline{\varepsilon}}(\mathbf{v}(\mathbf{x})) \end{cases}$$

- Free surface condition :  $\underline{\sigma}\mathbf{n} = 0$  on  $\Gamma_I$
- Absorbing boundary condition :  $\underline{\sigma} \mathbf{n} = v_p(\mathbf{v} \cdot \mathbf{n})\mathbf{n} + v_s(\mathbf{v} \cdot \mathbf{t})\mathbf{t}$  on  $\Gamma_a$
- $\rho$  : mass density

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• <u>C</u> : tensor of elasticity coefficients

• 
$$f_{s}$$
 : source term,  $f_{s}\in L^{2}(\Omega)$ 

- v<sub>p</sub> : P-wave velocity
- v<sub>s</sub> : S-wave velocity

## 2D Helmholtz isotropic elastic equations

First order formulation of Helmoltz isotropic wave equations

$$i\omega \mathbf{v}_{\mathbf{x}} = \frac{1}{\rho} \left( \frac{\partial \sigma_{\mathbf{xx}}}{\partial \mathbf{x}} + \frac{\partial \sigma_{\mathbf{xz}}}{\partial z} \right)$$
$$i\omega \mathbf{v}_{\mathbf{z}} = \frac{1}{\rho} \left( \frac{\partial \sigma_{\mathbf{xz}}}{\partial \mathbf{x}} + \frac{\partial \sigma_{\mathbf{zz}}}{\partial z} \right)$$
$$i\omega \sigma_{\mathbf{xx}} = (\lambda + 2\mu) \frac{\partial \mathbf{v}_{\mathbf{x}}}{\partial \mathbf{x}} + \lambda \frac{\partial \mathbf{v}_{\mathbf{z}}}{\partial z}$$
$$i\omega \sigma_{\mathbf{zz}} = \lambda \frac{\partial \mathbf{v}_{\mathbf{x}}}{\partial \mathbf{x}} + (\lambda + 2\mu) \frac{\partial \mathbf{v}_{\mathbf{z}}}{\partial z}$$
$$i\omega \sigma_{\mathbf{xz}} = \mu \left( \frac{\partial \mathbf{v}_{\mathbf{x}}}{\partial z} + \frac{\partial \mathbf{v}_{\mathbf{z}}}{\partial x} \right)$$

$$\lambda$$
 and  $\mu$  Lamé's constants and  $v_{
m p}=\sqrt{rac{\lambda+2\mu}{
ho}}$  and  $v_{s}=\sqrt{rac{\mu}{
ho}}$ 

## 2D Helmholtz isotropic elastic equations

# Vectorial form $i\omega \mathbf{Q} + \mathbf{A}_{\mathbf{x}} \frac{\partial \mathbf{Q}}{\partial \mathbf{x}} + \mathbf{A}_{\mathbf{z}} \frac{\partial \mathbf{Q}}{\partial \mathbf{z}} = 0$ where $\mathbf{Q} = (\mathbf{v}_{x}, \mathbf{v}_{z}, \sigma_{xx}, \sigma_{zz}, \sigma_{xz})^{\mathrm{T}}$ and : $\mathbf{A}_{\mathbf{x}} = - \begin{pmatrix} 0 & 0 & \frac{1}{\rho} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{\rho} \\ \lambda + 2\mu & 0 & 0 & 0 & 0 \\ \lambda & 0 & 0 & 0 & 0 \\ 0 & \mu & 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{A}_{\mathbf{z}} = - \begin{pmatrix} 0 & 0 & 0 & 0 & \frac{1}{\rho} \\ 0 & 0 & 0 & \frac{1}{\rho} & 0 \\ 0 & \lambda & 0 & 0 & 0 \\ 0 & \lambda + 2\mu & 0 & 0 & 0 \\ \mu & 0 & 0 & 0 & 0 \end{pmatrix}$

Centered flux DG scheme Upwind flux DG scheme

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  - Upwind flux DG scheme

3 Numerical results



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DG methods in time domain for seismic applications

#### DG methods in time domain for seismic applications

- M. Dumbser and M. Käser, An arbitrary high-order discontinuous Galerkin method for elastic waves on unstructured meshes - II; The three-dimensional isotropic case, 2006 (upwind scheme)
- S. Delcourte, L.Fezoui and N. Glinsky-Olivier, A high order discontinuous Galerkin method for the seismic wave propagation, 2009 (centered scheme)

Centered flux DG scheme Upwind flux DG scheme

## Notations and definitions

#### Notations

- Γ<sub>1</sub> free surface boundary
- Γ<sub>a</sub> the absorbing boundary
- $\mathcal{T}_h$  mesh of  $\Omega$  composed of triangles K
- $\mathcal{F}_h$  set of all faces F of  $\mathcal{T}_h$
- **n** the normal outward vector of an element K

Centered flux DG scheme Upwind flux DG scheme

## Notations and definitions

#### Definitions

• Jump [[·]] of a vector **u** for *F* :

$$\llbracket u \rrbracket = u^+ \cdot n^+ + u^- \cdot n^- = u^+ \cdot n^+ - u^- \cdot n^+$$

• Jump of a tensor  $\underline{\sigma}$  for F :

$$\llbracket \underline{\underline{\sigma}} \rrbracket = \underline{\underline{\sigma}}^+ \mathbf{n}^+ + \underline{\underline{\sigma}}^- \mathbf{n}^- = \underline{\underline{\sigma}}^+ \mathbf{n}^+ - \underline{\underline{\sigma}}^- \mathbf{n}^+$$



Centered flux DG scheme Upwind flux DG scheme

## Notations and definitions

#### Definitions

• Average 
$$\{\cdot\}$$
 of a variable  $u$ , for  $F$  :

$$\{u\}=\frac{u^++u^-}{2}$$



Centered flux DG scheme Upwind flux DG scheme

# DG formulation of the original equation

$$i\omega \mathbf{Q} + \mathbf{A}_{\mathbf{x}} \frac{\partial \mathbf{Q}}{\partial x} + \mathbf{A}_{\mathbf{z}} \frac{\partial \mathbf{Q}}{\partial z} = \mathbf{0}$$

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# DG formulation of the original equation

$$i\omega \mathbf{Q}\varphi + \mathbf{A}_{\mathbf{x}}\frac{\partial \mathbf{Q}}{\partial x}\varphi + \mathbf{A}_{\mathbf{z}}\frac{\partial \mathbf{Q}}{\partial z}\varphi = \mathbf{0}$$

Centered flux DG scheme Upwind flux DG scheme

# DG formulation of the original equation

$$\int_{K} i\omega \mathbf{Q}^{K} \varphi - \int_{K} \mathbf{A}_{x}^{K} \frac{\partial \mathbf{Q}^{K}}{\partial x} \varphi - \int_{K} \mathbf{A}_{z}^{K} \frac{\partial \mathbf{Q}^{K}}{\partial z} \varphi = \mathbf{0}$$

Centered flux DG scheme Upwind flux DG scheme

# DG formulation of the original equation

$$\int_{K} i\omega \mathbf{Q}^{K} \varphi - \int_{K} \mathbf{A}_{x}^{K} \mathbf{Q}^{K} \frac{\partial \varphi}{\partial x} - \int_{K} \mathbf{A}_{z}^{K} \frac{\partial \varphi}{\partial z} + \sum_{F \in \mathcal{F}(K)} \int_{F} \mathbf{D}_{n} \mathbf{Q} \varphi = \mathbf{0}$$

$$\mathbf{D}_{\mathbf{n}} = n_{\mathbf{x}}\mathbf{A}_{\mathbf{x}} + n_{\mathbf{z}}\mathbf{A}_{\mathbf{z}} = - \begin{pmatrix} 0 & 0 & \frac{n_{\mathbf{x}}}{\rho} & 0 & \frac{n_{\mathbf{z}}}{\rho} \\ 0 & 0 & 0 & \frac{n_{\mathbf{z}}}{\rho} & \frac{n_{\mathbf{x}}}{\rho} \\ n_{\mathbf{x}}(\lambda + 2\mu) & n_{\mathbf{z}}\lambda & 0 & 0 & 0 \\ n_{\mathbf{x}}\lambda & n_{\mathbf{z}}(\lambda + 2\mu) & 0 & 0 & 0 \\ n_{\mathbf{z}}\mu & n_{\mathbf{x}}\mu & 0 & 0 & 0 \end{pmatrix}$$

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## DG formulation of the original equation

#### Global DG formulation

$$\sum_{K \in \mathcal{T}_{h}} \int_{K} i \omega \mathbf{Q} \varphi - \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{x} \mathbf{Q} \frac{\partial \varphi}{\partial x} - \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{z} \mathbf{Q} \frac{\partial \varphi}{\partial z} + \sum_{F \in \mathcal{F}_{h}} \int_{F} \left[ \mathbf{D}_{n} \mathbf{Q} \varphi \right] = 0$$

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## DG formulation of the original equation

#### Global DG formulation

$$\sum_{K \in \mathcal{T}_{h}} \int_{K} i \omega \mathbf{Q} \varphi - \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{x} \mathbf{Q} \frac{\partial \varphi}{\partial x} - \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{z} \mathbf{Q} \frac{\partial \varphi}{\partial z} + \sum_{F \in \mathcal{F}_{h}} \int_{F} \left[ \mathbf{D}_{n} \mathbf{Q} \varphi \right] = 0$$

## $\llbracket \mathsf{D}_{\mathsf{n}} \mathsf{Q} \varphi \rrbracket \simeq (\mathsf{D}_{\mathsf{n}} \mathsf{Q}) \llbracket \varphi \rrbracket$

Centered flux DG scheme Upwind flux DG scheme

# DG formulation of the original equation

#### Global DG formulation

$$\begin{split} \sum_{K \in \mathcal{T}_{h}} \int_{K} i \omega \mathbf{Q} \varphi &- \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{x} \mathbf{Q} \frac{\partial \varphi}{\partial x} - \sum_{K \in \mathcal{T}_{h}} \int_{K} \mathbf{A}_{z} \mathbf{Q} \frac{\partial \varphi}{\partial z} \\ &+ \sum_{F \in \mathcal{F}_{h}} \int_{F} \left( \mathbf{D}_{n} \mathbf{Q} \right) \llbracket \varphi \rrbracket = 0 \end{split}$$

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## Centered flux DG scheme

#### Centered flux on a face F

$$(\mathbf{D}_{\mathbf{n}}\mathbf{Q})|_{F} = \{\mathbf{D}_{\mathbf{n}}\mathbf{Q}\} = \frac{1}{2} \left(\mathbf{D}_{\mathbf{n}}{}^{K}\mathbf{Q}^{K} + \mathbf{D}_{\mathbf{n}}{}^{K'}\mathbf{Q}^{K'}\right)$$

#### Centered flux DG scheme

$$\int_{K} i\omega \mathbf{Q}^{K} \varphi - \int_{K} \mathbf{A}_{x}^{K} \mathbf{Q}^{K} \frac{\partial \varphi}{\partial x} - \int_{K} \mathbf{A}_{z}^{K} \mathbf{Q}^{K} \frac{\partial \varphi}{\partial z} + \sum_{F} \int_{F} \frac{1}{2} \left( \mathbf{D}_{\mathbf{n}}^{K} \mathbf{Q}^{K} + \mathbf{D}_{\mathbf{n}}^{K'} \mathbf{Q}^{K'} \right) \varphi = \mathbf{0}$$

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## Upwind flux DG scheme

### Definition

$$\left\{ \begin{array}{rcl} \mathsf{D}_n^{\,+} &=& \mathsf{R}_n \Gamma^+ \left(\mathsf{R}_n\right)^{-1} \\ \mathsf{D}_n^{\,-} &=& \mathsf{R}_n \Gamma^- \left(\mathsf{R}_n\right)^{-1} \end{array} \right.$$

where

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## Upwind flux DG scheme

#### Definition

$$\begin{cases} D_{n}^{+} = R_{n}\Gamma^{+}(R_{n})^{-1} \\ D_{n}^{-} = R_{n}\Gamma^{-}(R_{n})^{-1} \end{cases}$$

#### and

$$\mathbf{R}_{n} = \begin{pmatrix} n_{x}\mathbf{v}_{p} & -n_{z}\mathbf{v}_{s} & 0 & n_{z}\mathbf{v}_{s} & -n_{x}\mathbf{v}_{p} \\ n_{z}\mathbf{v}_{p} & n_{x}\mathbf{v}_{s} & 0 & -n_{x}\mathbf{v}_{s} & -n_{z}\mathbf{v}_{p} \\ \lambda + 2n_{x}^{2}\mu & -2n_{z}n_{x}\mu & n_{z}^{2} & -2n_{z}n_{x}\mu & \lambda + 2n_{x}^{2}\mu \\ \lambda + 2n_{z}^{2}\mu & 2n_{z}n_{x}\mu & n_{x}^{2} & 2n_{z}n_{x}\mu & \lambda + 2n_{z}^{2}\mu \\ 2n_{z}n_{x}\mu & \mu(n_{x}^{2} - n_{z}^{2}) & -n_{x}n_{z} & \mu(n_{x}^{2} - n_{z}^{2}) & 2n_{z}n_{x}\mu \end{pmatrix}$$

Centered flux DG scheme Upwind flux DG scheme

## Upwind flux DG scheme

#### Upwind flux on a face F

$$\left(\mathsf{D}_{\mathsf{n}}\mathsf{Q}\right)|_{\mathsf{F}} = \left(\mathsf{D}_{\mathsf{n}}^{\mathsf{K}}\right)^{+}\mathsf{Q}^{\mathsf{K}} + \left(\mathsf{D}_{\mathsf{n}}^{\mathsf{K}'}\right)^{-}\mathsf{Q}^{\mathsf{K}'}$$

#### Upwind flux DG scheme

$$\int_{K} i\omega \mathbf{Q}^{K} \varphi - \int_{K} \mathbf{A}_{x}^{K} \mathbf{Q}^{K} \frac{\partial \varphi}{\partial x} - \int_{K} \mathbf{A}_{z}^{K} \mathbf{Q}^{K} \frac{\partial \varphi}{\partial z} + \sum_{F} \int_{F} \left[ \left( \mathbf{D}_{\mathbf{n}}^{K} \right)^{+} \mathbf{Q}^{K} + \left( \mathbf{D}_{\mathbf{n}}^{K'} \right)^{-} \mathbf{Q}^{K'} \right] \varphi = 0$$

Plane wave in an homogeneous medium Circular diffraction

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Plane wave



Computational domain  $\Omega$  setting

Plane wave in an homogeneous medium Circular diffraction

• Physical parameters :

• 
$$\rho = 2.10^3 kg.m^{-3}$$

• 
$$\lambda = 1, 6.10^{1}0Pa$$

• 
$$v_p = 4.10^3 m.s^{-1}$$

• 
$$v_s = 2.10^3 m.s^{-1}$$

- Boundary :
  - boundary conditions on ∂Ω such as :

$$u = \nabla e^{i(k\cos\theta x + k\sin\theta y)}$$
  
where  $k = \frac{\omega}{v_p}$  or  $k = \frac{\omega}{v_s}$ 

Plane wave in an homogeneous medium Circular diffraction

# Plane wave for a frequency f = 2 Hz, component $V_x$



Exact solution

 $P_2$  centered flux DG formulation

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# Plane wave for a frequency f = 2 Hz, component $V_x$



Exact solution

 $P_2$  upwind flux DG formulation

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## Plane wave



Plane wave in an homogeneous medium Circular diffraction

## Plane wave



Mesh size h

#### L<sub>2</sub>-error for the upwind flux

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## Circular diffraction



Configuration of the computational domain  $\boldsymbol{\Omega}$ 

- Physical parameters :
  - $\rho = 2.10^3 kg.m^{-3}$
  - $\lambda = 1, 6.10^{1}0Pa$
  - $\mu = 8.10^9 Pa$

• 
$$v_p = 4.10^3 m.s^{-1}$$

• 
$$v_s = 2.10^3 m.s^{-1}$$

- Boundary :
  - $\Gamma_1$  is a free surface :  $\sigma \mathbf{n} = 0$
  - $\overline{\overline{\Gamma}}_a$  absorbing boundary :  $\underline{\sigma}\mathbf{n} = v_p(\mathbf{v}\cdot\mathbf{n})\mathbf{n} + v_s(\mathbf{v}\cdot\mathbf{t})\mathbf{t}$

• *a* = 2000*m* 

• b = 8000m

•  $\mathcal{T}_h$  composed of 9653 elements

M. Bonnasse-Gahot

Plane wave in an homogeneous medium Circular diffraction

## Results for various frequencies : f = 2 Hz



Exact solution

 $P_1$  centered scheme

Plane wave in an homogeneous medium Circular diffraction

## Results for various frequencies : f = 2 Hz



Exact solution

 $P_1$  upwind scheme

Plane wave in an homogeneous medium Circular diffraction

## Results for various frequencies : f = 2 Hz

Nb dof		Centered	Upwind
144795	$V_x$ $L_2$ -error	3.44e-01	1.49e-01
$(P_1)$	Factres. time (s)	13	16
	Memory	800	980
289590	$V_x$ $L_2$ -error	4.41e-02	4.67e-02
( <i>P</i> <sub>2</sub> )	Factres. time (s)	40	57
	Memory	1900	2800

Numerical statistics

Plane wave in an homogeneous medium Circular diffraction

## Results for various frequencies : f = 4 Hz



Exact solution

 $P_2$  centered scheme

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## Results for various frequencies : f = 4 Hz



Exact solution

P2 upwind scheme

Plane wave in an homogeneous medium Circular diffraction

## Results for various frequencies : f = 4 Hz

Nb dof		Centered	Upwind
144795	$V_x$ $L_2$ -error	1.19	0.506
	Factres. time (s)	13	16
	Memory	800	970
289590	$V_x$ $L_2$ -error	4.24e-01	1.66e-01
	Factres. time (s)	40	57
	Memory	1900	2800

Numerical statistics

Plane wave in an homogeneous medium Circular diffraction

## Results with p - adaptativity

Area of the triangle	Interpolation order	Number of triangles	
]0 ;10000]	0	3	
]10000 ;15000]	1	1745	
]15000 ;20000]	2	3999	
]20000 ;25000]	3	2658	
]25000 ;30000]	4	1248	

Distribution of the interpolation orders

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## Results with p - adaptativity: f = 2 Hz



Exact solution

"p-local" centered scheme

Plane wave in an homogeneous medium Circular diffraction

## Results with p - adaptativity: f = 2 Hz



Exact solution

"p-local" upwind scheme

Plane wave in an homogeneous medium Circular diffraction

## Results with p - adaptativity: f = 4 Hz



Exact solution

#### "p-local" centered scheme

Plane wave in an homogeneous medium Circular diffraction

## Results with p - adaptativity: f = 4 Hz



Exact solution

"p-local" upwind scheme

Plane wave in an homogeneous medium Circular diffraction

## Results with p - adaptativity

	f = 2 Hz		f = 4 Hz	
	Centered	Upwind	Centered	Upwind
$V_x$ $L_2$ -error	5.02e-02	6.00e-02	2.83e-01	2.76e-01
Factres. time (s)	57	79	57	80
Memory	3000	3800	3000	3800

Numerical statistics for both schemes as function of the frequency

Plane wave in an homogeneous medium Circular diffraction

# Comparison between p - adaptativity and p - global for f = 2Hz

	p — adaptativity		p — global	
	Centered	Upwind	Centered	Upwind
$V_x$ $L_2$ -error	5.02e-02	6.00e-02	4.41e-02	4.41e-02
Factres. time (s)	57	79	40	57
Memory	3000	3800	1900	2800

Plane wave in an homogeneous medium Circular diffraction

# Comparison between p - adaptativity and p - global for f = 4Hz

	p — adaptativity		p — global	
	Centered	Upwind	Centered	Upwind
$V_x$ $L_2$ -error	2.83e-01	2.75e-01	4.24e-01	1.66e-01
Factres. time (s)	57	80	40	57
Memory	3000	3800	1900	2800





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## **Conclusion-Perspectives**

#### Conclusion

- Upwind flux DG formulation gives better results on coarse meshes or for high frequencies than centered flux DG formulation
- With the upwind flux DG formulation we obtain one convergence order more than the centered flux DG formulation

- Develop 3D upwind flux DG formulation for Helmholtz equations
- Adapt the program for parallel computing

## **Conclusion-Perspectives**

#### Conclusion

- Upwind flux DG formulation gives better results on coarse meshes or for high frequencies than centered flux DG formulation
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## Perspectives

#### Drawback

• Linear system with 5 unknowns to store

- Use of the upwind flux DG formulation as a reference method
- Compare upwind DG formulation with hybridizable DG formulation
- Construction of a HDG formulation
- Develop other linear solvers for sparse matrices (in collaboration with INRIA team, *Hiepacs*)

## Perspectives

#### Drawback

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- Use of the upwind flux DG formulation as a reference method
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